# EP POST. out

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
- CN\* = 80.0 Ia = Dep. Storage (Above)

  (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

  THAN THE STORAGE COEFFICIENT.

  (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0004)     IN= 2> OUT= 1     DT= 5.0 min	OUTFLOW (cms) 0. 0000 0. 0610 0. 0870 0. 1060 0. 1230 0. 1370	STORAGE (ha.m.) 0.0000 0.0144 0.0288 0.0433 0.0577 0.0721	OUTFLOW (cms) 0. 1500 0. 1620 0. 1740 0. 1840 0. 1940 0. 0000	0. 1154 0. 1298	
TIME	ARE (ha 2001) 2.2	EA QPEAK (a) (cms) (280 0.37 (280 0.09 (EDUCTION [Qoue EAK FLOW	TPEAK (hrs) 78 12.25	R. V. (mm) 48. 38 48. 36 5. 34 0. 00	
** SI MULATI ON NUMBER:	2 **				

READ STORM	Filename:	C: \Users\mark. sullivan\AppD
		ata\local\Temn\

ata\Local\Temp\
58d7a035-5c9b-4dcd-a8a9-886d29d4331d\7d647cf8
Comments: 24-Hour 5-Year SCS Type II Storm Sarnia

Ptotal = 67.60 mm

hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/ 0.25 0.00 6.50 1.22 12.75 9.73 19.00 1.0 0.50 0.74 6.75 1.22 13.00 5.14 19.25 1.3	•				٠.			
1.00       0.74       7.25       1.22       13.50       3.79       19.75       1.3         1.25       0.74       7.50       1.62       13.75       3.52       20.00       1.0         1.50       0.73       7.75       1.35       14.00       2.97       20.25       1.3         1.75       0.76       8.00       1.62       14.25       2.70       20.50       0.8         2.00       0.73       8.25       1.35       14.50       2.16       20.75       0.8         2.25       0.76       8.50       1.89       14.75       1.89       21.00       0.8         2.50       0.87       8.75       1.62       15.00       1.89       21.25       0.8         2.75       0.89       9.00       1.89       15.25       2.16       21.50       0.8         3.00       0.87       9.25       1.89       15.50       1.89       21.75       0.8         3.25       0.89       9.50       2.16       15.75       2.16       22.00       0.8         3.50       0.87       9.75       2.16       16.00       1.89       22.25       0.8         3.75       0.89	hrs m 0. 25 0. 50 0. 75 1. 00 1. 25 1. 50 1. 75 2. 00 2. 25 2. 50 2. 75 3. 00 3. 25 3. 50 3. 75 4. 00 4. 25	m/hr 0. 00 0. 74 0. 74 0. 74 0. 74 0. 73 0. 76 0. 73 0. 76 0. 87 0. 89 0. 87 0. 89 0. 87 0. 89 10. 89	hrs r 6. 50 6. 75 7. 00 7. 25 7. 50 7. 75 8. 00 8. 25 8. 50 8. 75 9. 00 9. 25 9. 50 9. 75 10. 00 10. 25 10. 50	1. 22 1. 22 1. 22 1. 22 1. 62 1. 35 1. 62 1. 35 1. 62 1. 89 1. 62 1. 89 2. 16 2. 16 2. 43 2. 43 3. 24	hrs 12. 75 13. 00 13. 25 13. 50 13. 75 14. 00 14. 25 14. 50 14. 75 15. 00 15. 25 15. 50 16. 00 16. 25 16. 50 16. 75	mm/hr 9. 73 5. 14 4. 87 3. 79 3. 52 2. 97 2. 70 2. 16 1. 89 2. 16 1. 35 1.	hrs 19. 00 19. 25 19. 50 19. 75 20. 00 20. 25 20. 50 20. 75 21. 00 21. 25 21. 50 21. 75 22. 00 22. 25 22. 50 22. 75 23. 00	RAIN mm/hr 1.08 1.35 1.08 1.35 1.08 1.35 0.81 0.81 0.81 0.81 0.81 0.81 0.81 0.81

```
EP POST. out 00 4. 33 |
                                             17. 25
17. 50
17. 75
18. 00
                                                                     23. 50
23. 75
24. 00
24. 25
4.75
           1.08
                     11.00
                                                           1.35
                                                                                  0.81
                                                          1. 08
1. 35
1. 08
5.00
                      11. 25
           1.08
                                   4.06
                                                                                  0.81
                     11. 50
11. 75
5. 25
            1.08
                                   6.49
                                                                                  0.81
5.50
           1.08
                                   6.49
                                                                                  0.81
                     12. 00
12. 25
5.75
           1.08
                                  20.01
                                             18. 25
                                                           1.35
                                             18.50
6.00
           1.08
                                  82.74
                                                          1.08
           1. 08 | 12. 50
                                  9. 73 | 18. 75
6. 25
                                                          1. 35
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CALIB
STANDHYD (0001)
| ID= 1 DT= 5.0 min
                           Area (ha) = 2.28
Total Imp(\%) = 90.00
                                                      Dir. Conn. (%) = 90.00
                                   I MPERVI OUS
                                                    PERVIOUS (i)
                          (ha)=
                                                        0. 23
     Surface Area
                                       2.05
                                        1.00
                                                        5.00
     Dep. Storage
                          (mm) =
     Average Slope
                           (%) =
                                        1.00
                                                       2.00
                                      123. 29
                                                       40.00
     Lengtň
                           (m) =
     Manni ngs n
                                      0.013
                                                      0.250
```

TIME hrs 0. 083 0. 167 0. 250 0. 333 0. 417 0. 500 0. 583 0. 667 0. 750 0. 833 1. 167 1. 250 1. 333 1. 417 1. 500 1. 583	RAIN mm/hr 0.00 0.00 0.00 0.74 0.74 0.74 0.74 0.74	TIME hrs 6. 167 6. 250 6. 333 6. 417 6. 500 6. 583 6. 667 6. 750 6. 833 6. 917 7. 000 7. 083 7. 167 7. 250 7. 333 7. 417 7. 500 7. 583 7. 667	ANSFORME RAIN mm/hr 1.08 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.2	TIME hrs 12. 250 12. 333 12. 417 12. 500 12. 583 12. 667 12. 750 12. 833 12. 917 13. 000 13. 083 13. 167 13. 250 13. 333 13. 417 13. 500 13. 583 13. 667 13. 750	APH RAIN mm/hr 82. 74 9. 74 9. 73 9. 73 9. 73 9. 73 5. 14 5. 14 4. 87 4. 87 4. 87 4. 87 3. 79 3. 79 3. 52 3. 52	TI ME hrs 18. 33 18. 42 18. 50 18. 58 18. 67 18. 75 18. 83 18. 92 19. 00 19. 08 19. 17 19. 25 19. 33 19. 42 19. 50 19. 58 19. 75 19. 83	RAIN mm/hr 1. 08 1. 08 1. 35 1. 35 1. 08 1. 35 1. 35 1. 35 1. 08 1. 35 1. 35 1. 08 1. 35 1. 08 1. 35 1. 35 1. 08
1. 583 1. 667 1. 750 1. 833 1. 917 2. 000 2. 083 2. 167 2. 250 2. 333 2. 417 2. 500 2. 583 2. 667 2. 750 2. 833 2. 917	0. 76 0. 76 0. 73 0. 73 0. 73 0. 76 0. 76 0. 87 0. 87 0. 89 0. 89 0. 89 0. 89	7. 667 7. 750 7. 833 7. 917 8. 000 8. 083 8. 167 8. 250 8. 333 8. 417 8. 500 8. 583 8. 667 8. 750 8. 833 8. 917 9. 000	1. 35 1. 35 1. 62 1. 62 1. 35 1. 35 1. 89 1. 89 1. 62 1. 62 1. 89 1. 89	13. 750 13. 833 13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 500 14. 583 14. 667 14. 750 14. 833 14. 917 15. 000 15. 083	3. 52 2. 97 2. 97 2. 70 2. 70 2. 16 2. 16 1. 89 1. 89 1. 89 1. 89 2. 16	19. 83 19. 92 20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17	1. 08 1. 08 1. 08 1. 35 1. 35 1. 35 0. 81 0. 81 0. 81 0. 81 0. 81 0. 81 0. 81

