Niagara Peninsula Energy Incorporated

Asset Management Plan 2011 – 2015



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1 Executive Summary

1.1 Objective of AMP

Niagara Peninsula Energy Inc.'s (NPEI) Asset Management Plan provides a high level overview of the corporation as well as a summary of the corporate objectives, strategies, and practices that go into developing a business plan.

The resultant business plan is summarized in this document for the period 2011-2015 with more details, such as major projects and programs, included for 2011, by dividing expenditures in the major investment buckets under capital, O&M, Billing and Collecting and General and Administrative categories.

The Asset Management Plan could and should be used as a means of sharing information about NPEI and the rational for investments it makes with customers, shareholders, regulators and the general public.

1.2 AMP Components

The Asset Management Plan includes a number of sections. The following is a brief description of the contents for each section:

About NPEI – Section 2

This section provides a description of NPEI's company's overview, geographic location and demand and energy consumption (both historical and forecasted).

Corporate Information – Section 3

This section provides high level corporate information that governs decision making processes and includes vision, mission statement, and corporate values.

System Description and Reliability Performance – Section 4

This section gives a description of the NPEI's distribution system and provides information on all supply points, SCADA, major asset categories and reliability performance, including historical values for SAIFI, SAIDI and CAIDI.

Major External Challenges – Section 5

This section lists external challenges that, in order to be addressed properly, require NPEI to make significant investments, mostly capital in nature. These external challenges include Smart Grid development, DG connections, new loads, both residential and commercial, and municipal infrastructure improvement projects, such as a road widening.

<u>Internal Initiatives – Section 6</u>

This section describes major internal initiatives aimed at improving the performance of NPEI's distribution system. These initiatives include a number of programs, such as replacement of high voltage switching kiosks and submersible transformers, inspection and replacement of poles and pad mounted equipment, and vegetation management.

Business Practices –Section 7

This section describes NPEI's business practices and approach specifically regarding replacement and maintenance of existing distribution assets.

Asset Condition Assessment - Section 8

This section presents results and recommendations from the Asset Condition Assessment study for the distribution assets performed by an external consultant (Kinectrics Inc).

2011 Business Plan - Section 9

This section presents 2011 Business Plan divided into 6 major buckets: Sustainment Capital, Development Capital, Other Capital, Operations & Maintenance, Billing and Collecting and General and Administration. Major programs and projects are also identified within each investment bucket.

2012-2015 Business Plan – Section 10

This section presents the 2012-2015 Business Plans for each of the years in the range using the same buckets as for 2011 Business Plan but without identifying major projects and programs.

2 About NPEI

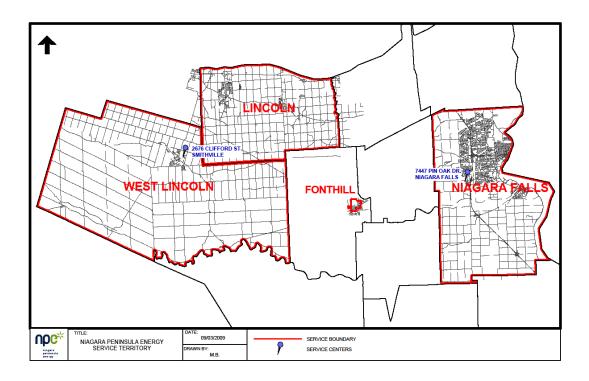
2.1 Company Overview

Niagara Peninsula Energy Inc. (NPEI) was established in 2008 as a result of the amalgamation of Niagara Falls Hydro Incorporated and Peninsula West Utilities Limited. NPEI is a medium sized utility in the Province of Ontario and is responsible for providing all regulated electricity distribution services to over 50,000 residential and business customers in the City of Niagara Falls, the Town of Lincoln, the Township of West Lincoln and the Town of Pelham. Niagara Peninsula Energy has a service area of 827 sq. km.

The table below shows NPEI's Provincial ranking in 3 major categories: number of customers, Net Book Value of Assets and geographic territory.

	Area (sq. km.)	Number of Customers	NBV (\$M)
NPEI	827	> 50,000	101
Ontario Rank	6	14	9

2.2 Geographic Map



NPEI's neighboring utilities are Fortis, Welland Hydro, Niagara-on-the Lake Hydro, Hydro One, Horizon Utilities, Haldimand County Hydro and Grimsby Power.

2.3 Customer Base

Niagara Peninsula Energy Inc. (NPEI) services approximately 45,616 residential and 5,311 commercial customers. Customers in urban portions of the service territory are as follows:

Area	Size	Customers
Niagara Falls Urban	60.8 sq. km.	31,850
Beamsville	10.3 sq. km.	4,153
Vineland	5.9 sq. km.	1,714
Fonthill	1.8 sq. km.	1,161

The majority of NPEI's service territory is rural. NPEI has 748.2 sq. km. of rural territory servicing approximately 12,049 customers.

2.4 Demand and Energy

2.4.1 Energy Usage

The following table summarizes NPEI's energy usage in 2009 and 2010 to present. The remaining columns for 2012 to 2015 are the projected demand forecast for NPEI:

	Energy (gWh)						
Month	2009	2010	2011	2012	2013	2014	2015
January	118	112	117	117	117	118	118
February	98	99	103	103	103	103	104
March	102	100	103	104	104	104	105
April	92	89	92	93	92	93	93
May	91	98	101	102	102	102	103
June	98	107	111	111	111	111	112
July	106	130	135	135	135	136	136
August	118	125	130	130	130	131	131
September	97	98	102	102	102	102	103
October	94	95	99	99	99	99	100
November	94	95	98	99	99	99	100
December	110	111	115	116	116	116	117

Legend:

Actual Usage Data
 Forecasted Using the Weather Normalization Model
Forecasted Based on Assumptions

Energy Usage Forecast Assumptions:

In the years 2012 through 2015, a moderate energy growth of 0.5% is expected year to year. In 2013, NPEI anticipates that energy usage will drop by 0.25% based on the expected completion of the Ontario Power Generation tunnel project in Niagara Falls.

2.4.2 Demand

The following table summarizes NPEI's demand between 2009 and 2015. From 2009 to August 2010, the demand values were obtained from metered data. The remainder of the table contains the projected demand values based on the assumptions stated below:

	Demand (MW)						
Month	2009	2010	2011	2012	2013	2014	2015
January	180	190	187	188	185	186	187
February	183	181	190	191	187	188	189
March	187	167	181	182	178	179	180
April	150	156	156	157	153	154	155
May	157	220	198	199	196	197	198
June	223	223	241	242	239	240	241
July	205	261	265	266	262	264	265
August	255	253	271	272	268	270	271
September	187	188	196	197	193	194	195
October	161	163	169	170	166	167	168
November	177	179	186	187	184	184	185
December	194	196	202	204	201	202	203

Legend:

Actual Demand Data
Forecasted Based on Assumptions

Demand Forecast Assumptions:

In the years 2011 through 2015, the forecasted demand is based on the energy usage forecast and average load factor per month from 2009 and 2010. In 2013, NPEI anticipates that demand will drop by 3 MW based on the expected completion of the Ontario Power Generation tunnel project in Niagara Falls. The tunnel project's demand on NPEI's system averages 3 MW per month.

2.4.3 Load Factor

The following table summarizes NPEI's calculated load factor between 2009 and 2015:

	Demand (MW)						
Month	2009	2010	2011	2012	2013	2014	2015
January	89.6%	80.9%	85.3%	85.3%	86.7%	86.7%	86.7%
February	73.2%	74.7%	74.0%	74.0%	75.1%	75.1%	75.1%
March	74.6%	81.9%	78.3%	78.3%	79.6%	79.6%	79.6%
April	84.0%	78.1%	81.0%	81.0%	82.6%	82.6%	82.6%
May	79.2%	60.9%	70.0%	70.0%	71.1%	71.1%	71.1%
June	60.2%	65.5%	62.8%	62.8%	63.6%	63.6%	63.6%
July	71.3%	68.1%	69.7%	69.7%	70.5%	70.5%	70.5%
August	63.7%	67.7%	65.7%	65.7%	66.4%	66.4%	66.4%
September	71.1%	71.1%	71.1%	71.1%	72.2%	72.2%	72.2%
October	79.9%	79.9%	79.9%	79.9%	81.3%	81.3%	81.3%
November	72.4%	72.4%	72.4%	72.4%	73.6%	73.6%	73.6%
December	77.8%	77.8%	77.8%	77.8%	79.0%	79.0%	79.0%

Legend:

Calculated Load Factor		Calculated Load Factor
------------------------	--	------------------------

3 Corporate Information

3.1 Vision Statement

Niagara Peninsula Energy is committed to delivering environmentally responsible and sustainable energy for the future of our communities.

3.2 Mission Statement

Niagara Peninsula Energy delivers safe, efficient and reliable electricity through dedicated employees in an environmentally sustainable and technologically focused manner. We provide excellence in customer service and respond to the needs of our communities.

3.3 Corporate Values

Niagara Peninsula Energy and its staff will maintain conduct with commitment to the values of:

- Integrity- we are ethical and our actions are truthful and trustworthy
- Fairness- we treat everyone equally and free of bias
- Responsibility- we provide services with safety first for our customers and employees
- Respect- we listen to each other and see value that each member of the team brings and respect the needs of our stakeholders
- Transparency- we are open and accountable for our actions and decisions

4 System Description and Reliability Performance

4.1 System Description

NPEI's distribution system consists of 1059 km of overhead primary feeders and 482 km of underground primary cable. The distribution system operates at one of the following four primary voltages:

- 27.6kV
- 13.8kV
- 8.32kV
- 4.16kV

NPEI's distribution system receives power from the Hydro One operated transmission system through one of the following supply points:

Substation Name	Primary Voltage	Secondary Voltage	# of Transformers	Station Owner	City/Town
Pelham DS	27.6 kV	4.16 kV	1	NPEI	Fonthill
Station DS	27.6 kV	4.16 kV	1	NPEI	Fonthill
Beamsville TS	115 kV	27.6 kV	2	Hydro One	Lincoln
Campden DS	27.6 kV	8.32 kV	1	NPEI	Lincoln
Greenlane DS	27.6 kV	8.32 kV	2	NPEI	Lincoln
Jordan DS	27.6 kV	8.32 kV	1	NPEI	Lincoln
Vineland DS	115 kV	27.6 kV	2	Hydro One	Lincoln
Kalar TS	115 kV	13.8 kV	2	NPEI	Niagara Falls
Murray TS	115 kV	13.8 kV	4	Hydro One	Niagara Falls
NF Station 3	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 6	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 7	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 8	13.8 kV	4.16 kV	2	NPEI	Niagara Falls
NF Station 10	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 14	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 17	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 18	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 22	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
NF Station 23	13.8 kV	4.16 kV	1	NPEI	Niagara Falls
Stanley TS	13.8 kV	4.16 kV	2	Hydro One	Niagara Falls
Bismark DS	27.6 kV	8.32 kV	1	Hydro One	West Lincoln
Niagara West TS	230 kV	27.6 kV	2	NWTC	West Lincoln
Smithville DS	27.6 kV	8.32 kV	1	NPEI	West Lincoln

NPEI monitors its distribution system through a supervisory control system at its main office located in Niagara Falls. The system is used to monitor and control all TS supply breakers feeding NPEI's distribution system. The Supervisory Control and Data Acquisition System ("SCADA") is monitored twenty-four hours a day, seven days a week.

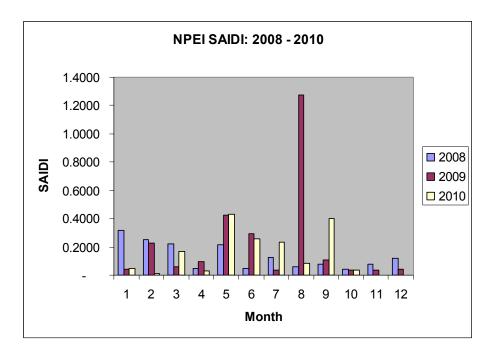
4.2 Main Asset Categories

The table below shows the number of assets in each of NPEI's major asset categories:

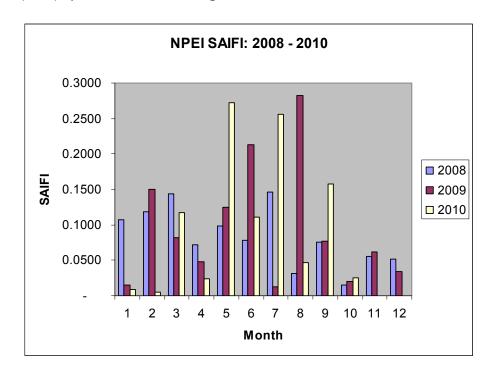
Asset Description	Population
Station Power Transformers	21
Large Pad Mounted Transformers (> 750 kVA)	56
Standard Pad Mounted Transformers (< 750 kVA)	2408
Pole Top Transformers	6835
Poles	22247
Pad Mounted Switchgear	89

4.3 System Performance

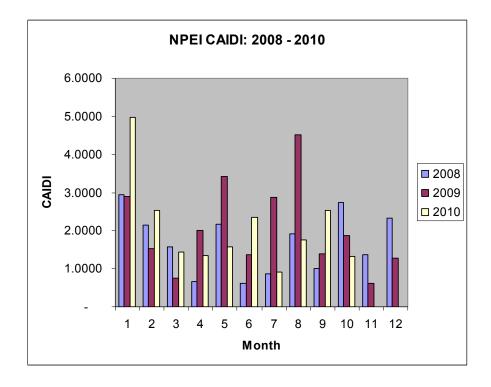
The following chart summarizes NPEI's System Average Interruption Duration Index (SAIDI) by month for 2008 through 2010:



The following chart summarizes NPEI's System Average Interruption Frequency Index (SAIFI) by month for 2008 through 2010:



The following chart summarizes NPEI's Customer Average Interruption Duration Index (CAIDI) by month for 2008 through 2010:



NPEI has compiled outage data used to derive SAIDI, SAIFI, and CAIDI since the merger. This data as well as historical values from the former two utilities indicate higher than desired values for SAIDI, specifically in the western portion of NPEI's service territory. Following the merger, NPEI has implemented initiatives that specifically target improving this index such as the installation of feeder sectionalizing and advanced reclosing devices. In 2010 NPEI's distribution system performed with an improved SAIDI compared to previous years.

5 Major External Challenges

5.1 Smart Grid

NPEI is in the early stages of developing a formal smart grid strategy. NPEI leverages a mature geographic information system (GIS) to manage asset data. NPEI'S high level strategy is to build on the current GIS functionality in support of smart grid operations.

NPEI is currently implementing a work force management / outage management (WFMS/OMS) system that leverages GIS data. This system is used to manage the distribution of work to NPEI crews as well as to manage the distribution system operationally. NPEI has a long term strategy to integrate smart meters and smart devices with the OMS as the foundation of its smart grid.

Smart Grid technologies are factored into new equipment purchases where feasible from a technical and cost perspective.

5.2 DG Connections

NPEI currently has 30 microFIT connections on its system and is averaging 5 new connections per month as of December 2010. NPEI also has 1.25MW of generation connected under the FIT program as well as applications for an additional 10MW.