Page 5

```
0.87
                                9.083
                                          1.89
             3.000
                                                 |15. 167
                                                             2. 16
                                                                      21.25
                                                                                0.81
             3.083
                       0.89
                                9.167
                                          1.89
                                                  15. 250
                                                              2. 16
                                                                      21.33
                                                                                0.81
                                9. 250
             3.167
                       0.89
                                           1.89
                                                  15.333
                                                              1.89
                                                                      21.42
                                                                                0.81
                                          2. 16
             3.250
                                9.333
                                                                      21.50
                       0.89
                                                             1.89
                                                  15. 417
                                                                                0.81
             3.333
                       0.87
                                9.417
                                           2.16
                                                  15.500
                                                             1.89
                                                                      21.58
                                                                                0.81
                       0.87
                                9.500
                                          2.16
                                                  15.583
             3.417
                                                              2.16
                                                                      21.67
                                                                                0.81
             3.500
                       0.87
                                9.583
                                          2.16
                                                  15.667
                                                             2.16
                                                                      21.75
                                                                                0.81
                                          2.16
             3.583
                       0.89
                               9.667
                                                  15.750
                                                             2.16
                                                                      21.83
                                                                                0.81
             3.667
                       0.89
                               9.750
                                          2.16
                                                  15.833
                                                             1.89
                                                                      21.92
                                                                                0.81
             3.750
                                          2. 43
2. 43
                                                             1.89
                                                                      22.00
                       0.89
                               9.833
                                                  15.917
                                                                                0.81
                                                                                0.81
             3.833
                       0.89
                               9. 917
                                                  16,000
                                                              1.89
                                                                      22.08
                                          2. 43
2. 43
                               10.000
                                                  16.083
                                                             2. 16
2. 16
                                                                      22. 17
22. 25
             3.917
                       0.89
                                                                                0.81
             4.000
                       0.89
                                                  16. 167
                              10.083
                                                                                0.81
                                          2. 43
2. 43
             4.083
                       0.87
                               10. 167
                                                  16.250
                                                             2.16
                                                                      22.33
                                                                                0.81
             4.167
                       0.87
                               10.250
                                                  16.333
                                                             1.08
                                                                      22.42
                                                                                0.81
             4. 250
                                          3.24
                       0.87
                               10. 333
                                                  16. 417
                                                             1.08
                                                                      22.50
                                                                                0.81
             4.333
                                           3. 24
                                                  16.500
                       1.08
                                                             1.08
                              10. 417
                                                                      22. 58
                                                                                0.81
             4.417
                       1.08
                               10.500
                                          3.24
                                                  16.583
                                                             1.35
                                                                      22.67
                                                                                0.81
                                          2. 97
2. 97
                                                             1. 35
1. 35
1. 08
             4.500
                               10.583
                                                                                0.81
                       1.08
                                                  16.667
                                                                      22.75
             4.583
                       1.08
                               10.667
                                                  16.750
                                                                      22.83
                                                                                0.81
                                           2.97
             4.667
                       1.08
                               10.750
                                                  16.833
                                                                      22.92
                                                                                0.81
             4.750
                       1.08
                                          4.33
                                                  16.917
                                                                      23.00
                              10.833
                                                             1.08
                                                                                0.81
             4. 833
                                          4.33
                                                  17.000
                       1.08
                              10.917
                                                             1.08
                                                                      23.08
                                                                                0.81
             4.917
                       1.08
                              11.000
                                          4.33
                                                  17.083
                                                             1.35
                                                                      23.17
                                                                                0.81
             5.000
                       1.08
                              11.083
                                          4.06
                                                  17. 167
                                                             1.35
                                                                      23.25
                                                                                0.81
             5.083
                       1.08
                                                                      23.33
                              11. 167
                                          4.06
                                                  17.250
                                                             1.35
                                                                                0.81
             5. 167
                               11. 250
                       1.08
                                          4.06
                                                  17.333
                                                             1.08
                                                                      23.42
                                                                                0.81
                                                  17. 417
17. 500
             5. 250
                                                                      23.50
                       1.08
                               11. 333
                                          6.49
                                                             1.08
                                                                                0.81
             5.333
                       1.08
                               11.417
                                          6.49
                                                             1.08
                                                                      23.58
                                                                                0.81
                                                  17.583
                                                             1. 35
1. 35
             5.417
                       1.08
                               11.500
                                          6.49
                                                                      23.67
                                                                                0.81
             5.500
                       1.08
                              11. 583
                                          6.49
                                                 17. 667
                                                                      23.75
                                                                                0.81
                                                 17. 750
                                                                      23.83
             5.583
                       1.08
                              11.667
                                         6. 49
                                                             1.35
                                                                                0.81
             5.667
                       1.08
                              11.750
                                          6.49
                                                  17.833
                                                             1.08
                                                                      23.92
                                                                                0.81
             5.750
                       1.08
                              11.833
                                         20.01
                                                  17.917
                                                             1.08
                                                                      24.00
                                                                                0.81
                       1.08
                              11.917
                                         20.01
                                                  18.000
                                                             1.08
                                                                      24.08
                                                                                0.81
             5.833
             5.917
                       1.08
                              12.000
                                         20.01
                                                  18.083
                                                             1.35
                                                                      24. 17
                                                                                0.81
                                                             1. 35
1. 35
                       1.08
                                         82. 73
82. 74
             6.000
                              12.083
                                                  18. 167
                                                                      24. 25
                                                                                0.81
             6.083
                       1. 08
                              12. 167
                                                 18. 250
                           82. 74
5. 00
3. 12 (ii)
5. 00
0. 27
Max. Eff. Inten. (mm/hr)=
                                                46.67
            over (min)
                                                10.00
                                                6.29 (ii)
Storage Coeff.
                   (min) =
Unit Hyd. Tpeak (min)=
                                                10.00
Unit Hyd. peak (cms)=
                                                0. 15
                                                                *TOTALS*
                   (cms) = 0.47
(hrs) = 12.25
(mm) = 66.60
(mm) = 67.60
                                        0. 02
12. 25
31. 08
PEAK FLOW
TIME TO PEAK
                                                                  0. 493 (iii)
12. 25
RUNOFF VOLUME
                                                                 63.05
TOTAL RAINFALL
                                                67.60
                                                                  67.60
RUNOFF COEFFICIENT
                                 0.99
                                                 0.46
                                                                  0.93
```

EP POST. out

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
- CN\* = 80.0 Ia = Dep. Storage (Above)
  (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
  THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