5.3 Municipal Commitments – Load Growth

NPEI has experienced a moderate and consistent level of load growth in the residential customer class. Approximately 500 new residential customer connections have been performed per year since the incorporation of NPEI.

Commercial development in NPEI's service area has been consistent since incorporation. Approximately 1.5 MVA of new commercial load has been connected to NPEI's system per year.

Currently, NPEI does not supply any significant industrial sector load.

NPEI anticipates that the level of growth in both the residential and commercial customer classes will remain consistent in the coming years. A capital expenditure allowance has been established to permit the connection of new customer loads based upon historical levels.

5.4 Municipal Commitments – Infrastructure

NPEI's capital expenditures have been influenced significantly by external factors in recent years. Federal and provincial stimulus funding for infrastructure improvements has resulted in a substantial increase in municipally driven construction activities. Due to obligations under the Municipal Act to accommodate road reconstruction projects, NPEI has substantially increased capital expenditures related to these activities.

We anticipate that a return to pre-stimulus infrastructure spending levels will reduce the capital requirement for these types of projects. Going forward, NPEI has allocated capital funding for such projects based on pre-stimulus historical requirements. As such projects are externally driven; NPEI may experience elevated levels of investments in this area.

6 Major Internal Initiatives

6.1 Information Technology Initiatives

NPEI manages data related to its assets in a corporate geographic information system (GIS). The GIS is Intergraph's G/Technology system designed and customized for electric utilities based in Ontario. All of the distribution assets that are managed by NPEI are modeled within the GIS. NPEI has invested heavily in GIS data as it provides a foundation for managing the lifecycle of assets. NPEI has integrated the GIS to its corporate customer information system (CIS), financial systems, analysis software, and its outage management system.

Inspection data collected by NPEI is linked to specific asset features within GIS. The GIS is used to analyze inspection results and prioritize the required corrective maintenance or replacement activities. Any maintenance activity and associated data is also tracked in the GIS.

NPEI routinely uses Distribution Engineering Simulation Software (DESS) to analyze the distribution system. NPEI has integrated DESS with the GIS to ensure that the model used for engineering analysis is kept current with minimal effort. DESS supports decisions made by NPEI's engineering and operations staff related to the design and operation of the distribution system.

NPEI is currently implementing an outage management system (OMS). The GIS provides the data utilized by the OMS and as such, the two systems have been integrated. The OMS automates several stages of outage management for operations staff at the utility. The system tracks and manages calls, predicts probable points of failure, and provides a mechanism to dispatch outage related work orders to field crews electronically. Beyond outage type work flows, the system also provides work force management capability. The system is utilized to mange work assignment to operations field staff electronically.

6.2 Kiosk/Submersible Replacement Program

NPEI's distribution system contains approximately 200 legacy switching cubicle installations referred to as kiosks. A kiosk is a masonry structure with a metal or concrete lid that contains primary voltage switching apparatus. These installations do not conform to current distribution standards and are at end of life. The installations are inspected on a 5 year cycle to confirm condition. The inspection results are assessed annually to prioritize units that require replacement with new equipment. In a typical year, NPEI replaces 15 to 20 kiosks.

NPEI also has submersible distribution transformer installations on its system which are at end of life. These installations do not meet current standards and are subject to premature failure. A program is in place to replace these installations with pad mounted transformation. At the end of 2010, NPEI had 18 submersible installations remaining on its distribution system. NPEI typically replaces approximately 20 of these installations a year which will lead to the elimination of submersible transformers from the system by the end of 2011.

6.3 Pole Replacement Program

NPEI has been inspecting and testing poles on its distribution system since 2004. Approximately 5000 poles are tested per year. Wood poles are tested using a sound and bore method. Steel and concrete poles are visually inspected. All overhead distribution apparatus installed on poles are visually inspected at the time of the pole test.

The resulting data from the annual pole testing program is analyzed in order to prioritize the required pole replacements. NPEI replaces between 150 and 250 poles annually under the pole replacement program.

6.4 Switchgear Replacement Program

NPEI has 89 primary voltage switchgear installations on its distribution system. Approximately 20 units are inspected annually. The inspection consists of a visual condition assessment, infrared scan, and ultrasonic scan.

The resulting data from the annual switchgear inspection program is analyzed in order to prioritize the required switchgear replacements. NPEI replaces approximately 4 units per year under the switchgear replacement program.

6.5 Vegetation Management

Following the merger in 2008, NPEI adjusted its tree trimming program for the overall service area. The western portion of the service area (Lincoln, West Lincoln and Fonthill) is split into 4 trimming areas (1 per year) based on experience in growth rate. The eastern portion of the service area (Niagara Falls) is split into 5 trimming areas (1 per year).

6.6 Other Reliability Initiatives

NPEI strives to improve reliability on its distribution system through the design and incorporation of features such as:

- Wildlife Bushing Guards
- Insulated Drop Leads
- Insulated Switch Brackets/Bases
- Over Insulated Components
- Increased Designed Clearances
- Encapsulated Switching and Terminal Components
- Covered Line Wire
- Advanced Reclosers and Controls

The application of these components minimizes the occurrence of foreign interference with the distribution system that negatively impacts the reliability of service to our customers.

7 Business Practices

7.1 Proactive vs. Reactive Replacements

Based on replacement practices, assets can be divided into 2 distinct categories: assets that are replaced "reactively" only when they fail, and assets that are replaced "pro-actively" based on their condition before they fail.

Failure of assets that are replaced "proactively" usually does not result in significant cost and/or risk to corporate objectives and values. Conversely, failure of assets that are replaced "reactively" usually results in significant incremental cost over and above planned replacement cost and, furthermore, poses high risk to objectives and values.

NPEI "proactively" replaces distribution facilities as part of the Internal Initiatives described in the Section 6.

7.2 Maintenance Practices

NPEI follows the requirements outlined in the distribution system code. The following table summarizes maintenance practices on major equipment within NPEI's asset base:

Equipment	Cycle	What is Done
TS/DS Inspection	Monthly	Visual Inspection
Station Transformers	Annually	Oil Analysis, Dissolved Gas Analysis,
		Visual Inspection
Large Padmounted Transformers	Annually	Oil Analysis, Dissolved Gas Analysis,
		Visual Inspection
Small Padmounted Transformers	5 Year Cycle	Infrared Scan, Ultrasonic Scan,
		Visual Inspection
Poles	5 Year Cycle	Sound and Bore (Structural Integrity
		Assessment), Treatment Application,
		Component Inspection
Switchgear	5 Year Cycle	Infrared Scan, Ultrasonic Scan,
		Visual Inspection
Manholes/Civil Structures	5 Year Cycle	Visual Inspection, Cleaning
Switching Kiosks	5 Year Cycle	Condition Review, Prioritized
		Elimination of Legacy Equipment
Vegetation Management	5 Year Cycle	5 Year Cutback

7.3 Work Integration

NPEI adjusts its maintenance practices and sustainment capital programs due to their inherent interdependencies and to account for internal initiatives. An adjustment is made in situations where commercial and operational benefits can be achieved. Examples of this include:

- Reducing capital replacement cost projections to account for distribution plant that will be replaced as a part of an externally driven project, such as a municipal road widening
- Initiation of a rebuild project rather than per pole replacement approach due to the quantity of identified deficiencies in a test area
- Extension in maintenance activities to provide increased life expectancy in distribution assets where a known end of service date exists

8 Asset Condition Assessment

NPEI retained the services of Kinectrics Inc. to carry out an Asset Condition Assessment of NPEI's key distribution assets. The resulting Distrubtion Asset Condition Assessment report is included in Appendix A of this document.

9 2011 Business Plan

9.1 Sustaining Capital with Major Project Types

Item	Project Type	Sustainment Capital
1	Replacement of distribution facilities due to	\$2,005,619
	deteriorated condition	
2	Line extensions/relocations due to municipal road work	\$388,370
	requirements	
3	Replacement of poles identified with limited structural	\$1,226,524
	integrity	
4	Required overhead line rebuild of deteriorated facilities	\$776,740
	identified in the pole condition survey	
5	Replacement of kiosks and submersible transformers	\$480,835
6	Minor Betterments	\$488,926
		\$5,367,014
	Less Capital Contributions	\$-100,000
	Total	\$5,267,014

9.2 Development Capital with Major Project Types

Item	Project Type	Development Capital
1	Expansion of the primary distribution system to	\$1,295,495
	accommodate load growth and reliability requirements	
2	Subdivisions and new residential services	\$631,059
3	Demand based system requirements for new	\$1,156,938
	commercial service connections and expansions	
	Projects under materiality	\$194,185
		\$3,227,677
	Less Capital Contributions	\$-750,000
	Total	\$2,527,677

9.3 Other Capital

Item	Туре	Other Capital
1	Metering	\$185,185
2	Vehicles	\$462,963
3	Other Capital	\$659,954
	Total	\$1,308,102

9.4 O&M with Major Categories

Item	Туре	Other Capital
1	Stations	\$190,778
2	Overhead Lines	\$1,921,782
3	Underground	\$651,140
4	Other	\$3,378,406
	Total	\$6,142,106

9.5 Billing and Collecting with Major Categories

Item	Туре	Other Capital
1	Billing	\$3,302,566
2	Collecting	\$893,163
3	Community Relations	\$81,464
	Total	\$4,277,193

9.6 General and Administration

Item	Туре	Other Capital
1	G & A	\$3,876,136

10 2012-2015 Business Plan

10.1 Sustaining Capital

Year	Amount
2012	\$5,223,331
2013	\$5,320,205
2014	\$5,368,186
2015	\$5,464,149

10.2 Development Capital

Year	Amount
2012	\$2,766,249
2013	\$2,908,623
2014	\$2,981,100
2015	\$3,101,559

10.3 Other Capital

Year	Amount
2012	\$1,324,074
2013	\$1,273,148
2014	\$1,273,148
2015	\$1,273,148

10.4 O&M

Year	Amount
2012	\$6,278,477
2013	\$6,418,728
2014	\$6,562,315
2015	\$6,709,323

10.5 Billing and Collecting

Year	Amount
2012	\$4,365,422
2013	\$4,463,294
2014	\$4,563,847
2015	\$4,667,161

10.6 General and Administration

Year	Amount		
2012	\$3,963,342		
2013	\$4,052,768		
2014	\$4,144,473		
2015	\$4,238,521		

Appendix A – NPEI Distribution Asset Condition Assessment Report

The remaining pages of this document contain the Distribution Asset Condition Assessment Report produced by Kinectrics Incorporated.





Niagara Peninsula Energy Inc

Distribution Asset Condition Assessment

Kinectrics Report: K-418046-RC-001-R3

February 10, 2011

PRIVATE INFORMATION

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DISCLAIMER

Kinectrics Inc. has prepared this report in accordance with, and subject to, the terms and conditions of the agreement between Kinectrics Inc. and Niagara Peninsula Energy Inc.

@Kinectrics Inc., 2011.

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DISTRIBUTION ASSET CONDITION ASSESSMENT

Kinectrics Report: K-418046-RC-001-R3

February 10, 2011

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KINECTRICS INC ii K-418046-RC-001-R3

Revision History

Revision Number	Date	Comments	Approved
R0	December 20, 2010	Initial Draft	N/A
R1	January 28, 2011	Final Draft	N/A
R2	February 9, 2011	Final Report	SC
R3	February 10, 2011	Final Report (re-formatted)	

EXECUTIVE SUMMARY

Niagara Peninsula Energy Inc (NPEI) retained Kinectrics Inc. (Kinectrics) to carry out an Asset Condition Assessment (ACA) of NPEI's key distribution assets. The assets were divided into several Asset Groups. For each of these Asset Groups, the ACA included the following tasks:

- Derive Health Indexes
- Conduct Field Surveys
- Provide Capital Replacement Plan
- Recommend condition data gap closure strategy

This report summarizes the methodology, demonstrates specific approaches used in this project, and presents the resultant findings and recommendations.

Information Availability and Health Index Methodology

The general methodology for Asset Condition Assessment is described, while each Asset Group is presented in detail in its own section. Where appropriate, the formulations were modified based on the expert opinion of NPEI staff, for example air-insulated pad mounted switchgear located near major roads were automatically assigned poor condition and, thus, flagged for replacement. Field observations generally supported the Health Index distribution derived using Kinectrics' methodology. Some differences could be attributed to the fact that the field survey observations weigh all the condition parameters equally while the Health Index formulation used a weighted sum of condition parameters scores.

Health Index Results Summary

For six of the seven Asset Groups there was sufficient asset information to calculate Health Indexes. Table ES - 1 shows, for each of the seven Asset Group, the total number of assets, sample size, and Health Index distribution. Detailed results for each Asset Group are shown in Section C RESULTS AND FINDINGS.

Table ES - 1 Health Index Results Summary

ASSET			SAMPLE SIZE		HEALTH INDEX DISTRIBUTION				
No	Description	Population	Units	%	Very Poor	Poor	Fair	Good	Very Good
1	Power Transformers	21	21	100%	0%	17%	26%	22%	35%
2	Large Pad Mounted Transformers	56	51	91%	0%	2%	6%	27%	65%
3	Standard Pad Mounted Transformers	2,408	716	30%	5%	1%	1%	4%	89%
4	Pole Top Transformers	6,835	6,711	98%	1%	4%	11%	17%	67%
5	Poles	22,247	5,985	27%	0%	5%	6%	28%	61%
6	Pad Mounted Switchgear	89	38	43%	8%	34%	3%	18%	37%

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Capital Replacement Plan

The Capital Replacement Plan (CRP) includes two aspects: the number of units that are planned to be replaced and the corresponding replacement cost. For asset categories 2 through 6 capital requirements for the whole population were extrapolated from the sample and the comments regarding appropriateness of such an assumption were included in Section C for each of these asset categories.

The number of units to be replaced was estimated based on asset condition and the corresponding probability of failure. Table ES - 2 summarizes the assumed replacement cost, replacement plan approach, and resultant capital replacement plan in the first year as well as the capital replacement plan approach. Assets which are 'run to failure' are replaced reactively, compared to those assets which are replaced proactively.

Table ES - 2 Capital Replacement Plan Summary

Asset	Assumed Replacement Cost	Units to Replace in First Year	Planned Capital Replacement Cost in First Year	CRP Approach	
Power Transformers	\$300,000	1	\$300,000	Proactive	
Large Pad Mounted Transformers	\$45,000	0	\$0	Proactive	
Standard Pad Mounted Transformers	\$15,000	31	\$465,000	Proactive	
Pole Top Transformers	\$5,000	38	\$190,000	Reactive	
Poles	\$5,000	160	\$800,000	Reactive	
Pad Mounted Switchgear	\$75,000	5	\$375,000	Proactive	

The scheduling of capital expenditure for assets which are replaced **proactively** has been levelized so replacement is done over a period of time after the optimal replacement year. Those assets which are replaced **reactively** also have a levelized schedule so replacement is done over a period of time before the optimal replacement year. This methodology is to ensure that run to failure assets are replaced before they fail.

Figure ES -1 presents the Overall Levelized Capital Replacement Plan. This is the total replacement projections for all the assets over the next five (5) years in 2011 dollars (cost does not take inflation rates into account).

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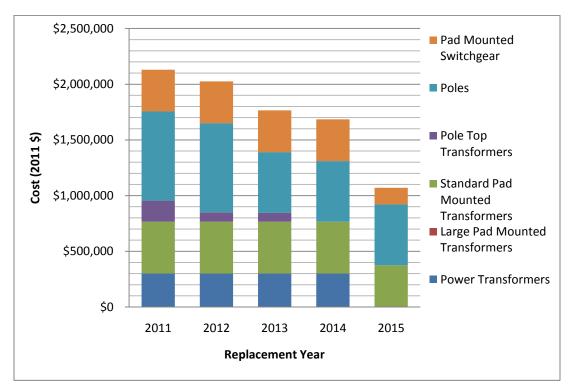


Figure ES - 1 Five Year Capital Replacement Plan

Conclusions and Recommendations

- 1. There was generally sufficient condition data available for Power Transformers, Large Padmounted Transformers, Poles (inspected after 2008) and Switchgear.
- For Pole-mounted transformers, only age and operating practices were available (i.e., number of customers serviced by each transformer). Gathering and recording detailed inspection data should be considered.
- 3. For Standard Pad Mounted Switchgear, age was provided for 87% of the population however sufficient data was provided for only 28% of the population. It is recommended that NPEI collect data for a greater population of Pad Mounted Switchgear.
- 4. For Poles that have not been inspected, age is only available for half of the population. Sufficient age and inspection data should be collected for the rest of the population.
- 5. Sufficient data was not available for Underground Cables. It is recommended that inspection and maintenance information be collected for these assets to enable future asset condition assessment.

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6. Comparison of poles with adequate condition data vs poles with only age known shows that the former have a better overall condition than the latter. This is due to the fact that over the last several years substantial capital investments were made to achieve that. It is therefore recommended that capital investments be made to bring be made to bring the rest of the pole population to the same Health Index distribution as the subset with adequate condition data.

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A INTRODUCTION

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To: Niagara Peninsula Energy 7447 Pin Oak Drive Niagara Falls, ON L2E 6S5

INTRODUCTION

Niagara Peninsula Energy Inc (NPEI) supplies electricity to homes and businesses and is regulated by the Ontario Energy Board.

Kinectrics Inc. (Kinectrics) is an independent consulting engineering company with the advantage of 90 years of expertise gained as part of one of North America's largest integrated electric power companies. Kinectrics has a depth of experience in the area of transmission and distribution systems and components and has become a prime source of Asset Management and Asset Condition services to some of the largest power utilities in North America.

NPEI retained the services of Kinectrics to carry out condition assessment of its electrical distribution system assets.

A considerable portion of this work was devoted to the development of Health Indices based on the information provided by NPEI, a brief visual field survey conducted by Kinectrics and the expert opinion of NPEI staff.

This report presents the findings of the NPEI's distribution assets condition assessment and includes the development of Health Indices for the specified Asset Groups.

Objective

Kinectrics performed an Asset Condition Assessment of NPEI's electrical distribution system. The following distribution system assets, referred to as Asset Groups throughout this report, were covered under the scope of work for this project:

- 1 Power Transformers
- 2 Large Pad-Mounted Transformers
- 3 Standard Pad-Mounted Transformers
- 4 Pole-Top Transformers
- 5 Poles
- 6 Pad Mounted Switchgear

As part of the asset condition assessment, a visual inspection of the power system physical assets was conducted by Kinectrics. The objective of the inspections was to confirm the average condition of the equipment as indicated by the condition data bases provided to Kinectrics.

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Scope of the Work

The project includes the following:

- 1 Provide Recommended Health Index formulations used to derive Health Indices
- 2 Calculate and provide Health Index distribution for each of the aforementioned asset categories
- 3 Provide Capital Replacement Plan
- 4 Identify condition data gaps and provide recommendations for their prioritized closure

These areas and the factors of assessments covered under this project, are based on Kinectrics experience and familiarity with the industry requirements, and provides rational for the capital replacement expenditures being sought by NPEI. As such, the results will help NPEI in its service rate application submission to the OEB and will provide a basis for a medium to long-term capital plan for its distribution assets. It is worth noting, however, that replacement requirement due to poor asset condition is not the only basis for developing a capital plan: other factors, such as obsolescence, design flaws, exposure to severe environmental conditions, system requirements, etc. should also be taken into account when developing such plan.

Visual field inspection was conducted at several locations and included:

- 3 locations of three-phase pad mounted transformers
- 2 locations of overhead switches
- 5 locations of wood poles
- 2 locations of pole mounted transformers,
- 1 location of pad mounted switchgear
- 2 locations of distribution station transformers.

All of the locations were inspected directly by Kinectrics staff that traveled to the sites accompanied by a NPEI employee. The sample locations were scattered at 11 geographic areas within the service territory of NPEI.

Deliverables

The deliverables in this report include the following information:

- Short description of the asset groups being considered in the study
- Discussion of asset degradation and end-of-life issues
- Health Index results for the Asset Groups
- Description of methodology for assessment of asset replacements
- Capital replacement plan
- Data Gap Closure
- Field inspection results

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B ASSET CONDITION ASSESSMENT METHODOLOGY

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Niagara Peninsula Energy Inc Distribution Asset Condition Assessment

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Health Indexing

Health Indexing quantifies equipment condition based on numerous condition criteria that are related to the long-term degradation factors that cumulatively lead to an asset's end of life. The Health Index (HI) is an indicator of the asset's overall health and is typically given in terms of percentage, with 100% representing an asset in brand new condition. Health Indexing differs from maintenance testing, whose objective is finding defects and deficiencies that need correction or remediation in order to keep an asset operating prior to reaching its end of life.

Condition Parameters are the asset characteristics that are used to derive the Health Index. In formulating a Health Index, condition parameters are ranked and evaluated, through the assignment of corresponding weights, based on their contribution to asset degradation. The condition parameter score is an evaluation of an asset with respect to a condition parameter.

A condition parameter may also be comprised of several sub-condition parameters. For example, a parameter called "insulation" for power transformers may be a composite of Oil Quality and Oil DGA.

The Health Index, which is a function of the condition parameter scores and weightings, is therefore given by:

$$HI = \frac{\sum_{m=1}^{\forall m} \alpha_m (CPS_m \times WCP_m)}{\sum_{m=1}^{\forall m} \alpha_m (CPS_{m.\max} \times WCP_m)}$$

where

$$CPS = \frac{\sum_{n=1}^{\forall n} \beta_n (CPF_n \times WCPF_n)}{\sum_{n=1}^{\forall n} \beta_n (CPF_{n.\max} \times WCPF_n)}$$

CPS Condition Parameter Score
WCP Weight of Condition Parameter

 α_{m} Data availability coefficient for condition parameter

(=1 when data available, =0 when data unavailable)

CPF Sub-Condition Parameter Score WCPF Weight of Sub-Condition Parameter

 β_n Data availability coefficient for sub-condition parameter

(=1 when data available, =0 when data unavailable)

While weightings are assigned based on the priority level of condition parameters, scores represent the evaluation of an asset against condition criteria. A condition criterion is the scale that is used to determine an asset's score for a particular parameter.

Consider, for example, a system where the Health Index is described under one of the following five categories: very poor, poor, fair, good, and very good. A scoring system of 0 through 4 corresponds to the "very poor" through "very good" categorization. Consider a parameter "age" for which this scoring

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system is applied. The condition criteria will define the age that constitutes scores of 0 through 4 (i.e. a pole mounted transformer that is 50 years old will receive a score of 0; whereas one that is 2 years old will receive the maximum score of 4). Note that in this study, the condition criteria scoring system consist of values from zero (0) through four (4), with 0 being the worst and 4 being the best score.

De-rating factors are also used to adjust a calculated Health Index to reflect certain conditions. These may be factors that may or may not be related to asset condition, but contribute to the asset's risk of failure. For example, an air-insulated Pad Mounted Switchgear by a major roadway is prone to problems. Dominant parameters may be used as de-rating factors. These are asset properties that are considered to be of such importance that its status has a dominant impact on the value of the Health Index. De-rating factors are used to reduce the Health Index of an asset by a certain percentage. If a calculated Health Index is, say, 90%, a de-rating factor of 80% will reduce the effective Health Index to 90% x 80% = 72%.

Relating Health Index to Effective Age

Once the Health Index of an asset is determined, its *effective age* can be evaluated by establishing a relationship between its Health Index and its probability of failure. Effective age is different from chronological age in that it is based on the asset's condition and the stress stresses applied to the asset.

Probability of Failure

Where failure rate data is not available, a frequency of failure that grows exponentially with age provides the best model. The failure rate equation is in the form of:

$$f = e^{\beta(t-\alpha)}$$

where

f = failure rate of an asset (frequency or the number of expected failures per year) at time t

t = time

 α , β = constant parameters that control the rise of the curve

The corresponding probability of failure is given as:

$$P_f = 1 - e^{-(f - e^{\alpha \beta})/\beta}$$

where

P_f = probability of failure
f = failure rate of an asset

 α , β = constant parameters that control the rise of the curve

Different assets groups experience different failure rates and therefore different probabilities of failure. As such, the shapes of the failure and probability curves are different. The parameters α and β are used

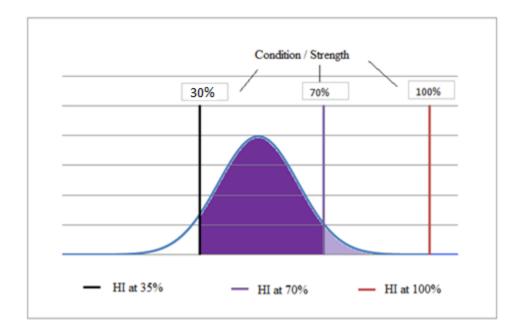
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control the location and steepness of the exponential rise of these curves. For each asset group, the values of these constant parameters were selected to reflect typical useful lives for these assets.

Quantitative Relationship Between Health Index and Probability of Failure

Failure of an asset occurs when the stress that an asset experiences exceeds is strength. Assuming that stress is not constant and the stress probability is normally distributed, the probability of stress exceeding asset strength leads to the probability of failure.

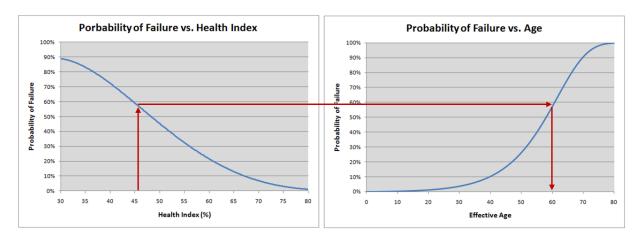
Consider the Health Index to be a representation of condition. Two Health Index points and the probabilities of failure at those Health Index points can be used to find the probabilities of failure at other Health Index values. This is illustrated in the figure below. The vertical line represents condition (Health Index) and the area under the curve to the right of the line represents the probability of failure. A Health Index of 100% represents an asset that is in brand new condition and a Health Index of 30% at its end of life. Moving the vertical line left from 100% to 30%, the probabilities of failure at other Health Indices can be found.



Effective Age and Remaining Life

The effective age associated with a particular Health Index is found by first plotting the Probability of Failure vs. Health Index curve. This is the area under the probability density curve between the 100% and 30% Health Index points. This curve is shown on the left hand graph of the figure below. The associated probability of failure is then found on Probability of Failure vs. Age graph (right hand graph). The effective age is read from the horizontal axis of the right hand graph.

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Relationship between Health Index and Effective Age

The remaining life can be estimated as the difference between the asset's maximum life expectancy and its effective age. For example, a pole mounted transformer that has an effective age of 35 years will have a remaining life of 45-35 = 10 years.

Capital Replacement Plan

Simple Replacement

Asset groups that have little consequence of failure or that are run to failure are reactively replaced. The number of predicted failures multiplied by the replacement cost per unit at the year of failure determined the yearly investments for the asset group.

Risk Analysis

For assets that are have a high consequence of failure (i.e. power transformers), risk analysis determined the economic optimal time of intervention. Planned replacement cost, cost of failure, and risk cost were considered.

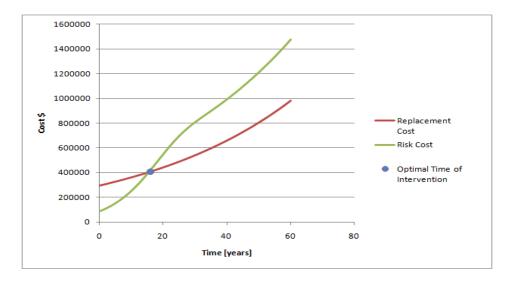
The utility's costs of failure for an asset can include the replacement cost of the asset, any collateral damage to adjacent equipment, environmental clean-up costs, overtime labour premiums, and the lost revenue. Some utilities also include the cost of interruptions to customers. For this analysis, the cost of failure was estimated as a multiple of its planned replacement cost. For non-critical power transformers, the cost of failure was defined as 1.5 times the planned replacement cost, whereas for critical power transformers, the cost of failure multiple was 2.

The *risk cost* is defined as the failure cost times the probability of failure, probability of failure is dependent on an asset's effective age.

The optimal time of intervention (refurbishment or replacement) was found as the point where the risk cost begins to exceeds the replacement cost. The number of units that were flagged for replacement in

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a given year times replacement cost for the given year determined the investment required for that year.



Data Gap Closure

Prioritized strategy for data gap closure is included for each asset category using 3 priority levels, from the highest (3 stars) to the lowest (a single star). It is recommended to start collecting condition data for the highest priority condition parameters as this will improve credibility of the Health Index results the most. This is the case for both assets with some condition data available and assets with no condition data available.

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C RESULTS AND FINDINGS

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1 Power Transformers

The application of substation station transformers generally involves the step down of a higher to lower voltage. Power transformers vary in capacity and ratings over a broad range.

Station transformers employ many different design configurations, but they are typically made up of the following main components:

- Primary, secondary and, possibly, tertiary windings
- Laminated iron core
- Internal insulating media
- Main tank
- Bushings
- Cooling system, including radiators, fans and pumps (Optional)
- Off load tap changer (Optional)
- On load tap changer (Optional)
- Instrument transformers
- Control mechanism cabinets
- Instruments and gauges

1.1 Degradation Mechanism

For a majority of transformers, End-of-Life (EOL) is expected to be caused by the failure of the insulation system and more specifically the failure of pressboard and paper insulation. While the insulating oil can be treated or changed, it is not practical to change the paper and pressboard insulation. The condition and degradation of the insulating oil, however, plays a significant role in aging and deterioration of the transformer, as it directly influences the speed of degradation of the paper insulation. The degradation of oil and paper in transformers is essentially an oxidation process. The three important factors that impact the rate of oxidation of oil and paper insulation are the presence of oxygen, high temperature, and moisture.

Oil analysis is such a powerful diagnostic and condition assessment technique that combining it with background information, related to the specification, operating history, loading conditions and system related issues, provides a very effective means of assessing the condition of transformers and identifying units with a probable high risk of failure. It is the ideal means on which to base an ongoing management strategy for aging transformers, identifying units that warrant consideration for continued use, consideration of remedial measures to extend life or identification of transformers that should be considered for replacement within a defined time frame.