\_\_\_\_\_\_

RESERVOIR (0004) | IN= 2---> OUT= 1

```
EP POST. out
| DT= 5.0 min |
                           OUTFLOW
                                       STORAGE
                                                      OUTFI OW
                                                                  STORAGE
                            (cms)
                                        (ha. m.)
                                                       (cms)
                                                                   (ha. m.)
                            0.0000
                                        0.0000
                                                       0.1500
                                                                    0.0865
                                                       0.1620
                            0.0610
                                        0.0144
                                                                    0.1009
                                        0.0288
                            0.0870
                                                       0.1740
                                                                    0.1154
                                        0.0433
                                                       0.1840
                                                                    0.1298
                            0.1060
                            0.1230
                                        0.0577
                                                       0.1940
                                                                    0.1442
                                                       0.0000
                            0.1370
                                        0.0721
                                                                    0.0000
                                   AREA
                                             QPEAK
                                                        TPEAK
                                                                      R. V.
                                   (ha)
                                             (cms)
                                                        (hrs)
                                                                      (mm)
     INFLOW: ID= 2 (0001)
OUTFLOW: ID= 1 (0004)
                                                          12. 25
                                   2. 280
2. 280
                                               0. 493
                                                                       63.05
                                               0.111
                                                          12.42
                                                                       63.02
                    PEAK
                            FLOW
                                    REDUCTION [Qout/Qin](%) = 22.58
                    TIME SHIFT OF PEAK FLOW
                                                        (mi n) = 10.00
                    MAXIMUM STORAGE
                                        USED
                                                      (ha. m.) = 0.0482
  ** SIMULATION NUMBER: 3 **
                          Filename: C:\Users\mark.sullivan\AppD
     READ STORM
                                     ata\Local \Temp\
                                     58d7a035-5c9b-4dcd-a8a9-886d29d4331d\1d16d696
 Ptotal = 77.60 mm
                          Comments: 24-Hour 10-Year SCS Type II Storm Sarnia
                  TIME
                                                                RAI N
                           RAIN
                                    TIME
                                             RAIN |
                                                       TIME
                                                                         TI ME
                                                                                  RAIN
                   hrs
                          mm/hr
                                                               mm/hr
                                     hrs
                                            mm/hr
                                                        hrs
                                                                          hrs
                                                                                 mm/hr
                                    6.50
                                                    12.75
                                                                      19.00
                  0.25
                           0.00
                                             1.40
                                                              11. 17
                                                                                 1. 24
                  0.50
                                    6.75
                                                               5. 90
                                                                       19.25
                           0.85
                                             1.40
                                                    13.00
                                                                                 1.55
                  0.75
                                             1.40
                                                               5.59
                                                                       19.50
                           0.85
                                    7.00
                                                    13. 25
                                                                                 1.24
                                             1.40
                  1.00
                           0.85
                                    7. 25
                                                    13.50
                                                               4.35
                                                                       19.75
                                                                                 1.55
                           0.85
                                    7.50
                                                     13.75
                                                                       20.00
                  1.25
                                             1.86
                                                               4.04
                                                                                 1.24
                  1. 50
1. 75
                           0.84
                                    7.75
                                             1.55
                                                     14.00
                                                               3.41
                                                                       20.25
                                                                                 1.55
                                                                       20.50
                                                               3.10
                                                                                 0.93
                           0.87
                                    8.00
                                             1.86
                                                     14.25
                  2.00
                           0.84
                                    8.25
                                                     14.50
                                                                       20.75
                                                                                 0.93
                                             1.55
                                                               2.48
                  2.25
                           0.87
                                    8.50
                                             2.17
                                                     14.75
                                                               2.17
                                                                       21.00
                                                                                 0.93
                  2.50
                           0.99
                                    8.75
                                             1.86
                                                     15.00
                                                               2.17
                                                                       21.25
                                                                                 0.93
                  2.75
                           1.02
                                                     15. 25
                                                               2.48
                                                                                 0.93
                                    9.00
                                                                       21.50
                                             2. 17
                  3.00
                           0.99
                                    9. 25
                                             2.17
                                                               2.17
                                                                                 0.93
                                                     15. 50
                                                                       21.75
                           1.02
                  3.25
                                    9.50
                                             2.48
                                                     15.75
                                                               2.48
                                                                       22.00
                                                                                 0.93
                  3.50
                           0.99
                                    9.75
                                             2.48
                                                     16.00
                                                               2.17
                                                                                 0.93
                                                                       22.25
                  3.75
                                             2.79
                           1.02
                                   10.00
                                                     16.25
                                                               2.48
                                                                       22.50
                                                                                 0.93
                                             2.79
                                                               1.24
                                                                       22.75
                  4.00
                                                     16.50
                                                                                 0.93
                           1.02
                                   10. 25
                                                     16. 75
                           0.99
                                   10.50
                                             3.72
                                                                       23.00
                                                                                 0.93
                  4.25
                                                               1.55
                           1.24
                                   10.75
                  4.50
                                             3.41
                                                     17.00
                                                               1.24
                                                                       23.25
                                                                                 0.93
                                             4.97
                                                                                 0.93
                  4.75
                           1.24
                                   11.00
                                                     17. 25
                                                               1.55
                                                                       23.50
                  5.00
                                                                                 0.93
                           1.24
                                   11. 25
                                             4.66
                                                     17.50
                                                               1.24
                                                                       23.75
                                   11.50
                  5.25
                           1.24
                                             7.45
                                                     17. 75
                                                               1.55
                                                                       24.00
                                                                                 0.93
                  5.50
                                                     18.00
                           1.24
                                   11. 75
                                             7.45
                                                               1.24
                                                                       24.25
                                                                                 0.93
                                   12.00
                  5.75
                           1. 24
                                            22.97
                                                     18.25
                                                               1.55
                                   12.25
                                            94.98
                  6.00
                           1.24
                                                     18.50
                                                               1.24
                           1. 24
                                   12.50
                                                    18.75
                  6. 25
                                            11. 17
                                                               1.55
```

CALIB STANDHYD (0001) | Area (ha)= 2.28 Page 7

TRANSFORMED HYETOGRAPH	
TIME RAIN   TIME RAIN   TIME RAIN   TIME hrs mm/hr   hrs mm/hr   hrs	RAIN mm/hr
0. 083	1. 24
	1. 24
	1. 24 1. 55
0. 417	1. 55
	1. 55 1. 24
0. 667	1. 24
	1. 24 1. 55
0. 917	1.55
1. 000	1. 55 1. 24
	1. 24
	1. 24
	1. 55 1. 55
1. 500 0. 84   7. 583 1. 55   13. 667 4. 04   19. 75	1.55
	1. 24 1. 24
1. 750 0. 87   7. 833 1. 86   13. 917 3. 41   20. 00	1. 24
	1. 55 1. 55
2. 000 0. 84 8. 083 1. 55 14. 167 3. 10 20. 25	1. 55
	0. 93 0. 93
2. 250 0. 87   8. 333 2. 17   14. 417 2. 48   20. 50	0. 93
	0. 93 0. 93
2. 500 0. 99 8. 583 1. 86 14. 667 2. 17 20. 75	0. 93
	0. 93 0. 93
2. 750	0. 93
	0. 93 0. 93
3. 000 0. 99   9. 083 2. 17   15. 167 2. 48   21. 25	0. 93
	0. 93
	0. 93 0. 93
	0. 93
	0. 93 0. 93
3. 583	0. 93
	0. 93 0. 93
3. 833	0. 93
	0. 93 0. 93