Other condition assessment techniques for substation transformers include the use of online monitors, capable of monitoring specific parameters, e.g. dissolved gas monitors, continuous moisture measurement or temperature monitoring, winding continuity checks, DC insulation resistance measurements and no-load loss measurements. Dielectric measurements that attempt to give an indication of the condition of the insulation system include dielectric loss, dielectric spectroscopy, polarization index, and recovery voltage measurements. Doble testing is a procedure that falls within this general group. Other techniques that are commonly applied to

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transformers include infrared surveys, partial discharge detection and location using ultrasonic and/or electromagnetic detection and frequency response analysis.

The health indicator parameters for substation transformers usually include:

- Condition of the bushings
- Condition of transformer tank
- Condition of gaskets and oil leaks
- Condition of transformer foundations
- Oil test results
- Transformer age and winding temperature profiles
- Maximum loading profile

1.1.1 Failure Mechanism of Station Transformers

1.1.1.1 Thermal Aging:

Thermal aging involves the progress of chemical and physical changes because of chemical degradation reactions, polymerization, depolymerization, and diffusions.

1.1.1.2 Electrical Aging:

Electrical aging, as it relates to AC, impulse, or switching involves the effects of the following:

- partial discharges
- treeing
- electrolysis
- increased temperatures produced by high dielectric losses
- space charges

1.1.1.3 Mechanical Aging

Mechanical aging involves the following:

- fatigue failure of insulation components caused by a large number of low-level stress cycles
- thermo mechanical effects caused by thermal expansion and or contraction
- rupture of insulation by high levels of mechanical stress such as may be caused by external forces or operation condition of the equipment
- Insulation creep or flow under electrical, thermal, or mechanical stresses

1.2 Health Index Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m} \times WCP_{m})}{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m.\max} \times WCP_{m})} \times DF$$

where

$$CPS = \frac{\displaystyle\sum_{n=1}^{} \beta_{n} \left(CPF_{n} \times WCPF_{n} \right)}{\displaystyle\sum_{n=1}^{} \beta_{n} \left(CPF_{n.max} \times WCPF_{n} \right)} \times 4$$

CPS --- Condition Parameter Score

WCP --- Weight of Condition Parameter

DF --- De-rating Factor

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_m --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

1.3 Condition and Sub-Condition Parameters

Table 1-1 Condition Weights and Maximum CPS

	U					
	m	Condition parameter	WCP _m	CPS _{m.max}		
	1	Insulation	4	4		
Ī	2	Sealing & Connection	1	4		
	3	Service record	3	4		

Table 1-2 Insulation (m=1) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Oil Quality	4	4
2	Oil DGA	5	4

1.3.1 *Oil Quality*

Table 1-3 Oil Quality Test

Condition Rating	CPF	Description	
Α	4	Overall factor is less than 1.2	
В	3	verall factor between 1.2 and 1.5	
С	2	Overall factor is between 1.5 and 2.0	
D	1	Overall factor is between 2.0 and 3.0	
E	0	Overall factor is greater than 3.0	

Where the Overall factor is the weighted average of the following gas scores:

Table 1-4 Oil Quality Overall Factoring

		Scores				
		1	2	3	4	Weight
Diele	ctric Str. kV D877	>40	>30	>20	Less than 20	3
	230 kV ≤ U	>32	25-32	20-25	Less than 20	2 *
IFT* dynes/cm	69 kV <u< 230<="" td=""><td>>30</td><td>23-30</td><td>18-23</td><td>Less than 18</td><td></td></u<>	>30	23-30	18-23	Less than 18	
ayes, e	U ≤ 69 kV	>25	20-25	15-20	Less than 15	
	Color		1.5-2	2-2.5	> 2.5	2
	230 kV ≤U	Less than 0.03	0.03-0.07	0.07- 0.1	>0.1	
Acid Number*	69 kV <u< 230<="" td=""><td>Less than 0.04</td><td>0.04-0.1</td><td>0.1- 0.15</td><td>>0.15</td><td></td></u<>	Less than 0.04	0.04-0.1	0.1- 0.15	>0.15	
	U ≤ 69 kV	Less than 0.05	0.05-0.1	0.1- 0.2	>0.2	1 *

^{*} Select the row applicable to the equipment rating

$$\text{Overall Factor} = \frac{\sum Score_i \times Weight_i}{\sum Weight}$$

1.3.2 Oil Dissolved Gas Analysis (DGA)

Table 1-5 Transformer DGA

Condition Rating*	CPF	Description	
Α	4	DGA overall factor is less than 1.2	
В	3	DGA overall factor between 1.2 and 1.5	
С	2	DGA overall factor is between 1.5 and 2.0	
D	1	DGA overall factor is between 2.0 and 3.0	
E	0	DGA overall factor is greater than 3.0	

*In the case of a score other than A, check the variation rate of DGA parameters. If the maximum variation rate (among all the parameters) is greater than 30% for the latest 3 samplings or 20% for the latest 5 samplings, overall Health Index is multiplied by 0.9 for score B, 0.85 for score C, 0.75 for score D and 0.5 for score E.

Where the DGA overall factor is the weighted average of the following gas scores:

Scores 1 2 3 4 5 6 Weight H2 <=100 <=200 <=300 <=500 <=700 >700 2 CH4(Methane) <=120 <=150 <=200 <=400 <=600 >600 3 C2H6(Ethane) <=65 <=100 <=150 <=250 <=500 >500 3 3 C2H4(Ethylene) <=50 <=80 <=150 <=250 <=500 >500 C2H2(Acetylene) <=3 <=7 <=35 <=50 <=80 >80 5 CO <=350 <=700 <=900 <=1100 <=1300 >1300 1 CO2 <=2500 <=3000 <=4000 <=4500 <=5000 >5000 1

Table 1-6 Oil DGA Overall Factoring

$$\text{Overall Factor} = \frac{\sum Score_i \times Weight_i}{\sum Weight}$$

Table 1-7 Sealing & Connection (m=2) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Tank Oil Leak	1	4
2	Conservator Oil Level	1	4

Table 1-8 Service Record (m=3) Weights and Maximum CPF

n Sub-Condition Parameter		WCPF _n	CPF _{n.max}	
ĺ	1	Age	1	4

1.3.3 *Age*

Table 1-9 Transformer Age

		<u> </u>
Condition Rating	CPF	Description
Α	4	0-19
В	3	20-29
С	2	30-44
D	1	45-54
Е	0	>=55

1.4 Health Index Results

The total population of assets for this category is 23. The Sample Size or total number of assets within the population that have data is 23, which means there was data for each asset.

The year purchased was assumed to the transformers age. There was full data for Oil dissolved gas analysis (DGA). It is recommended that data be collected on moisture ppm, power factor (for winding doble score), as well as collecting data on grounding and IR thermography.

The Health Indexing Result by Unit and Percentage are presented below:

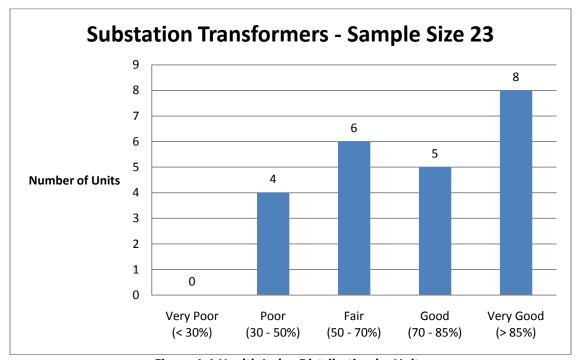


Figure 1-1 Health Index Distribution by Units

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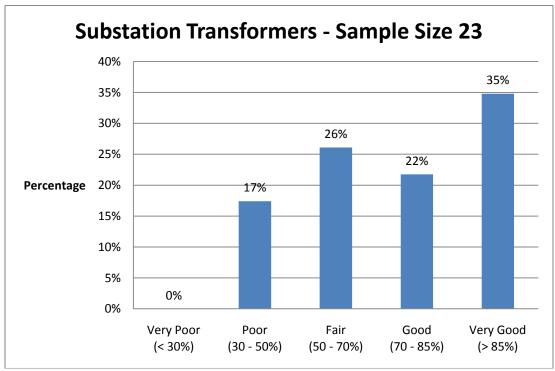


Figure 1-2 Health Index Distribution by Percentage

The exact rating for each Transformer is presented below:

Table 1-10 Substation Health Index Score and Criticality

Transformer No	Substation Name	Score	HI Rating	Critical
SD71844-3	SMITHVILLE DS - NF1844	38%	POOR	YES
SD1856-T2	GREEN LANE D.S NF 1856	43%	POOR	YES
SD71844-1	SMITHVILLE DS - NF1844	50%	POOR	YES
SD71844-2	SMITHVILLE DS - NF1844	50%	POOR	YES
SD1856-T1	GREEN LANE D.S NF 1856	56%	FAIR	YES
800089	VIRGINIA A-144	59%	FAIR	NO
800095	MARGARET A-127	61%	FAIR	YES
800073	ARMOURY A-113	61%	FAIR	NO
800084	ALLENDALE A-175	69%	FAIR	NO
SD1850	CAMPDEN D.S NF 1850	69%	FAIR	YES
SD001	STATION ST. D.S.	74%	GOOD	NO
800100	O'NEIL A-148	81%	GOOD	NO
800082	ALLENDALE A-175	81%	GOOD	NO
800295	LEWIS A-119	78%	GOOD	NO
800077	ONTARIO A-115	78%	GOOD	NO

800389	DRUMMOND A-122	86%	VERY GOOD	NO
800052	PARK A-33	86%	VERY GOOD	NO
800054	VIRGINIA A-144	88%	VERY GOOD	NO
2515T2	KALAR TS	93%	VERY GOOD	NO
800388	PEW A-135	93%	VERY GOOD	NO
800053	SWAYZE A-145	100%	VERY GOOD	NO
2515T1	KALAR TS	100%	VERY GOOD	NO
SD1836	JORDAN D.S NF 1836	100%	VERY GOOD	YES

1.5 Field Inspection Results

Four Power Transformers were inspected. The data can be found in Section E FIELD INSPECTION FORMS and the summary is shown in Figure 1-3 below. There were no major concerns with the units inspected.

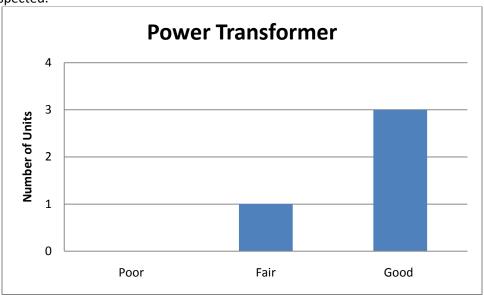


Figure 1-3 Field Inspection Results

1.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 25 years the probability of failure is 10% and at age of 45 years the probability of failure is 90%.

1.6.1 Optimal Capital Replacement Plan

Figure 1-4 shows the number of Transformer units that will need to be replaced over the next 20 years for the whole population extrapolated from the results for the sample with adequate condition data. Given the full sample size (100%) the recommendations are for the entire population.

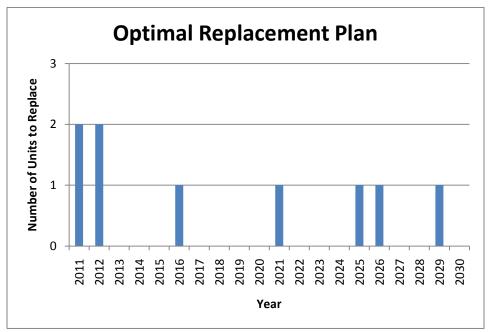


Figure 1-4 Optimal Replacement Plan

1.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing 2 units in the next year. While this is optimal based on NPEI's Power Transformers HI scores, it may not be ideal financially.

Power Transformers are replaced **proactively**. The Levelized replacement plan allows for Transformers that would optimally be replaced in one year to be replaced over a period of time in the future.

Figure 1-5 shows a Levelized capital replacement plan, where transformer replacements can occur over a longer period of time.

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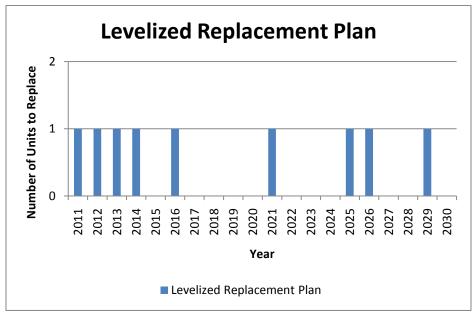


Figure 1-5 Levelized Replacement Plan

1.7 Data Gap Closure

The following table summarizes the data gap for power transformers in this project.

	•	
Sub-system	Condition Parameter	Data Collection Priority
Insulation	Winding Doble	* *
Cooling	Temperature	**
Sealing & connection	Grounding	*
	IR thermography	**
Service record	Loading	☆☆

Table 1-11 Data Gap Closure

IR thermography is a useful approach in detecting hot spots due to a loose connection or leakage. In this project, it also can address the temperature issue in cooling system as well as the transformer loading status, when the data on those 2 parameters are unavailable.

In the sub-system of insulation, another parameter "oil quality" indirectly addresses the winding insulation deterioration, as it detects on some contents that are the consequence of insulation deterioration (moisture, oxygen due to cellulose degradation).

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2 Large Pad Mounted Transformers

Pad Mounted transformers typically employ sealed tank construction and are liquid filled, with mineral insulating oil being the predominant liquid. For the purposes of this report, the padmounted transformer has been componentized into the transformer itself and the enclosure. Large Pad Mounted Transformers are Pad Mounted Transformers greater than 700 kVA.

2.1 Degradation Mechanism

It has been demonstrated that the life of the transformer's internal insulation is related to temperature-rise and duration. Therefore, transformer life is affected by electrical loading profiles and length of service life. Other factors such as mechanical damage, exposure to corrosive salts, and voltage and current surges also have a strong effect. Therefore, a combination of condition, age and load based criteria is commonly used to determine the useful remaining life of distribution transformers.

The impacts of loading profiles, load growth, and ambient temperature on asset condition, loss-of-life, and life expectancy can be assessed using methods outlined in ANSI\IEEE Loading Guides. This also provides an initial baseline for the size of transformer that should be selected for a given number and type of customers to obtain optimal life.

Visual inspections provide considerable information on transformer asset condition. Leaks, cracked bushings, and rusting of tanks can all be established by visual inspections. Transformer oil testing can be employed for distribution transformers to assess the condition of solid and liquid insulation.

Distribution transformers sometimes need to be replaced because of customer load growth. A decision is then required whether to keep the transformer as spare or to scrap it. Many utilities make this decision through a cost benefit analysis, by taking into consideration anticipated remaining life of transformer, cost of equivalent sized new transformer, labor cost for transformer replacement and rated losses of the older transformer in comparison to the newer designs.

The following factors are considered in developing the Health Index for distribution transformers:

- Tank corrosion, condition of paint
- Extent of oil leaks
- Condition of bushings
- Condition of padlocks, warning signs etc
- Transformer operating age and winding temperature profile
- Loading profile

The consequences of distribution transformer failure are relatively minor. This is why most utilities run their residential-service distribution transformers to failure. However, larger distribution transformers supplying commercial or industrial customers, where reduction in reliability impacts could be high, may be replaced as they reach near the end of life (EOL) before actual failure. The average transformer life is expected to be approximately 40 years.

2.2 Health Index Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m} \times WCP_{m})}{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m.\max} \times WCP_{m})} \times DF$$

where

$$CPS = \frac{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n} \times WCPF_{n} \right)}{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n.max} \times WCPF_{n} \right)} \times 4$$

CPS --- Condition Parameter Score

WCP --- Weight of Condition Parameter

DF --- De-rating Factor

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_m --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

2.3 Condition and Sub-Condition Parameters

Table 2-1 Condition Weights and Maximum CPS

M	Condition parameter	WCP _m	CPS _{m.max}
1	Insulation	4	4
2	Sealing & Connection	1	4
3	Service Record	3	4

Table 2-2 Insulation (m=1) Weights and Maximum CPF

N	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Oil Quality	4	4
2	Oil DGA	5	4

2.3.1 *Oil Quality*

Table 2-3 Oil Quality Test

Condition Rating	CPF	Description
Α	4	Overall factor is less than 1.2
В	3	Overall factor between 1.2 and 1.5
С	2	Overall factor is between 1.5 and 2.0
D	1	Overall factor is between 2.0 and 3.0
E	0	Overall factor is greater than 3.0

Where the Overall factor is the weighted average of the following gas scores:

Table 2-4 Oil Quality Overall Factoring

		Scores					
		1	2	3	4	Weight	
Diele	ctric Str. kV D877	>40	>30	>20	Less than 20	3	
	230 kV ≤ U	>32	25-32	20-25	Less than 20	2 *	
IFT* dynes/cm	69 kV <u< 230<="" td=""><td>>30</td><td>23-30</td><td>18-23</td><td>Less than 18</td><td>2</td></u<>	>30	23-30	18-23	Less than 18	2	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	U ≤ 69 kV	>25	20-25	15-20	Less than 15		
	Color	Less than 1.5	1.5-2	2-2.5	> 2.5	2	
	230 kV ≤U	Less than 0.03	0.03-0.07	0.07- 0.1	>0.1		
Acid Number*	69 kV <u< 230<="" td=""><td>Less than 0.04</td><td>0.04-0.1</td><td>0.1- 0.15</td><td>>0.15</td><td></td></u<>	Less than 0.04	0.04-0.1	0.1- 0.15	>0.15		
	U ≤ 69 kV	Less than 0.05	0.05-0.1	0.1- 0.2	>0.2	1 *	

^{*} Select the row applicable to the equipment rating

$$\text{Overall Factor} = \frac{\sum Score_i \times Weight_i}{\sum Weight}$$

2.3.2 Oil Dissolved Gas Analysis (DGA)

Table 2-5 Transformer DGA

Condition Rating*	CPF	Description	
Α	4	DGA overall factor is less than 1.2	
В	3	DGA overall factor between 1.2 and 1.5	
С	2	DGA overall factor is between 1.5 and 2.0	
D	1	DGA overall factor is between 2.0 and 3.0	
E	0	DGA overall factor is greater than 3.0	

*In the case of a score other than A, check the variation rate of DGA parameters. If the maximum variation rate (among all the parameters) is greater than 30% for the latest 3 samplings or 20% for the latest 5 samplings, overall Health Index is multiplied by 0.9 for score B, 0.85 for score C, 0.75 for score D and 0.5 for score E.

Where the DGA overall factor is the weighted average of the following gas scores:

Scores 1 2 3 4 5 6 Weight H2 <=100 <=200 <=300 <=500 <=700 >700 2 CH4(Methane) <=120 <=150 <=200 <=400 <=600 >600 3 C2H6(Ethane) <=65 <=100 <=150 <=250 <=500 >500 3 3 C2H4(Ethylene) <=50 <=80 <=150 <=250 <=500 >500 C2H2(Acetylene) <=3 <=7 <=35 <=50 <=80 >80 5 CO <=350 <=700 <=900 <=1100 <=1300 >1300 1 CO2 <=2500 <=3000 <=4000 <=4500 <=5000 >5000 1

Table 2-6 Oil DGA Overall Factoring

$$\text{Overall Factor} = \frac{\sum Score_i \times Weight_i}{\sum Weight}$$

Table 2-7 Sealing & Connection (m=2) Weights and Maximum CPF

N	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Tank Oil Leak	1	4
2	Conservator Oil Level	1	4

Table 2-8 Service Record (m=3) Weights and Maximum CPF

N	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Age	1	4

2.3.3 *Age*

The age used was based on the manufacture date on the name plate of the transformer.

Table 2-9 Transformer Age

Condition Rating	CPF	Description
Α	4	0-19
В	3	20-29
С	2	30-44
D	1	45-54
E	0	>=55

2.4 Health Index Results

The total population of assets for this category is 56. The Sample Size or total number of assets within the population that have data is 51.

The Health Indexing Result by Unit and Percentage are presented below:

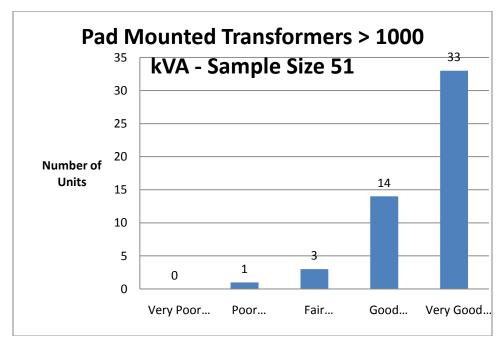


Figure 2-1 Health Index Distribution by Units

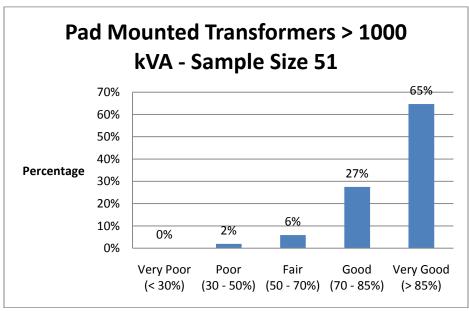


Figure 2-2 Health Index Distribution by Percentage

The exact rating for each Transformer is presented below:

Table 2-10 Pad Mounted Transformer Health Index Score

Transformer	Substation Name	HI	
No	Substation Name	Score	HI Rating
800135		50%	POOR
	SMITHVILLE 85	60%	FAIR
800105		63%	FAIR
732	FROST ROAD	69%	FAIR
2529		75%	GOOD
800515	DOUBLE TREE	75%	GOOD
800109		78%	GOOD
	NO NAMEPLATE	80%	GOOD
800554		81%	GOOD
800129	STATION 52	81%	GOOD
800128	STATION 52	81%	GOOD
800197		81%	GOOD
800148	HEDGSON	81%	GOOD
800127	DAYS INN FALLVIEW	81%	GOOD
800210	MANSIONS OF FOREST GLEN	81%	GOOD
800116	BUCKLEY TOWER	81%	GOOD
800126		84%	GOOD
77045	INDUSTRIAL PARK	86%	VERY GOOD
800526	DAYS INN VICTORIA AVE	86%	VERY GOOD
494	HILLSIDE DRIVE (5050)	86%	VERY GOOD
3040	SOUTH SERVICE RD	88%	VERY GOOD
800413	SUPER 8	90%	VERY GOOD
9201	BARTLETT ROAD (4306)	91%	VERY GOOD
3176	4927 ONTARIO ST.	91%	VERY GOOD
1652	SECOND AVE	93%	VERY GOOD
800568		93%	VERY GOOD
800546	NF COMM CENTRE	93%	VERY GOOD
800587		93%	VERY GOOD
800430	SWAGELOK	100%	VERY GOOD
800465		100%	VERY GOOD
301	4655 BARTLETT	100%	VERY GOOD
546	4927 ONTARIO ST.	100%	VERY GOOD
800550	NIAGARA REGION	100%	VERY GOOD
800601		100%	VERY GOOD
599	ONTARIO ST (SOBEYS)	100%	VERY GOOD
800589		100%	VERY GOOD
73201	PEARSON STREET	100%	VERY GOOD

81	FROST ROAD	100%	VERY GOOD
8099	4758 CHRISTIE ST.	100%	VERY GOOD
629	TWENTY THIRD ST	100%	VERY GOOD
800414	TGI FRIDAYS	100%	VERY GOOD
202	JORDAN ROAD	100%	VERY GOOD
800532		100%	VERY GOOD
800585		100%	VERY GOOD
800443	NPE BUILDING	100%	VERY GOOD
83005	REGIONAL ROAD 20 EAST	100%	VERY GOOD
800586		100%	VERY GOOD
800490	GOLDEN HORSESHOE	100%	VERY GOOD
800584		100%	VERY GOOD
800588		100%	VERY GOOD
99121	NORTH SERVICE RD	NO DATA	
800147	EVENTIDE HOME	NO DATA	
229	DURHAM ROAD		NO DATA

2.5 Field Inspection Results

Field inspections were only done on Standard Pad Mounted Transformers.

2.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 25 years the probability of failure is 10% and at age of 45 years the probability of failure is 90%.

2.6.1 Optimal Capital Replacement Plan

Figure 2-3 shows the number of Transformer units that will need to be replaced over the next 20 years for the whole population extrapolated from the results for the sample with adequate condition data. Given a significant sample size (93%) there is a high degree of confidence that the recommendations for the sample and the whole population are the same.

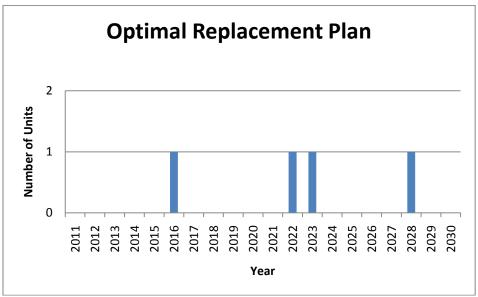


Figure 2-3 Optimal Replacement Plan

2.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing no units in the next 5 years. There are no peaks in replacement years.

Large Pad Transformers are replaced **proactively**. The Levelized replacement plan allows for Transformers that would optimally be replaced in one year to be replaced over a period of time.

Figure 2-4 shows a Levelized capital replacement plan, where transformer replacements can occur over a longer period of time, it is the same as the optimal replacement plan.

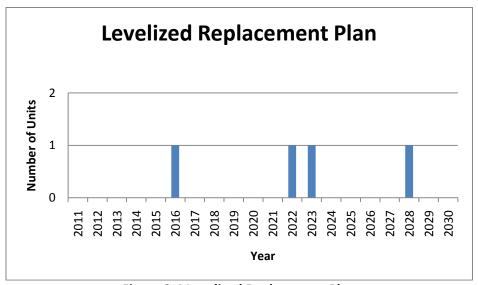


Figure 2-4 Levelized Replacement Plan

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2.7 Data Gap Closure

The following table summarizes the data gap for large pad mounted transformers in this project.

Sub-system	Condition	Data Collection Priority
Sealing & connection	Grounding	☆
	IR thermography	* * *
Service record	Loading	* *
	Age	**

IR thermography is a useful approach in detecting hot spots due to a loose connection or leakage. In this project, it also can address the transformer loading status, when the data on such parameter are unavailable.

Niagara Peninsula Energy Inc Distribution Asset Condition Assessment	2 - Large Pad Mounted Transformers
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3 Standard Pad-Mounted Transformers

Pad Mounted transformers typically employ sealed tank construction and are liquid filled, with mineral insulating oil being the predominant liquid. For the purposes of this report, the padmounted transformer has been componentized into the transformer itself and the enclosure. Standard Pad Mounted Transformers are smaller than 750 kVA.

3.1 Degradation Mechanism

It has been demonstrated that the life of the transformer's internal insulation is related to temperature-rise and duration. Therefore, transformer life is affected by electrical loading profiles and length of service life. Other factors such as mechanical damage, exposure to corrosive salts, and voltage and current surges also have a strong effect. Therefore, a combination of condition, age and load based criteria is commonly used to determine the useful remaining life of distribution transformers.

The impacts of loading profiles, load growth, and ambient temperature on asset condition, loss-of-life, and life expectancy can be assessed using methods outlined in ANSI\IEEE Loading Guides. This also provides an initial baseline for the size of transformer that should be selected for a given number and type of customers to obtain optimal life.

Visual inspections provide considerable information on transformer asset condition. Leaks, cracked bushings, and rusting of tanks can all be established by visual inspections. Transformer oil testing can be employed for distribution transformers to assess the condition of solid and liquid insulation.

Distribution transformers sometimes need to be replaced because of customer load growth. A decision is then required whether to keep the transformer as spare or to scrap it. Many utilities make this decision through a cost benefit analysis, by taking into consideration anticipated remaining life of transformer, cost of equivalent sized new transformer, labor cost for transformer replacement and rated losses of the older transformer in comparison to the newer designs.

The following factors are considered in developing the Health Index for distribution transformers:

- Tank corrosion, condition of paint
- Extent of oil leaks
- Condition of bushings
- Condition of padlocks, warning signs etc
- Transformer operating age and winding temperature profile
- Loading profile

The consequences of distribution transformer failure are relatively minor. This is why most utilities run their residential-service distribution transformers to failure. However, larger distribution transformers supplying commercial or industrial customers, where reduction in reliability impacts could be high, may be replaced as they reach near the end of life (EOL) before actual failure. The average transformer life is expected to be approximately 40 years.

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3.2 Health Index Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_m (CPS_m \times WCP_m)}{\sum_{m=1}^{\infty} \alpha_m (CPS_{m.\max} \times WCP_m)}$$

where

$$CPS = \frac{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n} \times WCPF_{n} \right)}{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n.max} \times WCPF_{n} \right)} \times 4$$

CPS --- Condition Parameter Score

WCP --- Weight of Condition Parameter

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_m --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

3.3 Condition and Sub-Condition Parameters

Standard Pad Mounted Transformers that are base type **Collar** are **de-rated** to **30%** of the calculated Health Index Value.

Table 3-1 Condition Weights and Maximum CPS

m	Condition Parameter	WCP _m	CPS _{m.max}
1	Physical condition	3	4
2	Connection & insulation	5	4
3	Service record	5	4
4	Testing	10	4

Table 3-2 Physical Condition (m=1) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Access (ok/not ok)	1	4

Table 3-3 Connection & insulation (m=2) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Oil contamination (ok/not ok)	2	4
2	Grounding	1	4
3	Insulator (ok/not ok)	4	4
4	Enclosure	1	4

Table 3-4 Testing (m=3) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	IR Scan (Pass/Fail)	1	4
2	Ultra Sound (Pass/Fail)	1	4

3.3.1 *Enclosure*

Table 3-5 Enclosure Rating Score ENCLOSURE

Condition Rating	CPF	Condition Description	
Α	4	Good	
В	3	Graffiti	
С	2	Needs Repainting	
D	0	Rusting	
E	0	Rusting and Graffiti	
F	0	Rusting and Needs Repairs	
G	0	Rusting and Needs Repainting	

3.3.2 *Grounding*

Table 3-6 Grounding Rating Score GROUNDING

Condition Rating	CPF	Condition Description	
Α	4	6	
Α	4	4	
Α	4	3	
Α	4	2	
E	0	1	
E	0	Other	

Table 3-7 Service Record (m=3) Weights and Maximum CPF

N	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Inspection result	2	4
2	Age	1	4

3.3.3 *Age*

Table 3-8 Age Rating Score

Age			
Condition Rating	Description	CPF	
Α	0	4	
В	24	3	
С	30	2	
E	40	0	

3.4 Health Index Results

The total population of assets for this category is 2408. The Sample Size or total number of assets within the population that have data other than age is 716.