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EP POST. out
7 2. 79 |
             4.083
                        0.99
                                10. 167
                                                   16. 250
                                                               2.48
                                                                        22.33
                                                                                   0.93
                                                                1.24
             4.167
                        0.99
                                10.250
                                            2.79
                                                   16.333
                                                                        22.42
                                                                                   0.93
                                                                1. 24
1. 24
                        0.99
                                            3. 72
3. 72
                                                                        22.50
             4.250
                                10.333
                                                   16.417
                                                                                   0.93
             4.333
                        1.24
                                                   16.500
                                                                        22.58
                                                                                   0.93
                                10. 417
                        1. 24
                                                                                   0.93
             4.417
                                10.500
                                            3.72
                                                   16.583
                                                                1.55
                                                                        22.67
             4.500
                        1.24
                                            3.41
                                                                1.55
                                                                        22.75
                                                                                   0.93
                                10.583
                                                   16.667
             4.583
                        1.24
                                10.667
                                            3.41
                                                   16.750
                                                                1.55
                                                                        22.83
                                                                                   0.93
                                            3.41
                        1.24
                                                                                   0.93
             4.667
                                10.750
                                                   16.833
                                                                1. 24
                                                                        22. 92
                                            4.97
                                                                                   0.93
             4.750
                        1.24
                                                   16. 917
                                                                1.24
                                                                        23.00
                                10.833
                                                   17.000
             4.833
                        1.24
                                10.917
                                            4.97
                                                                1.24
                                                                        23.08
                                                                                   0.93
             4.917
                        1.24
                                11.000
                                            4.97
                                                   17.083
                                                                1.55
                                                                        23.17
                                                                                   0.93
                        1. 24
1. 24
                                                   17. 167
17. 250
                                                                        23. 25
23. 33
             5.000
                                11.083
                                            4.66
                                                                1.55
                                                                                   0.93
                                                                1.55
                                                                                   0.93
             5.083
                                11. 167
                                            4.66
                        1.24
                                11.250
                                                   17.333
                                                                        23.42
                                                                                   0.93
             5. 167
                                            4.66
                                                                1.24
             5.250
                        1.24
                                11.333
                                            7.45
                                                   17.417
                                                                1.24
                                                                        23.50
                                                                                   0.93
             5.333
                                            7.45
                                                                1.24
                        1. 24
                                11. 417
                                                   17.500
                                                                        23.58
                                                                                   0.93
                        1. 24
                                11.500
                                                                1.55
                                                                                   0.93
             5. 417
                                            7.45
                                                   17. 583
                                                                        23. 67
             5.500
                        1. 24
                                            7.45
                                11.583
                                                                1.55
                                                                        23.75
                                                                                   0.93
                                                   17. 667
                                                   17. 750
17. 833
             5.583
                                11.667
                        1.24
                                            7.45
                                                                1.55
                                                                        23.83
                                                                                   0.93
                                                               1. 24
1. 24
1. 24
                        1. 24
1. 24
1. 24
                                            7.45
             5.667
                                11.750
                                                                        23.92
                                                                                   0.93
             5.750
                                11.833
                                           22.97
                                                   17.917
                                                                        24.00
                                                                                   0.93
                                           22.97
                                                                                   0.93
             5.833
                                11.917
                                                   18.000
                                                                        24.08
                        1. 24
                                           22.97
                                                                1.55
                                                                                   0.93
             5.917
                                12.000
                                                   18.083
                                                                        24.17
                                           94.97
             6.000
                        1.24
                                12.083
                                                   18. 167
                                                                1.55
                                                                        24.25
                                                                                   0.93
                                           94.98
             6.083
                        1. 24
                               12. 167
                                                  18. 250
                                                                1.55
Max. Eff. Inten. (mm/hr) =
                                  94.98
                                                  57.97
                                                  10.00
             over (min)
                                   5.00
Storage Coeff.
                    (min) =
                                   2.96 (ii)
                                                   5.95 (ii)
Unit Hyd. Tpeak (min) = Unit Hyd. peak (cms) =
                                                  10.00
                                   5.00
                                   0.28
                                                   0.15
                                                                  *TOTALS*
PEAK FLOW
                    (cms) =
                                   0.54
                                                   0.03
                                                                    0.569 (iii)
TIME TO PEAK
                    (hrs) =
                                  12.25
                                                  12.25
                                                                    12.25
RUNOFF VOLUME
                     (mm) =
                                  76.60
                                                  38. 73
                                                                    72.81
                                                                    77.60
TOTAL RAINFALL
                     (mm) =
                                  77.60
                                                  77.60
RUNOFF COEFFICIENT
                                   0.99
                                                   0.50
                                                                      0.94
```

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

RESERVOIR (0004)     IN= 2> OUT= 1				
DT= 5.0 min	OUTFLOW	STORAGE	OUTFLOW	STORAGE
5:	(cms)	(ha.m.)	(cms)	(ha. m. )
			, ,	
	0.0000	0.0000	0. 1500	0. 0865
	0. 0610	0. 0144	0. 1620	0. 1009
	0. 0870	0. 0288	0. 1740	0. 1154
	0. 1060	0. 0433	0. 1840	0. 1298
	0. 1230	0. 0577	0. 1940	0. 1442
				- · · · · -
	0. 1370	0. 0721	0.0000	0. 0000
	AR	EA QPEAK	TPEAK	R. V.
	(h	a) (cms)	(hrs)	(mm)
INFLOW : ID= 2 (00		280 0.50		72. 81
	- /			
OUTFLOW: ID= 1 (00	04) 2.	280 0. 12	21 12.42	72. 79
		D 0		

# EP POST. out

PEAK FLOW REDUCTION [Qout/Qi n] (%) = 21.27 TIME SHIFT OF PEAK FLOW (mi n) = 10.00 MAXIMUM STORAGE USED (ha. m.) = 0.0565

\*\*\*\*\*\*\*

\*\* SIMULATION NUMBER: 4 \*\*

Filename: C:\Users\mark.sullivan\AppD ata\Local\Temp\ READ STORM

58d7a035-5c9b-4dcd-a8a9-886d29d4331d\6b7e5e22

Ptotal = 90.20 mm | Comments: 24-Hour 25-Year SCS Type II Storm Sarnia

TIME hrs 0. 25 0. 50 1. 25 1. 75 1. 75 2. 25 2. 75 3. 25 2. 75 3. 25 3. 75 4. 25 4. 75 5. 25 5. 75 6. 00 6. 25	RAIN mm/hr 0.00 0.99 0.99 0.99 0.97 1.01 1.15 1.19 1.15 1.19 1.15 1.44 1.44 1.44 1.44 1.44 1.44 1.44	TI ME hrs 6. 50 6. 75 7. 00 7. 25 7. 50 8. 00 8. 25 8. 75 9. 25 9. 50 9. 75 10. 00 10. 25 11. 50 11. 75 12. 00 12. 25 12. 50	1. 62 1. 62 1. 62 1. 62 2. 16 1. 80 2. 16 2. 53 2. 16 2. 53 2. 53 2. 89 2. 89 3. 25 4. 33 3. 97 5. 77	TI ME hrs 12. 75 13. 00 13. 25 13. 50 14. 00 14. 25 14. 50 15. 50 15. 75 16. 00 16. 25 16. 50 17. 75 17. 00 17. 25 17. 50 17. 75 18. 00 18. 25 18. 50 18. 75	RAIN mm/hr 12. 99 6. 86 6. 49 5. 05 4. 69 3. 61 2. 89 2. 53 2. 53 2. 89 2. 53 2. 89 1. 44 1. 80 1. 44 1. 80 1. 44 1. 80 1. 44 1. 80 1. 44 1. 80	TIME hrs 19.00 19.25 19.50 19.75 20.00 20.25 20.50 21.00 21.25 21.50 21.75 22.00 22.25 22.75 23.00 23.25 23.50 23.75 24.00 24.25	mm/hr 1.44 1.80 1.44 1.80 1.44
0. 23	1. 77	12.50	12. //	10.75	1.00		
	.,	1 00	. =	1		I	

CALIB STANDHYD (0001) ID= 1 DT= 5.0 min	Area Total		2. 28 90. 00	Dir. Conn. (%)=	90. 00
Surface Area Dep. Storage Average SI ope Length Manni ngs n	(ha) = (mm) = (%) = (m) = =	I MPERVI 2. 0 1. 0 1. 0 123. 2 0. 01	5 0 0 9	PERVIOUS (i) 0. 23 5. 00 2. 00 40. 00 0. 250	

TI ME hrs 0. 083 0. 167 0. 250 0. 333 0. 417 0. 583 0. 667 0. 750 0. 833 1. 1. 250 1.	RAIN mm/hr 0.00 0.99 0.99 0.99 0.99 0.99 0.99 0.9	EP TI ME hrs 6. 167 6. 250 6. 333 6. 417 6. 583 6. 667 6. 833 7. 000 7. 083 7. 167 7. 250 7. 333 7. 417 7. 583 7. 750 7. 833 7. 750 7. 833 7. 750 8. 333 8. 417 8. 500 8. 333 8. 417 8. 500 8. 333 8. 417 9. 083 9. 167 9. 250 9. 167 9. 250 9.	RAIN mm/hr 1. 44 1. 62 1	TI ME hrs 12. 250 12. 333 12. 417 12. 500 12. 583 12. 667 12. 750 12. 833 12. 917 13. 000 13. 083 13. 167 13. 250 13. 333 13. 417 13. 500 13. 583 13. 667 13. 750 13. 833 13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 15. 000 15. 083 15. 167 15. 250 15. 333 15. 417 15. 500 15. 833 15. 917 16. 000	RAIN mm/hr 110. 40 12. 99 12.	TI ME hrs 18. 33 18. 42 18. 50 18. 58 18. 67 18. 75 18. 83 18. 92 19. 00 19. 33 19. 42 19. 50 19. 58 19. 75 19. 83 19. 67 19. 75 19. 83 20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 21. 00 21. 08 21. 17 21. 58 21. 67 21. 75 21. 83 21. 92 22. 08 23. 77	RAII mm/h 1. 44 1. 44 1. 80 1. 80 1. 80 1. 80 1. 44 1. 44 1. 80 1. 80 1. 80 1. 44 1. 44 1. 80 1. 80 1. 08 1.
3. 500 3. 583 3. 667 3. 750	1. 15 1. 19 1. 19 1. 19	9. 583 9. 667 9. 750 9. 833 9. 917 10. 000 10. 083 10. 167 10. 250 10. 333 10. 417 10. 500 10. 583 10. 667 10. 750 10. 833 10. 917 11. 000 11. 083 11. 167	2. 89 2. 89 2. 89 3. 25	15. 667 15. 750 15. 833 15. 917	2. 89 2. 89 2. 53 2. 53	21. 75 21. 83 21. 92 22. 00	1. 08 1. 08 1. 08 1. 08