The Health Indexing Result by Unit and Percentage are presented below for both the population of 716 (age and other data):

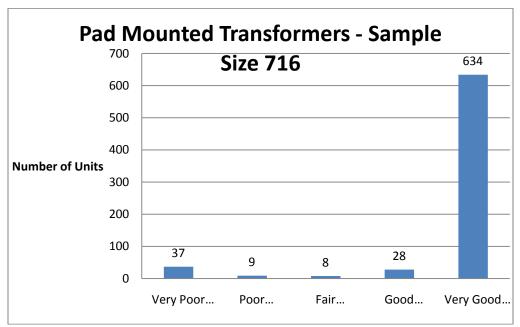


Figure 3-1 Health Index Distribution by Unit

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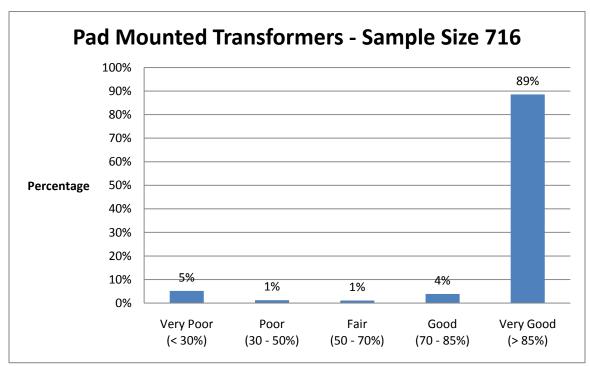


Figure 3-2 Health Index Distribution by Percentage

3.5 Field Inspection Results

Five Standard Pad Mounted Transformers were inspected. The data can be found in Section E FIELD INSPECTION FORMS and the summary is shown in Figure 3-3 below. Most of the units were in good to fair condition. The unit in poor condition was rated this way because of Pad Condition, Main Cabinet Condition and Overall Condition.

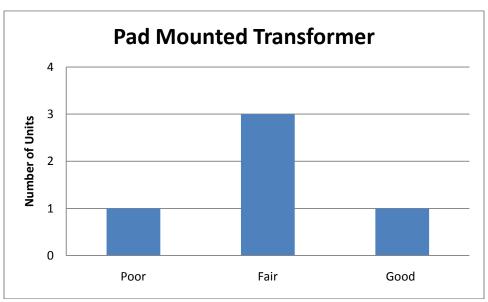


Figure 3-3 Field Inspection Results

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The field inspection data indicates a different pattern than the sample case. This may be because only 30% of NPEI's were included in the Health Index sample (716 units) that may not represent NPEI's total population's Health Index.

3.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 25 years the probability of failure is 10% and at age of 45 years the probability of failure is 90%.

3.6.1 Optimal Replacement Plan

Figure 3-4 the number of Transformer units that will need to be replaced over the next 20 years. The result was extrapolated from the 28% sample with more than just condition data available to the whole population. Since Health Index distribution based on age alone that was available for the whole population is similar to the sample's Health Index distribution, it appears that the sample was representative of the whole population.

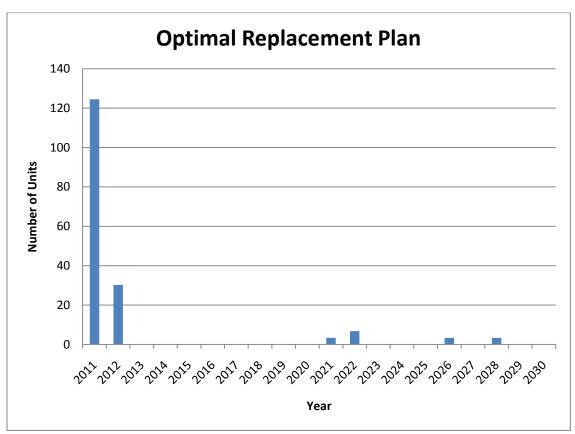


Figure 3-4 Optimal Replacement Plan

3.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing 124 units in the next year. While this is optimal based on NPEI's Pad Mounted Transformers HI scores, it may not be ideal financially.

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Standard Pad Transformers are typically replaced reactively (end of life.) However NPEI is replacing those transformers with collar type bases **proactively**. The Levelized replacement plan allows for Transformers that would optimally be replaced in one year to be replaced over a period of 5 years.

Figure 3-5 shows a Levelized capital replacement plan, where transformer replacements can occur over a longer period of time.

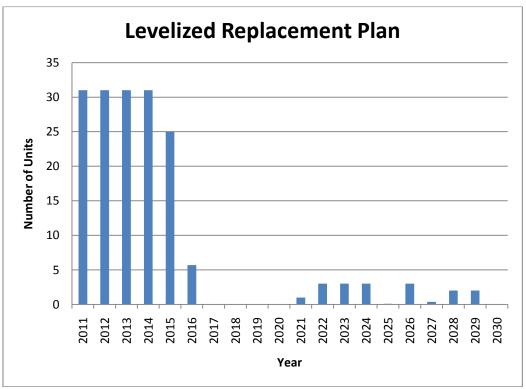


Figure 3-5 Levelized Replacement Plan

3.7 Data Gap Closure

The same information that has been collected for the sample needs to be collected for the remaining population.

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4 Pole-Mounted Transformers

Distribution pole top transformers change sub-transmission or primary distribution voltages to 120/240 V or other common voltages for use in residential and commercial applications.

4.1 Degradation Mechanism

It has been demonstrated that the life of the transformer's internal insulation is related to temperature-rise and duration. Therefore, transformer life is affected by electrical loading profiles and length of service life. Other factors such as mechanical damage, exposure to corrosive salts, and voltage and current surges also have a strong effect. Therefore, a combination of condition, age and load based criteria is commonly used to determine the useful remaining life of distribution transformers.

The impacts of loading profiles, load growth, and ambient temperature on asset condition, loss-of-life, and life expectancy can be assessed using methods outlined in ANSI\IEEE Loading Guides. This also provides an initial baseline for the size of transformer that should be selected for a given number and type of customers to obtain optimal life.

Visual inspections provide considerable information on transformer asset condition. Leaks, cracked bushings, and rusting of tanks can all be established by visual inspections. Transformer oil testing can be employed for distribution transformers to assess the condition of solid and liquid insulation.

Distribution transformers sometimes need to be replaced because of customer load growth. A decision is then required whether to keep the transformer as spare or to scrap it. Many utilities make this decision through a cost benefit analysis, by taking into consideration anticipated remaining life of transformer, cost of equivalent sized new transformer, labor cost for transformer replacement and rated losses of the older transformer in comparison to the newer designs.

The following factors are considered in developing the Health Index for distribution transformers:

- Tank corrosion, condition of paint
- Extent of oil leaks
- Condition of bushings
- Transformer operating age and winding temperature profile
- Loading profile

The consequences of distribution transformer failure are relatively minor. This is why most utilities run their residential-service distribution transformers to failure. However, larger distribution transformers supplying commercial or industrial customers, where reduction in reliability impacts could be high, may be replaced as they reach near the end of life (EOL) before actual failure. The average transformer life is expected to be approximately 40 years.

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4.2 Health Index Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_m (CPS_m \times WCP_m)}{\sum_{m=1}^{\infty} \alpha_m (CPS_{m.\max} \times WCP_m)}$$

where

$$CPS = \frac{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n} \times WCPF_{n} \right)}{\sum_{n=1}^{n} \beta_{n} \left(CPF_{n.max} \times WCPF_{n} \right)} \times 4$$

CPS --- Condition Parameter Score

WCP --- Weight of Condition Parameter

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_{m} --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

4.3 Condition and Sub-Condition Parameters

Table 4-1 Condition Weights and Maximum CPS

m	Condition Parameter	WCP _m	CPS _{m.max}
1	Operating Practices	2	4
2	Service record	1	4

Table 4-2 Operating Practices (m=1) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Operating Practices	1	4

4.3.1 *Operating Practices*

Table 4-3 Customer Score Rating

CUSTOMERS		
Condition Rating	Description	CPF
А	0	4
В	10	3
С	20	2
E	40	0

Table 4-4 Service Record (m=2) Weights and Maximum CPF

N	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Age	1	4

4.3.2 *Age*

Table 4-5 Age Score Rating

Age			
Condition Rating	Description	CPF	
А	0	4	
В	24	3	
С	30	2	
E	40	0	

4.4 Health Index Results

The total population of assets for this category is 6835. The Sample Size or total number of assets within the population that have data is 6711.

The year purchased was assumed to the transformers age. The other condition parameter was the number of customers serviced by the transformer.

The Health Indexing Result by Unit and Percentage are presented below:

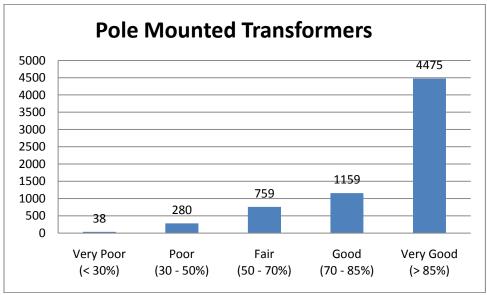


Figure 4-1 Health Index Distribution by Unit

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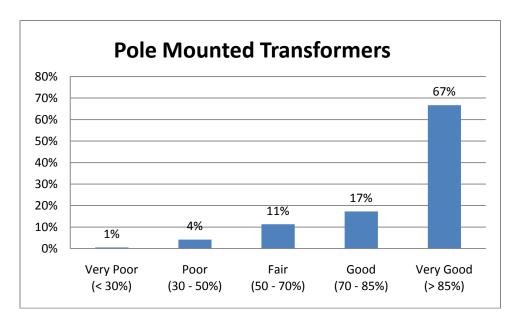


Figure 4-2 Health Index Distribution by Percentage

4.5 Field Inspection Results

Two Pole Mounted Transformers were inspected. The data can be found in Section E FIELD INSPECTION FORMS and are summarized in Figure 4-3 below. The units were in good and fair condition.

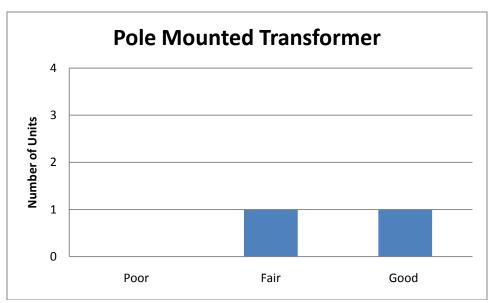


Figure 4-3 Field Inspection Results

4.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 30 years the probability of failure is 10% and at age of 60 years the probability of failure is 90%.

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4.6.1 Optimal Replacement Plan

Figure 4-4 shows the number of Transformer units that will need to be replaced over the next 20 years for the whole population extrapolated from the results for the sample with adequate condition data. Given a significant sample size (98%) there is a high degree of confidence that the recommendations for the sample and the whole population are the same.

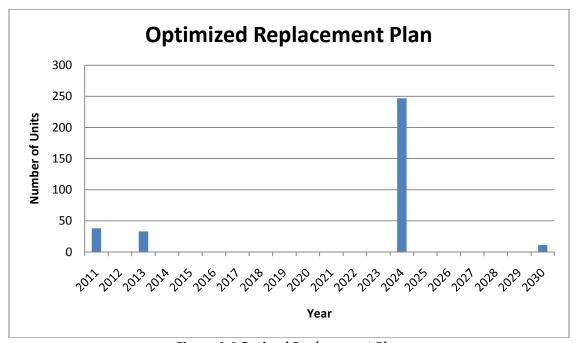


Figure 4-4 Optimal Replacement Plan

4.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing 247 units in 2024. While this is optimal based on NPEI's Pole Mounted Transformers HI scores, it may not be ideal financially.

Pole Mounted Transformers are typically replaced **reactively** (end of life.) Since the HI scores indicate the majority of failures happening over the next 25 years, NPEI can take a Levelized approach by replacing assets before they are estimated to fail. The Levelized replacement plan allows for Transformers that would optimally be replaced in 2024 year to be replaced over a period of 5 years (2020-2024).

Figure 4-5 shows a Levelized capital replacement plan, where transformer replacements can occur over a longer period of time.

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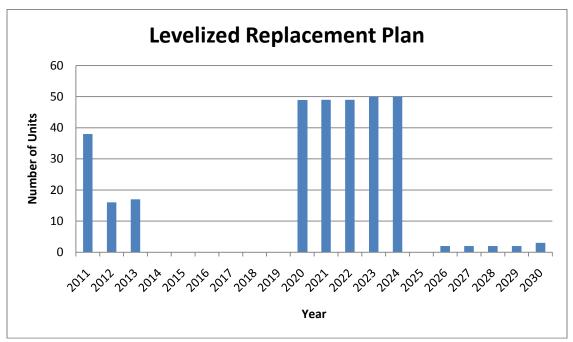


Figure 4-5 Levelized Replacement Plan

4.7 Data Gap Closure

The following table summarizes the data gap for pole mounted transformers in this project.

Sub-system	Condition Parameter	Data Collection Priority
Physical condition	Corrosion	冷冷
Connection & insulation	Oil leak	* *
Service record	Loading	**

As a pole mounted transformer is a run-to-failure asset, its service record has much impact on its life cycle. While corrosion and oil leak provide visual inspection on the external signs of degradation, its loading history can be used to estimate its actual aging process.

5 Poles

The asset referred to in this category is the fully dressed pole ranging in size from 30 to 75 feet. This includes the pole, cross arm, bracket, insulator, and anchor & guys. The most important component with respect to useful life is the pole itself.

5.1 Degradation Mechanism

As wood is a natural material the degradation processes are somewhat different to those which affect other physical assets on the electricity distribution systems. The critical processes are biological involving naturally occurring fungi that attack and degrade wood, resulting in decay. The nature and severity of the degradation depends both on the type of wood and the environment. Some fungi attack the external surfaces of the pole and some the internal heartwood. Therefore, the mode of degradation can be split into either external rot or internal rot.

As a structural item the sole concern when assessing the condition for a wood pole is the reduction in mechanical strength due to degradation or damage. A particular problem when assessing wood poles is the potentially large variation in their original mechanical properties. Depending on the species the mechanical strength of a new wood pole can vary greatly. Typically the first standard deviation has a width of $\pm 15\%$ for poles nominally in the same class. However in some test programs the minimum measured strength has been as low as 50% of the average.

Assessment techniques start with simple visual inspection of poles. This is often accompanied by basic physical tests, such as prodding tests and hammer tests to detect evidence of internal decay. Over the past 20 years, electricity companies have sought more objective and accurate means of determining condition and estimating remaining life. This has led to the development of a wide range of condition assessment and diagnostic tools and techniques for wood poles. These include techniques that are designed to apply the traditional probing or hammer tests in a more controlled, repeatable and objective manner. Devices are available that measure the resistance of a pin fired into the pole to determine the severity of external rot and instrumented hammers that record and analyze the vibration caused by a hammer blow to identify patterns that indicate the presence of decay. Direct assessment of condition by using a decay resistance drill or an auger to extract a sample through the pole, are also widely used. Indirect techniques, ultrasonic, X-rays, electrical resistance measurement have also been widely used.

There are many factors considered by utilities when establishing condition of wood poles. These include types of wood, historic rates of decay and average lifetimes, environment, perceived effectiveness of available techniques and cost. However, perhaps the most significant is the policy of routine line inspections. A foot patrol of overhead lines undertaken on a regular cycle is extremely effective in addressing the safety and security obligations.

The life expectancy of wood poles ranges from 40 to 80 years, with 60 years being the mean. Consequences of an in-service pole failure are quite serious, as they could lead to a serious accident involving the public. Depending on the number of circuits supported, a pole failure may also lead to a power interruption for a significant number of customers.

5.2 Health Index Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m} \times WCP_{m})}{\sum_{m=1}^{\infty} \alpha_{m} (CPS_{m.\max} \times WCP_{m})} \times DF$$

where

$$CPS = \frac{\displaystyle\sum_{n=1}^{n} \beta_{n} \left(CPF_{n} \times WCPF_{n} \right)}{\displaystyle\sum_{n=1}^{n} \beta_{n} \left(CPF_{n.max} \times WCPF_{n} \right)} \times 4$$

CPS --- Condition Parameter Score

WCP --- Weight of Condition Parameter

DF --- De-rating Factor

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_m --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

5.3 Condition and Sub-Condition Parameters

Those Poles that are **Red Cedar Butt Treated** have been **de-rated** to 80% of their calculated Health Index Value.

Table 5-1 Condition Weights and Maximum CPS

m	Condition parameter	WCP _m	CPS _{m.max}
1	Pole physical	3	4
2	Pole accessories	1	4
3	Overall	4	4

Table 5-2 Pole Physical (m=2) Weights and Maximum CPF

n	Sub-condition parameter	WCPF _n	CPF _{n.max}
1	Animal Damage	2	4
2	Lean	1	4
3	Rot / Soft	2	4
4	Crack	2	4
5	Hole / Void	2	4
6	Hollow	2	4
7	Chunk	2	4
8	Damp / Wet	2	4
9	Bend / Hit / Damage	2	4
10	Poor Top	2	4

Table 5-3 Pole Accessory (m=3) Weights and Maximum CPF

N	Sub-condition parameter	CPF lookup table	WCPF _n	CPF _{n.max}
2	Guy Wire	OK = 4; All others = 0	3	4
3	Defective Ground	OK=4; Exposed/connection issue/rod above grade= 2; Damaged = 0	2	4
4	Crossarm	OK=4; Crooked/Loose = 2; Damaged = 0	1	4
5	Riser (Cable Guard)	OK=4; Exposed/Loose = 2; Damaged = 0	1	4

Table 5-4 Overall (m=4) Weights and Maximum CPF

N	Sub-condition parameter	WCPF _n	CPF _{n.max}
1	Overall	3	4
3	Age	2	4

5.3.1 *Age*

Table 5-5 Pole Age

Condition Rating	CPF	Condition Description
А	4	0
В	3	10
С	2	25
D	1	40
Е	0	>50

5.4 Health Index Results

The total population of assets for this category is 22,247. The Sample Size or total number of assets within the population that have data is 5985. However those pole recently inspected were of newer vintage. Age was provided for 13,135 units (encompassing the 4943 units of the 5985 sample) so a comparison of the age range of the sample, as compared to the 13,135 population was done.

The Health Indexing Result by Unit and Percentage and the age range comparison of the sample to a broader sample of the pole population are presented below:

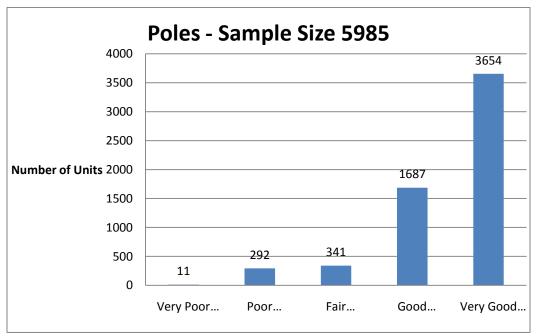


Figure 5-1 Health Index Distribution by Unit

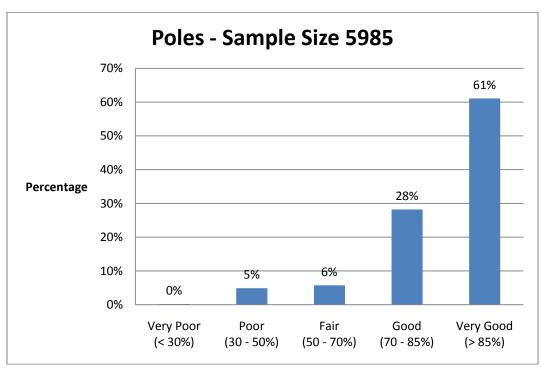


Figure 5-2 Health Index Distribution by Percentage

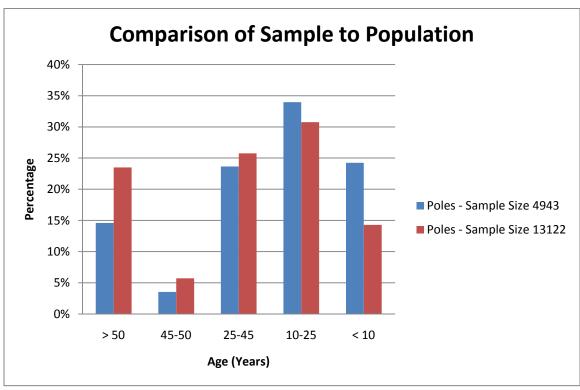


Figure 5-3 Comparison of Sample Age Data to a Larger Sample of the Population Age Data

5.5 Field Inspection Results

Four Poles were inspected. The data can be found in Section E FIELD INSPECTION FORMS and are summarized in Figure 5-4 below. The units were in good and fair condition.

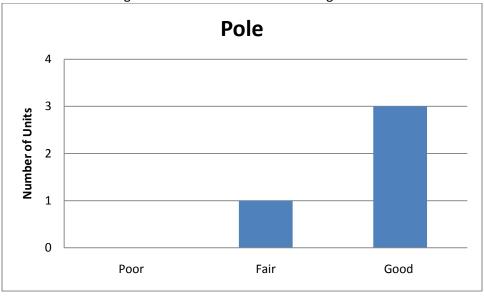


Figure 5-4 Field Inspection Results

5.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 40 years the probability of failure is 10% and at age of 60 years the probability of failure is 90%.

5.6.1 Optimal Capital Replacement Plan

Figure 5-5 shows the number of Poles that will need to be replaced over the next 20 years extrapolated for the whole population from the sample (27% of the population) with adequate condition data. However, it could be seen from Figure 5-3 that the overall condition of the poles in the sample is better than that for the population with only age available due to the investments made in testing and replacing poles found to be in poor condition. Therefore, to achieve similar Health Index distribution for the whole population more capital expenditures than what is shown would be required.

A separate analysis which is beyond the scope of this project would be required to estimate the incremental capital amount needed to improve overall condition of the whole pole population to the level of the poles in the sample with adequate condition data.

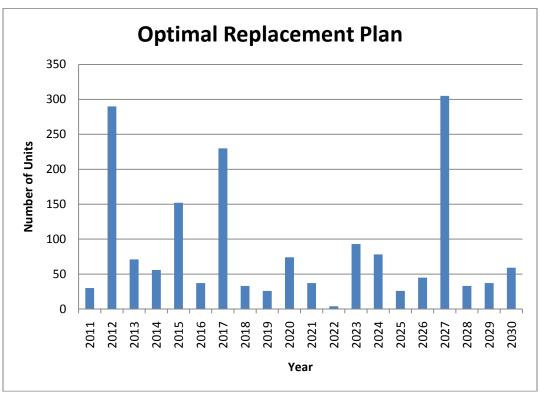


Figure 5-5 Optimal Replacement Plan

5.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing 30 units next year. While this is optimal based on NPEI's Pole HI scores, it may not be ideal financially.

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Poles are typically replaced **reactively** (end of life.) Since the HI scores indicate the majority of failures happening in spikes over the next 30 years, NPEI can take a Levelized approach by replacing assets before they are estimated to fail.

Figure 5-6 shows a Levelized capital replacement plan, where replacements pole can occur over a longer period of time.

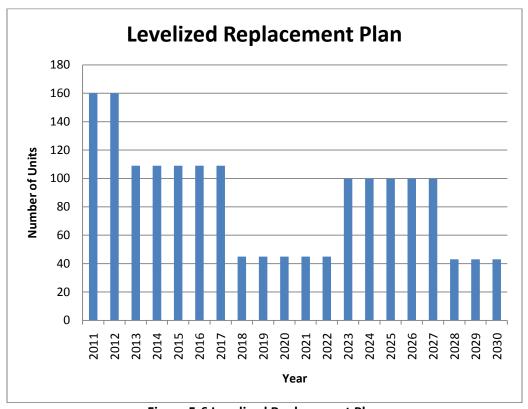


Figure 5-6 Levelized Replacement Plan

5.7 Data Gap Closure

The only data gap for poles in this project is the measured pole strength. It represents the actual physical size changes due to pole degradation. It is useful in scheduling reinforcement or replacement.

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6 Pad Mounted Switchgear

This asset class consists of pad mounted switchgear. The primary function of switches is to allow for isolation of line sections or equipment for maintenance, safety or other operating requirements.

6.1 Degradation Mechanism

The main degradation processes associated with line switches include:

- Corrosion of steel hardware or operating rod
- Mechanical deterioration of linkages
- Switch blades falling out of alignment, which may result in excessive arcing during operation
- Loose connections
- Insulator damage
- Non-functioning padlocks
- Missing ground connections

The rate and severity of these degradation processes depends on a number of inter-related factors including the operating duties and environment in which the equipment is installed. In most cases, corrosion or rust represents a critical degradation process. The rate of deterioration depends heavily on environmental conditions where the equipment operates.

Corrosion typically occurs around the mechanical linkages of these switches. Corrosion can cause seizing. While a lesser mode of degradation, air pollution also can affect support insulators. Typically, this occurs in heavy industrial areas or where road salt is used.

6.2 Formulation

Recommended Health Index Formulations:

$$HI = \frac{\sum_{m=1}^{\infty} \alpha_m (CPS_m \times WCP_m)}{\sum_{m=1}^{\infty} \alpha_m (CPS_{m.\max} \times WCP_m)}$$

where

$$CPS = \frac{\sum_{n=1}^{n} \beta_n (CPF_n \times WCPF_n)}{\sum_{n=1}^{n} \beta_n (CPF_{n.max} \times WCPF_n)} \times 4$$

CPS --- Condition Parameter Score
WCP --- Weight of Condition Parameter

CPF --- Sub-Condition Parameter Factor

WCPF --- Weight of Condition Parameter Factor

 α_m --- Data availability coefficient for condition parameter (=1 when data available, =0 when data unavailable)

 β_n --- Data availability coefficient for condition factor (=1 when data available, =0 when data unavailable)

6.3 Condition and Sub-Condition Parameters

Switchgear that is **Air Insulated** and near a **major roadway** is **de-rated** to **30%** of the calculated Health Index Value.

Table 6-1 Condition Weights and Maximum CPS

m	Condition Parameter	WCP _m	CPS _{m.max}
1	Physical Condition	3	4
2	Switch Condition	5	4
3	Insulation	7	4
4	Service record	5	4
5	Testing	10	4

Table 6-2 Physical Condition (m=1) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Enclosure	3	4
2	Access (ok/not ok)	1	4
3	Base (ok/not ok)	2	4

Table 6-3 Switch/Fuse Condition (m=2) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Grounding	1	4

Table 6-4 Insulation (m=3) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Insulator (ok/not ok)	1	4

Table 6-5 Service Record (m=4) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	Inspection result (Pass/Fail)	1	4

Table 6-6 Tests (m=5) Weights and Maximum CPF

n	Sub-Condition Parameter	WCPF _n	CPF _{n.max}
1	IR Scan (Pass/Fail)	1	4
2	Ultrasonic (Pass/Fail)	1	4

6.4 Health Index Results

The total population of assets for this category is 89. The Sample Size or total number of assets within the population that have data is 38.

The Health Indexing Result by Unit and Percentage are presented below:

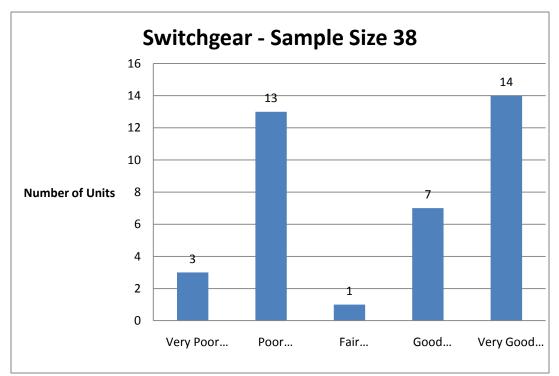


Figure 6-1 Health Index Distribution by Unit

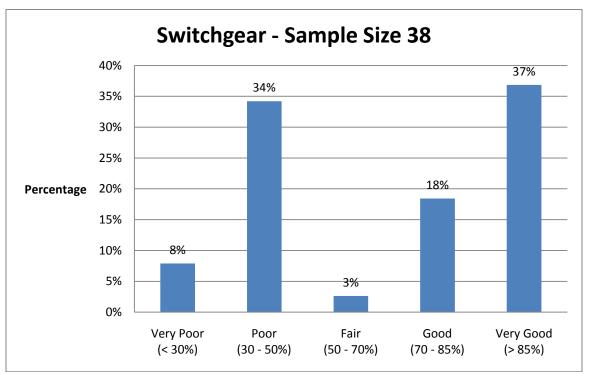


Figure 6-2 Health Index Distribution by Percentage

6.5 Field Inspection Results

On Pad Mounted Switchgear was inspected. The data can be found in Section E FIELD INSPECTION FORMS and are summarized in Figure 6-3 below.

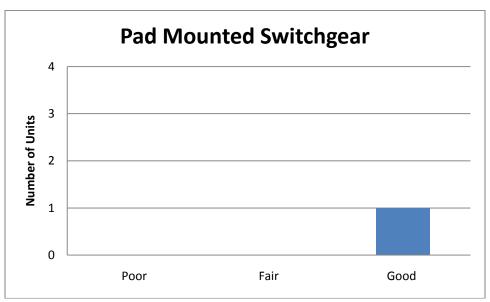


Figure 6-3 Field Inspection Results

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6.6 Capital Replacement Plan

For this asset category, the probability of failure curve was assumed such that at the age of 20 years the probability of failure is 10% and at age of 45 years the probability of failure is 90%.

6.6.1 Optimal Capital Replacement Plan

Figure 6-4 shows the number of Pad Mounted Switchgear units that will need to be replaced over the next 20 years extrapolated from the sample with adequate condition data (43%). There is no basis to confirm or deny whether this assumption is reasonable, so it is recommended to accelerate a process of collecting condition data for the reminder of the population.