```
EP POST. out
                                   11. 250
                                               5. 41
                                                                          23.42
                  5. 167
                            1.44
                                                     |17. 333
                                                                 1.44
                                                                                    1.08
                                                                                    1.08
                  5.250
                            1.44
                                               8.66
                                                      17.417
                                                                 1.44
                                                                          23.50
                                   11. 333
                  5.333
                                                      17.500
                            1.44
                                   11.417
                                               8.66
                                                                  1.44
                                                                          23.58
                                                                                    1.08
                                                      17.583
                            1.44
                  5.417
                                   11.500
                                               8. 66
                                                                  1.80
                                                                          23.67
                                                                                    1.08
                  5.500
                            1.44
                                   11.583
                                               8.66
                                                      17.667
                                                                 1.80
                                                                          23.75
                                                                                    1.08
                  5.583
                            1.44
                                                      17.750
                                                                 1.80
                                                                          23.83
                                   11.667
                                               8.66
                                                                                    1.08
                  5.667
                            1.44
                                   11.750
                                               8.66
                                                      17.833
                                                                 1.44
                                                                          23.92
                                                                                    1.08
                  5.750
                            1.44
                                                      17.917
                                                                 1.44
                                              26.70
                                                                          24.00
                                   11.833
                                                                                    1.08
                  5.833
                            1.44
                                   11.917
                                              26.70
                                                      18.000
                                                                 1.44
                                                                          24.08
                                                                                    1.08
                                   12.000
                                                                                    1.08
                  5.917
                            1.44
                                              26.70
                                                      18.083
                                                                 1.80
                                                                          24. 17
                  6.000
                            1.44
                                   12.083
                                             110.39
                                                      18. 167
                                                                 1.80
                                                                          24.25
                                                                                    1.08
                  6.083
                            1.44
                                   12. 167
                                             110. 40
                                                     18. 250
                                                                  1.80
     Max. Eff. Inten. (mm/hr)=
                                    110.40
                                                     72.74
                  over (min)
                                       5.00
                                                     10.00
                        (min) =
                                       2.78 (ii)
     Storage Coeff.
                                                      5.60 (ii)
     Unit Hyd. Tpeak (min)=
                                       5.00
                                                     10.00
     Unit Hyd. peak (cms)=
                                      0.28
                                                      0.15
                                                                    *TOTALS*
     PEAK FLOW
TIME TO PEAK
                                      0.63
                                                      0.04
                                                                      0.666 (iii)
                        (cms) =
                                      12. 25
89. 20
                                                     12.25
                        (hrs) =
                                                                      12.25
     RUNOFF VOLUME
                                                     48.82
                                                                      85.16
                         (mm) =
     TOTAL RAINFALL
                                      90.20
                                                     90.20
                                                                      90.20
                         (mm) =
     RUNOFF COEFFICIENT
                                       0.99
                                                      0.54
                                                                       0.94
**** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
        (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
      CN* = 80.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
     (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

RESERVOIR (0004)     IN= 2> OUT= 1     DT= 5.0 min		STORAGE (ha.m.) 0.0000 0.0144 0.0288 0.0433 0.0577 0.0721	OUTFLOW (cms) 0.1500 0.1620 0.1740 0.1840 0.1940 0.0000	0. 1154 0. 1298 0. 1442	
Т	(h (0001) 2. (0004) 2. EAK FLOW R IME SHIFT OF P AXIMUM STORAG	280 0.6 280 0.1 EDUCTION [Qo	(hrs) 66 12.25 32 12.42	85. 14 9. 79 0. 00	

READ STORM | Filename: C:\Users\mark.sullivan\AppD
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\*\* SIMULATION NUMBER: 5 \*\*

EP POST.out ata\Local\Temp\
58d7a035-5c9b-4dcd-a8a9-886d29d4331d\a1e5d969
Comments: 24-Hour 50-Year SCS Type II Storm Sarnia

TIME hrs         RAIN mm/hr         TIME hrs           0. 25         0. 00         6. 50         1. 79         12. 75         14. 34         19. 00           0. 50         1. 10         6. 75         1. 79         13. 00         7. 57         19. 25           0. 75         1. 10         7. 00         1. 79         13. 25         7. 17         19. 50           1. 00         1. 10         7. 25         1. 79         13. 50         5. 58         19. 75           1. 25         1. 10         7. 50         2. 39         13. 75         5. 18         20. 00           1. 50         1. 08         7. 75         1. 99         14. 00         4. 38         20. 25           1. 75         1. 12         8. 00         2. 39         14. 25         3. 98         20. 50           2. 00         1. 08         8. 25         1. 99         14. 50         3. 19         20. 75           2. 25         1. 12         8. 50         2. 79         14. 75         2. 79         21. 25           2. 75	RAIN mm/hr 1.59 1.99 1.59 1.99 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20

CALIB STANDHYD (0001) ID= 1 DT= 5.0 min	Area Total	(ha) = I mp(%) =	2. 28 90. 00	Dir.	Conn. (%)=	90. 00
		IMPERVI	OUS	PERVI OL	JS (i)	
Surface Area	(ha)=	2. 0		0. 23		
Dep. Storage	(mm) =	1. 0	0	5. 00		
Average Slope	(%)=	1. 0	0	2. 00	)	
Lengtȟ	(m) =	123. 2	9	40.00	)	
Manni ngs n		0. 01	3	0. 250	)	

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

	TRANSFORMED HYETOGRAPH									
TIME	RAIN	TIME	RAIN	' TIME	RAIN	TIME	RAIN			
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr	hrs	mm/hr			
0.083	0.00	6. 167	1. 59	12. 250	121. 91	<sup>'</sup> 18. 33	1. 59			
0. 167	0.00	6. 250	1. 59	12. 333	14. 36	18. 42	1. 59			
0. 250	0.00	6. 333	1. 79	12. 417	14. 34	18. 50	1. 59			
0. 333	1. 10	6. 417	1. 79	12. 500	14. 34	18. 58	1. 99			
0. 417	1. 10	6. 500	1. 79	12. 583	14. 34	18. 67	1. 99			
0.500	1. 10	6. 583	1. 79	12. 667	14. 34	18. 75	1. 99			
0. 583	1. 10	6. 667	1. 79	12. 750	14. 34	18. 83	1. 59			
0.667	1. 10	6. 750	1. 79	12. 833	7. 57	18. 92	1. 59			
0. 750	1. 10	6. 833	1. 79	12. 917	7. 57	19. 00	1. 59			
0.833	1. 10	6. 917	1. 79	13.000	7. 57	19. 08	1. 99			
0. 917	1. 10	7. 000	1. 79	13. 083	7. 17	19. 17	1. 99			
		· _								

		FD	POST. ou	t			
1. 083	.10 .10 .10 .10 .10 .10 .10 .10 .10 .10	7. 083 7. 167 7. 250 7. 333 7. 417 7. 583 7. 750 7. 833 7. 917 8. 083 8. 167 8. 250 8. 333 8. 417 8. 583 8. 417 9. 083 8. 750 9. 167 9. 250 9. 333 9. 417 9. 583 9. 417 10. 503 10. 167 10. 250 10. 333 11. 417 11. 500 11. 333 11. 417 11. 583 11. 667 11. 333 11. 417 11. 583 11. 670 11. 833 11. 670 11. 750 11. 833 11. 670 11. 750 11. 833 11. 670 11. 750 11. 75	1. 79 1. 79 1. 79 1. 79 1. 33 2. 33 99 99 99 99 99 99 99 99 99 99 99 99 9	13. 167 13. 250 13. 333 13. 417 13. 500 13. 583 13. 667 13. 833 13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 500 14. 833 14. 667 14. 833 14. 917 15. 000 15. 083 15. 167 15. 333 15. 417 15. 500 15. 833 15. 417 16. 500 16. 16. 250 16. 333 16. 417 17. 000 16. 833 17. 167 17. 250 16. 833 17. 167 17. 250 17. 333 17. 417 17. 500 17. 333 17. 417 17. 500 18. 333 17. 417 17. 500 17. 333 17. 417 17. 500 18. 250 18. 250	7. 17 7. 18 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5	19. 25 19. 33 19. 42 19. 50 19. 58 19. 67 19. 75 19. 83 19. 20. 08 20. 17 20. 25 20. 33 20. 42 20. 58 20. 67 20. 83 20. 92 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 67 21. 58 21. 67 21. 58 21. 67 21. 83 22. 42 22. 58 22. 67 22. 83 22. 42 22. 58 22. 67 22. 83 23. 67 23. 58 23. 67 23. 75 23. 83 23. 67 23. 75 23. 83 23. 67 23. 75 23. 83 24. 00 24. 25 25. 83 26. 67 27 28. 83 29. 67 29. 67 29. 75 29. 83 29. 67 29. 75 20. 83 20. 67 20. 75 21. 83 22. 67 22. 75 22. 83 22. 67 22. 75 23. 83 24. 00 25. 67 26. 75 27 28. 83 29. 67 29. 75 20. 83 20. 67 21. 75 22. 83 22. 67 22. 75 23. 83 24. 00 25. 67 26. 75 27 28. 83 29. 67 29. 75 29. 83 29. 67 29. 75 20. 83 20. 83 20. 75 20. 83 20. 83 20. 75 20. 83 20.	1. 99 1. 59 1. 59 1. 59 1. 99 1. 99 1. 99 1. 59 1. 59 1. 99 1. 20

	EP POST.	out	
Max. Eff. Inten. (mm/hr)=	121. 91	84. 03	
over (min)	5. 00	10. 00	
Storage Coeff. (min)=	2.68 (ii)	5.38 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	0. 29	0. 16	
			*TOTALS*
PEAK FLOW (cms)=	0. 69	0. 05	0.739 (iii)
TIME TO PEAK (hrs)=	12. 25	12. 25	12. 25
RUNOFF VOLUME (mm)=	98. 60	56. 60	94. 40
TOTAL RAINFALL (mm)=	99. 60	99. 60	99. 60
RUNOFF COEFFICIENT =	0. 99	0. 57	0. 95

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0004)     IN= 2> OUT= 1     DT= 5.0 min	OUTFLOW (cms) 0.0000 0.0610 0.0870 0.1060 0.1230 0.1370	STORAGE (ha. m.) 0.0000 0.0144 0.0288 0.0433 0.0577 0.0721	OUTFLOW (cms) 0. 1500 0. 1620 0. 1740 0. 1840 0. 1940 0. 0000	STORAGE (ha. m.) 0.0865 0.1009 0.1154 0.1298 0.1442 0.0000	
Ţ	(0001) 2 (0004) 2	a) (cms) 280 0.7; 280 0.14 EDUCTION [Qou EAK FLOW	(hrs) 39 12.25	0.00	

\*\* SI MULATI ON NUMBER: 6 \*\*
\*\*\*\*\*\*\*\*\*\*\*

READ STORM Ptotal =108.90 mm		ata\  58d7a	Local \Ter a035-5c9l	o-4dcd-a8	a9-886d2	29d4331d\l Storm Sai	
TIM hr 0. 2 0. 5 0. 7 1. 0 1. 2 1. 5	s mm/hr 5 0.00 0 1.20 5 1.20 0 1.20 5 1.20 0 1.18	TIME hrs 6.50 6.75 7.00 7.25 7.50 7.75 8.00	RAIN mm/hr 1.96 1.96 1.96 1.96 2.61 2.18 2.61	TIME hrs 12.75 13.00 13.25 13.50 13.75 14.00 14.25	RAIN mm/hr 15.68   8.28   7.84   6.10   5.66   4.79   4.36	TIME hrs 19.00 19.25 19.50 19.75 20.00 20.25 20.50	RAIN mm/hr 1.74 2.18 1.74 2.18 1.74 2.18 1.31

2. 00 2. 25	1. 18 1. 22	EP   8. 25   8. 50	POST. out 2. 18 3. 05	t   14.50   14.75	3. 48 3. 05	20. 75	1. 31 1. 31
2. 50	1. 39	8. 75	2. 61	15. 00	3. 05	21. 25	1. 31
2. 75	1. 44	9. 00	3. 05	15. 25	3. 48	21. 50	1. 31
3. 00	1. 39	9. 25	3. 05	15. 50	3. 05	21. 75	1. 31
3. 25	1. 44	9. 50	3. 48	15. 75	3. 48	22. 00	1. 31
3. 50	1. 39	9. 75	3. 48	16. 00	3. 05	22. 25	1. 31
3. 75	1. 44	10. 00	3. 92	16. 25	3. 48	22. 50	1. 31
4. 00	1. 44	10. 25	3. 92	16. 50	1. 74	22. 75	1. 31
4. 25	1. 39	10. 50	5. 23	16. 75	2. 18	23. 00	1. 31
4. 50	1. 74	10. 75	4. 79	17. 00	1. 74	23. 25	1. 31
4. 75	1. 74	11. 00	6. 97	17. 25	2. 18	23. 50	1. 31
5. 00 5. 25 5. 50 5. 75	1. 74 1. 74 1. 74 1. 74	11. 25 11. 50 11. 75 12. 00	6. 53 10. 45 10. 45 32. 23	17. 50 17. 75 18. 00 18. 25	1. 74 2. 18 1. 74 2. 18	23. 75 24. 00 24. 25	1. 31 1. 31 1. 31
6. 00 6. 25	1. 74 1. 74 1. 74	12. 00 12. 25 12. 50	133. 29 15. 68	18. 50 18. 75	1. 74 2. 18		

\_\_\_\_\_

```
CALI B
STANDHYD (0001)
| ID= 1 DT= 5.0 min
                                 Area (ha) = 2.28
Total Imp(%) = 90.00
                                                                   Dir. Conn. (%) = 90.00
                                           I MPERVI OUS
                                                                PERVIOUS (i)
                                                                    0. 23
5. 00
      Surface Area
                                (ha)=
                                                 2.05
      Dep. Storage
Average Slope
Length
                                (mm) =
                                                  1.00
                                                                   2. 00
40. 00
                                              1. 00
123. 29
                                 (%) =
                                  (m) =
      Manni ngs n
                                                0.013
                                                                   0.250
```

		TRA	ANSFORME	D HYETOGE	RAPH		
TIME	RAIN	TIME	RAIN	' TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr	hrs	mm/hr
0. 083	0. 00	6. 167	1. 74	12. 250	133. 29	18. 33	1. 74
0. 167	0.00	6. 250	1. 74	12. 333	15. 70	18. 42	1. 74
0. 250	0.00	6. 333	1. 96	12. 417	15. 68	18. 50	1. 74
0. 333	1. 20	6. 417	1. 96	12. 500	15. 68	18. 58	2. 18
0. 417	1. 20	6. 500	1. 96	12. 583	15. 68	18. 67	2. 18
0.500	1. 20	6. 583	1. 96	12. 667	15. 68	18. 75	2. 18
0. 583	1. 20	6. 667	1. 96	12. 750	15. 68	18. 83	1. 74
0. 667	1. 20	6. 750	1. 96	12. 833	8. 28	18. 92	1.74
0. 750 0. 833	1. 20 1. 20	6.833	1. 96 1. 96	12. 917  13. 000	8. 28	19. 00 19. 08	1. 74 2. 18
0. 633 0. 917	1. 20	6. 917 7. 000	1. 96	13.000	8. 28 7. 84	19. 06	2. 18
1. 000	1. 20	7.083	1. 96	13. 167	7. 84	19. 17	2. 18
1. 083	1. 20	7. 167	1. 96	13. 250	7. 84	19. 33	1. 74
1. 167	1. 20	7. 250	1. 96	13. 333	6. 10	19. 42	1. 74
1. 250	1. 20	7. 333	2. 61	13. 417	6. 10	19. 50	1.74
1. 333	1. 18	7. 417	2. 61	13. 500	6. 10	19. 58	2. 18
1. 417	1. 18	7. 500	2. 61	13. 583	5. 66	19. 67	2. 18
1.500	1. 18	7. 583	2. 18	13. 667	5. 66	19. 75	2. 18
1. 583	1. 22	7. 667	2. 18	13. 750	5. 66	19. 83	1. 74
1. 667	1. 22	7. 750	2. 18	13. 833	4. 79	19. 92	1. 74
1. 750	1. 22	7. 833	2. 61	13. 917	4. 79	20.00	1. 74
1. 833	1. 18	7. 917	2. 61	14. 000	4. 79	20. 08	2. 18
1. 917	1. 18	8.000	2. 61	14. 083	4. 36	20. 17	2. 18
2. 000	1. 18	8. 083	2. 18	14. 167	4. 36	20. 25	2. 18