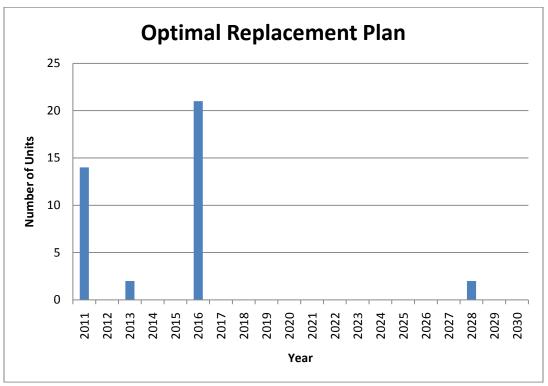


Figure 6-4 Optimal Replacement Plan

6.6.2 Levelized Capital Replacement Plan

For this asset category, the optimal replacement plan suggests replacing 14 units next year. While this is optimal based on NPEI's Pad Mounted Switchgear HI scores, it may not be ideal financially.

Standard Pad Transformers are typically replaced reactively (end of life.) However NPEI is replacing those transformers that are air insulated and near a major roadway **proactively**. The Levelized replacement plan allows for Switchgear that would optimally be replaced in one year to be replaced over a period of 5 years.

Figure 6-5 shows a Levelized capital replacement plan, where switchgear replacements can occur over a longer period of time.

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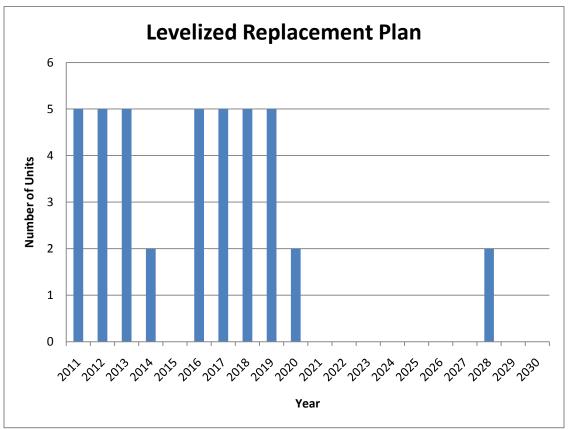


Figure 6-5 Levelized Replacement Plan

6.7 Data Gap Closure

The following table summarizes the data gap for pad mounted switchgear in this project.

Sub-system	Condition Parameter	Data Collection Priority
Physical condition	Debris/dirty	☆
Switch/fuse condition	Switch condition	* * *
	Arc chute	☆ ☆
Insulation	Barriers	* *
Service record	Age	☆

Switch main contact and its arc suppression parts are the main device inside pad mounted switchgear.

D CONCLUSIONS AND RECOMMENDATIONS

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D CONCLUSIONS AND RECOMMENDATIONS

Niagara Peninsula Energy Inc Distribution Asset Condition Assessment

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Conclusions and Recommendations

- 1. There was generally sufficient condition data available for Power Transformers, Large Padmounted Transformers, Poles (inspected after 2008) and Switchgear.
- 2. For Pole-mounted transformers, only age is available and operating practices (i.e., customers). Gathering and recording detailed inspection data should be considered.
- 3. For Standard Pad Mounted transformers, age was provided for 87% of the population however sufficient data was provided for only 28% of the population. It is recommended that NPEI collect data for a greater population of Pad Mounted Transformers.
- 4. For Poles that have not been inspected, age is only available for half of the population. Sufficient age and inspection data should be collected for the rest of the population.
- 5. Sufficient data was not available for Underground Cables. It is recommended that inspection and maintenance information be collected for these assets to enable future asset condition assessment.
- 6. A separate study is required to determine appropriate increase in the pole replacement program over the levels extrapolated from the sample with adequate condition data to achieve the desired overall Health Index distribution (similar to that of the sample).

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D CONCLUSIONS AND RECOMMENDATIONS

Niagara Peninsula Energy Inc Distribution Asset Condition Assessment

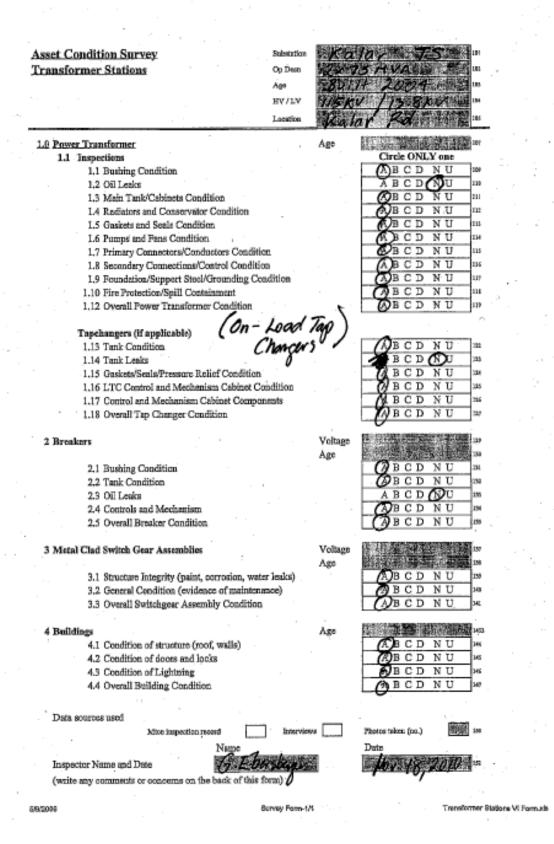
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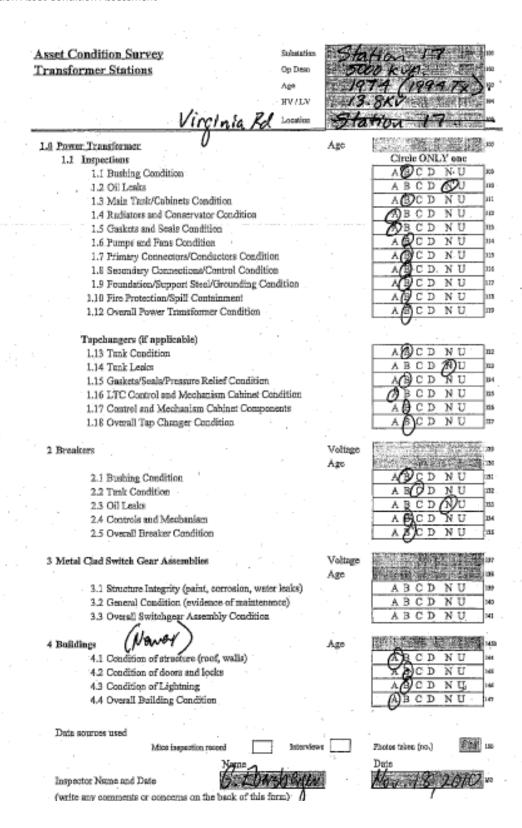
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E FIELD INSPECTION FORMS

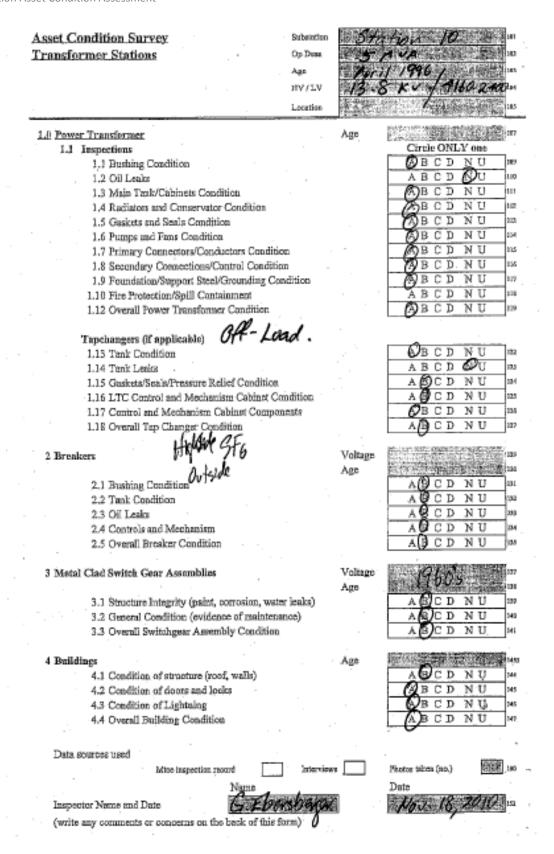
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	. Voltage	16 KV IN 15 KVA	
	Location	Various Handlast .	
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, 1.1 Main Cabinet Condition		ABCD NU 118	
1.2 Pad Condition		ABCD NU me	
1.3 insulators Condition		ABCDNU	
1.4 Contact Condition		ABCD NU 112	
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25 Cable Condition		ABCD NU III	
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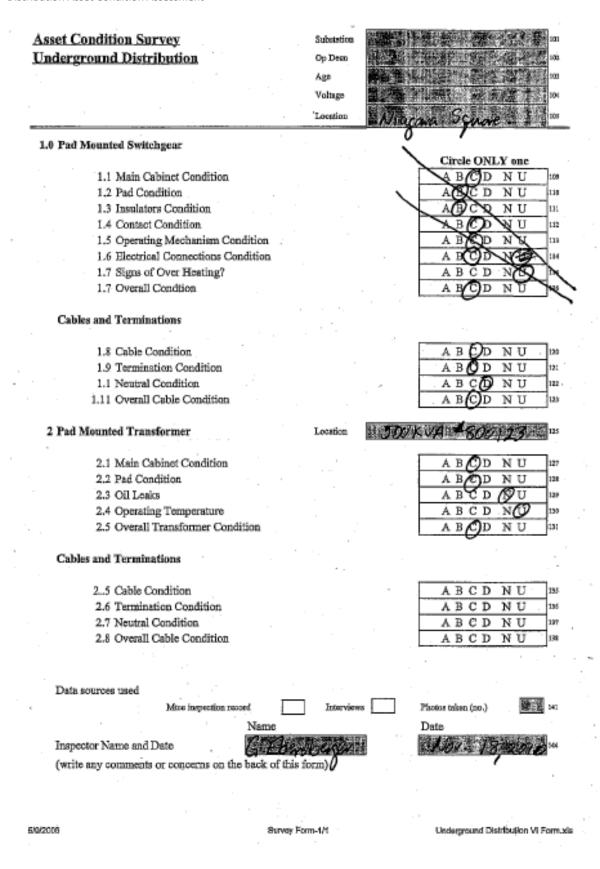
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Substitution Asset Condition Survey Op Desn Overhead Distribution Ago Voltage Location 1.6 Remotely Operated Pole Mounted Lead Break Switch Circle ONLY one ABCD NU NU ABCD 1.1 Insulator Condition NU 1.2 Mechanical Support Condition ABCD ABCD NU 1.3 Signs of Over Heating? NÜ A'B C D 1.4 Contact Condition 1,5 Operating Mechanism Condition ABCD NU 1.6 Motor Operator and Control Condition NU ABCD 1.7 Overall Condition Manually Operated Pole Mounted Load Break Switch NU ABCD NU 123 ABCD 1.1 Insulator Condition 722 1.2 Mechanical Support Condition NU ABCD 123 NU 1.3 Signs of Over Heating? ABCD 194 ABCD NU 1.4 Contact Condition 1.5 Operating Mechanism Condition ABCD ΝÜ 1.6 Overall Condition Location 3 Pole ΝÜ NU 1.1 Holes and Cracks ? C D 1.2 Ret 7 1.3 Cross arm Condition 1.4 Overall Pole Condition Location 3 Pole Mounted Transformer ABCD ΝÜ ΝU 127 ABCD 1.1 Tank Integrity 332 NU ABCD 1.2 Oil Leak 125 ABCD ΝU 1.3 Bushing Condition NU 1.4 Electrical Connections ABCD 1.5 Signs of Overheating? 1.6 Overall Transformer Condition Photos taken (no.) Data sources used Interviews Mixe inspection record Date Inspector Name and Date ments or concerns on the back of this form)

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Asset Condition Survey Underground Distribution	Substation Op Dess Age		10 mg
	Voltage	100 mm (100 mm)	NO.
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1.0 Pad Mounted Switchgear		Clark ON	
1.1 Main Cabinet Condition		Circle ON	
1.2 Pad Condition		ABCD	
1.3 Insulators Condition		ABCD	
1.4 Contact Condition		ABCD	
1.5 Operating Mechanism Condition		ABCD	
1.6 Electrical Connections Condition		ABCD	
1.7 Signs of Over Heating?		ABCD	-
1.7 Overall Condtion		ABCD	
			24 0
Cables and Terminations			
1.8 Cable Condition		ABCD	N U . 120
1.9 Termination Condition		ABCD	N U III
1.1 Neutral Condition		ABCD	N U 121
1.11 Oversill Cable Condition		ABCD	NU in
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2 Pad Mounted Transformer	Location	2. 15 · 传说是在	1965 T. 15 (2)
2.1 Main Cabinet Condition		ABCD	N U 127
2.2 Pad Condition		ABCD	N U 128
2.3 Oil Leaks		ABCD	N U 29
2.4 Operating Temperature		ABCD	N IJ 154
2.5 Overall Transformer Condition		ABCD	NUm
Cables and Terminations			
25 Cable Condition		A BCD	N U 115
2.6 Termination Condition		A/B/CD	N U . 125
2.7 Neutral Condition		A B € D	N U 137
2.8 Overall Cable Condition		A/B & D	NU ise
Data sources used			
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Inspector Name and Date	Test and assessment	Date	all the seconds.
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1.0 Remo	otely Operated Pole Mounted Load Break Sw				
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	1.2 Mechanical Support Condition			ABCD	N U III
	1.3 Signs of Over Heating?			ABCD	N U m
	1.4 Contact Condition			ABCD	N U 112
	1.5 Operating Mechanism Condition			ABCD	N U III
	1.6 Motor Operator and Control Condition	,		ABCD	N U . 114
	1.7 Overall Condition			ABCD	NU ns.
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2 Manu	sally Operated Pole Mounted Load Break Sw	itch .			
	1.1 Insulator Condition			(A)BCD	NU me.
	1.2 Mechanical Support Condition			A/B)C D	N U 20
	1.3 Signs of Over Heating?	1		ABCD	N(U) m
	1.4 Contact Condition			ABCD	NAO 110
	1.5 Operating Mechanism Condition			A BOD	NU 254
	1.6 Overall Condition			A/B C D	NU ms
3 Pole		Location.	The State of the last	estava relativ	70.5000
	'		Egg County Hall In		
1 1	1.1 Holes and Cracks ?			ABCD	N U 20
	1.2 Rot ?			ABCD	N U 20
	1.3 Cross arm Condition	,		ABCD	N U 192
	1.4 Overall Pole Condition		. :	A B C D	NU ms
3 Pole I	Mounted Transformer	Location.	胡声音篇		
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	1.1 Tank Integrity			ABCD	N U 120
	1.2 Oil Leak			ABCD	N.U. m
	1.3 Bushing Condition	100		ABCD	N U 122
	1.4 Electrical Connections			ABCD	N U 125
	1.5 Signs of Overheating?			ABCD	N U 125
	1.6 Overall Transformer Condition			N D O D	21 0
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