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	EP POST. ou				
2. 083	8. 167       2. 18         8. 250       2. 18         8. 333       3. 05         8. 500       3. 05         8. 583       2. 61         8. 750       2. 61         8. 833       3. 05         9. 000       3. 05         9. 083       3. 05         9. 167       3. 05         9. 250       3. 05         9. 333       3. 48         9. 500       3. 48         9. 583       3. 48         9. 750       3. 48         9. 833       3. 92         10. 000       3. 92         10. 083       3. 92         10. 167       3. 92         10. 250       3. 92         10. 500       5. 23         10. 583       4. 79         10. 667       4. 79         10. 833       6. 97         11. 083       6. 53         11. 167       6. 53         11. 333       10. 45         11. 583       10. 45         11. 583       10. 45         11. 583       10. 45         11. 583       10. 45         11. 667       10. 45         11. 833 </td <td>14. 250 14. 333 14. 417 14. 500 14. 583 14. 667 14. 750 14. 833 14. 917 15. 000 15. 083 15. 15. 250 15. 333 15. 417 15. 500 15. 833 15. 457 16. 000 16. 083 16. 167 16. 250 16. 333 16. 417 16. 500 16. 833 16. 417 16. 500 16. 833 16. 667 17. 000 18. 000 18</td> <td>4. 36 4. 36 4. 36 3. 48 3. 48 3. 05 5. 05 6. 05 6.</td> <td>20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 83 21. 92 22. 00 22. 08 22. 17 22. 25 22. 33 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 23. 50 23. 83 22. 92 23. 00 23. 08 23. 17 23. 25 23. 33 24. 00 23. 58 23. 75 23. 33 24. 00 24. 08 24. 17 24. 25</td> <td>1. 31 1. 31</td>	14. 250 14. 333 14. 417 14. 500 14. 583 14. 667 14. 750 14. 833 14. 917 15. 000 15. 083 15. 15. 250 15. 333 15. 417 15. 500 15. 833 15. 457 16. 000 16. 083 16. 167 16. 250 16. 333 16. 417 16. 500 16. 833 16. 417 16. 500 16. 833 16. 667 17. 000 18. 000 18	4. 36 4. 36 4. 36 3. 48 3. 48 3. 05 5. 05 6.	20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 83 21. 92 22. 00 22. 08 22. 17 22. 25 22. 33 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 23. 50 23. 83 22. 92 23. 00 23. 08 23. 17 23. 25 23. 33 24. 00 23. 58 23. 75 23. 33 24. 00 24. 08 24. 17 24. 25	1. 31 1. 31
Max. Eff. Inten. (mm/hr) = over (min) Storage Coeff. (min) = Unit Hyd. Tpeak (min) = Unit Hyd. peak (cms) =	133. 29 5. 00 2. 58 (ii) 5. 00 0. 29	95. 39 10. 00 5. 19 (ii) 10. 00 0. 16	****	-A1 C+	
PEAK FLOW (cms) = TIME TO PEAK (hrs) = RUNOFF VOLUME (mm) = TOTAL RAINFALL (mm) = RUNOFF COEFFICIENT =	0. 76 12. 25 107. 90 108. 90 0. 99	0. 05 12. 25 64. 49 108. 90 0. 59	0. 12 103 108	ALS* 811 (iii) 2. 25 3. 56 3. 90 3. 95	
* WARNING: STORAGE COFFE	IS SMALLER THAN	TIME STEDI			

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP! Page 17

# EP POST. out

RESERVOIR (0004)					
IN= 2> OUT= 1   DT= 5.0 min	OUTFLOW (cms) 0.0000	STORAGE (ha.m.) 0.0000	OUTFLOW (cms) 0.1500		
	0. 0610 0. 0870 0. 1060	0. 0144 0. 0288	0. 1620 0. 1740 0. 1840	0. 1009 0. 1154	
	0. 1370	'	0. 1940 0. 0000	0.0000	
INFLOW : ID= 2 ( OUTFLOW: ID= 1 (	(0001) 2.2	a) (cms)	(hrs) 11 12.25	(mm)	
TI	AK FLOW REME SHIFT OF PENCENTIAL		ut/Qi n] (%) = 1 (mi n) = 1 (ha. m.) =	0. 00	
FINI CU					
FINISH ====================================	:========:			========	=======

#### Greenfield South - CPCN - 651 EP POST MISSISSAUGA POND. out \_\_\_\_\_\_ ٧ SSSSS U Α U U ٧ SS U A A L ٧ SS U U AAAAA L Т SS U U Α VV SSSSS UUUUU LLLLL 000 TTTTT TTTTT Н Н M 000 TM M Н Н MM MM Т Т 0 Н Н M M 0 0 Company 000 Τ Т Н Н Υ M 000 Seri al M Developed and Distributed by Clarifica Inc. Copyright 1996, 2007 Clarifica Inc. All rights reserved. \*\*\*\*\* DETAILED OUTPUT \*\*\*\*\* Input filename: C:\Program Files (x86)\Visual Otthymo 2.4\V02\voin.dat Output filename: C:\Users\mark.sullivan\AppData\Local\Temp\26b19c33-92b6-46d3-963b-4d66ac4f1477\Scen ari o. out Summary filename: C:\Users\mark.sullivan\AppData\Local\Temp\26b19c33-92b6-46d3-963b-4d66ac4f1477\Scen ario.sum DATE: 09/17/2012 TIME: 11:08:15 USER:

READ STORM Ptotal = 52.50 mm		ata\I 26b19	Local \Ter 9c33-92b6	k.sullivan np\ 6-46d3-969 ar SCS Typ	3b-4d66a		
TIME hrs 0.25 0.50 0.75 1.00 1.25	RAIN mm/hr 0.00 0.58 0.58 0.58	TIME hrs 6.50 6.75 7.00 7.25 7.50	RAIN mm/hr 0.94 0.94 0.94 1.26	TI ME hrs 12.75 13.00 13.25 13.50 13.75	RAIN mm/hr 7.56 3.99 3.78 2.94 2.73	TIME hrs 19.00 19.25 19.50 19.75 20.00	RAIN mm/hr 0.84 1.05 0.84 1.05 0.84

	EP	POST MIS	SI SSAUGA	POND. out			
1.50	0. 57	7. 75	1. 05	14. 00	2. 31	20. 25	1. 05
1. 75	0. 59	8.00	1. 26	14. 25	2. 10	20. 50	0. 63
2.00	0. 57	8. 25	1. 05	14. 50	1. 68	20. 75	0. 63
2. 25	0. 59	8. 50	1. 47	14. 75	1. 47	21.00	0. 63
2.50	0. 67	8. 75	1. 26	15. 00	1. 47	21. 25	0. 63
2. 75	0. 69	9.00	1. 47	15. 25	1. 68	21. 50	0. 63
3.00	0. 67	9. 25	1. 47	15. 50	1. 47	21. 75	0. 63
3. 25	0. 69	9. 50	1. 68	15. 75	1. 68	22. 00	0. 63
3. 50	0. 67	9. 75	1. 68	16. 00	1. 47	22. 25	0. 63
3. 75	0. 69	10. 00	1. 89	16. 25	1. 68	22. 50	0. 63
4. 00	0. 69	10. 25	1. 89	16. 50	0. 84	22. 75	0. 63
4. 25	0. 67	10. 50	2. 52	16. 75	1. 05	23. 00	0. 63
4. 50	0. 84	10. 75	2. 31	17. 00	0. 84	23. 25	0. 63
4. 75	0. 84	11. 00	3. 36	17. 25	1. 05	23.50	0. 63
5. 00	0. 84	11. 25	3. 15	17. 50	0. 84	23. 75	0. 63
5. 25	0. 84	11. 50	5. 04	17. 75	1. 05	24.00	0. 63
5. 50	0. 84	11. 75	5. 04	18. 00	0.84	24. 25	0. 63
5. 75	0. 84	12. 00	15. 54	18. 25	1. 05		
6.00	0.84	12. 25	64. 26	18. 50	0.84		
6. 25	0. 84	12.50	7. 56	18. 75	1. 05		

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```
CALI B
STANDHYD (0001)
| ID= 1 DT= 5.0 min
                                  Area
                                              (ha)=
                                                         2. 28
                                  Total Imp(\%) = 90.00
                                                                     Dir. Conn. (%) = 90.00
                                             I MPERVI OUS
2. 05
1. 00
                                                                  PERVIOUS (i)
0.23
5.00
      Surface Area
Dep. Storage
Average Slope
Length
                                 (ha) =
(mm) =
                                  (%)=
                                                   1.00
                                                                      2.00
                                                123.29
                                                                     40.00
                                  (m) =
                                                                     0.250
      Manni ngs n
                                                 0.013
```

		TRA	ANSFORME	D HYETOGR	APH	-	
TIME	RAIN	TIME	RAIN	' TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr	hrs	mm/hr
0. 083	0. 00	6. 167	0. 84	12. 250	64. 26	18. 33	0. 84
0. 167	0. 00	6. 250	0. 84	12. 333	7. 57	18. 42	0. 84
0. 250	0. 00	6. 333	0. 94	12. 417	7. 56	18. 50	0. 84
0. 333	0. 58	6. 417	0. 94	12. 500	7. 56	18. 58	1. 05
0. 417	0. 58	6. 500	0. 94	12. 583	7. 56	18. 67	1. 05
0. 500	0. 58	6. 583	0. 94	12. 667	7. 56	18. 75	1. 05
0. 583	0. 58	6. 667	0. 94	12. 750	7. 56	18. 83	0.84
0. 667	0. 58	6. 750	0. 94	12. 833	3. 99	18. 92	0.84
0. 750	0. 58	6.833	0. 94	12. 917	3. 99	19.00	0.84
0.833	0. 58	6. 917	0. 94	13.000	3. 99	19. 08	1.05
0. 917 1. 000	0. 58 0. 58	7.000 7.083	0. 94 0. 94	13. 083  13. 167	3. 78 3. 78	19. 17 19. 25	1. 05 1. 05
1. 083	0. 58	7. 167	0. 94	13. 167	3. 78 3. 78	19. 23	0. 84
1. 167	0. 58	7. 107	0. 95	13. 230	2. 94	19. 42	0.84
1. 250	0. 58	7. 333	1. 26	13. 417	2. 94	19. 50	0.84
1. 333	0. 57	7. 417	1. 26	13. 500	2. 94	19. 58	1. 05
1. 417	0. 57	7. 500	1. 26	13. 583	2. 73	19. 67	1. 05
1. 500	0. 57	7. 583	1. 05	13. 667	2. 73	19. 75	1. 05
1. 583	0. 59	7. 667	1. 05	13. 750	2. 73	19. 83	0.84
1. 667	0. 59	7. 750	1. 05	13. 833	2. 31	19. 92	0.84
1. 750	0. 59	7. 833	1. 26	13. 917	2. 31	20.00	0.84
1. 833	0. 57	7. 917	1. 26	14. 000	2. 31	20. 08	1. 05
			D 0				

Page 2

1. 917	11. 917 1 12. 000 1 12. 083 6	1. 05       14. 167         1. 05       14. 250         1. 05       14. 333         1. 47       14. 417         1. 47       14. 500         1. 47       14. 583         1. 26       14. 667         1. 26       14. 833         1. 47       15. 000         1. 47       15. 083         1. 47       15. 250         1. 47       15. 500         1. 47       15. 500         1. 47       15. 500         1. 68       15. 583         1. 68       15. 583         1. 68       15. 833         1. 89       16. 000         1. 89       16. 083         1. 89       16. 500         1. 89       16. 500         1. 89       16. 583         2. 52       16. 583         2. 31       16. 667         2. 31       16. 750         2. 31       16. 750         2. 31       16. 750         3. 36       17. 083         3. 15       17. 167         3. 15       17. 500         5. 04       17. 583         5. 04       17. 750 <td< th=""><th>2. 10 2. 10 1. 68 1. 68 1. 47 1. 47 1. 47 1. 68 1. 68 1. 47 1. 68 1. 68 1. 05 1. 05 1.</th><th>20. 25 20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 83 21. 42 21. 50 22. 08 22. 17 22. 25 22. 33 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 23. 30 23. 08 23. 17 23. 25 23. 33 23. 42 23. 50 23. 58 23. 67 23. 75 23. 83 23. 42 23. 50 23. 75 23. 83 23. 42 24. 00 24. 08 24. 17 24. 25</th><th>1.00.00.00.00.00.00.00.00.00.00.00.00.00</th></td<>	2. 10 2. 10 1. 68 1. 68 1. 47 1. 47 1. 47 1. 68 1. 68 1. 47 1. 68 1. 68 1. 05 1.	20. 25 20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 83 21. 42 21. 50 22. 08 22. 17 22. 25 22. 33 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 22. 50 22. 83 22. 42 23. 30 23. 08 23. 17 23. 25 23. 33 23. 42 23. 50 23. 58 23. 67 23. 75 23. 83 23. 42 23. 50 23. 75 23. 83 23. 42 24. 00 24. 08 24. 17 24. 25	1.00.00.00.00.00.00.00.00.00.00.00.00.00
Max. Eff. Inten. (mm/hr) = over (min) Storage Coeff. (min) = Unit Hyd. Tpeak (min) = Unit Hyd. peak (cms) =	64. 26 5. 00 3. 46 (i 5. 00 0. 26	30.64 10.00 i) 6.95 (ii) 10.00 0.14			
PEAK FLOW (cms) = TIME TO PEAK (hrs) = RUNOFF VOLUME (mm) = TOTAL RAINFALL (mm) = RUNOFF COEFFICIENT =	0. 36 12. 25 51. 50 52. 50 0. 98	0. 02 12. 25 20. 33 52. 50 0. 39 ge 3	0. 12 48 52	ALS* 378 (iii) 2. 25 3. 38 2. 50 0. 92	

# EP POST MISSISSAUGA POND. out

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
- CN\* = 80.0 Ia = Dep. Storage (Above)

  (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

  THAN THE STORAGE COEFFICIENT.

  (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0004)     IN= 2> OUT= 1     DT= 5.0 min	0. 0080 0. 0400	STORAGE (ha.m.) 0.0000 0.0650 0.0720 0.1440	OUTFLOW (cms) 0.0690 0.0790 0.0890 0.0900		
INFLOW: ID= 2 (00 OUTFLOW: ID= 1 (00	(h 01) 2.	280 0. 3	TPEAK (hrs) 78 12.25 33 12.83	(mm)	
TIME	FLOW R SHIFT OF P MUM STORAG	EAK FLOW	ut/Qin](%)= (min)= 3 (ha.m.)=	35. 00	
**************************************	2 **				

READ STORM	Filename:	<pre>C: \Users\mark. sullivan\AppD ata\Local \Temp\</pre>

26b19c33-92b6-46d3-963b-4d66ac4f1477\7d647cf8
Comments: 24-Hour 5-Year SCS Type II Storm Sarnia

Ptotal = 67.60 mm

```
EP POST MISSISSAUGA POND. out 08 | 11.50 | 6.49 | 17.75 | 08 | 11.75 | 6.49 | 18.00
5. 25
              1.08
                                                                       1.35
                                                                                    24.00
                                                                                                    0.81
                                                       18. 00
18. 25
18. 50
                                                                       1. 08
1. 35
1. 08
5.50
              1.08
                                                                                    24. 25
                                                                                                    0.81
                                         20. 01
82. 74
9. 73
                          12. 00
12. 25
5.75
              1.08
6.00
              1.08
6. 25
                        12. 50
                                                      18. 75
                                                                       1.35
              1.08
```

\_\_\_\_\_

```
CALI B
 STANDHYD (0001)
                               (ha) = 2.28
                        Area
                        Total Imp(\%) = 90.00
ID= 1 DT= 5.0 min
                                                  Dir. Conn. (\%) = 90.00
                                I MPERVI OUS
                                                PERVIOUS (i)
    Surface Area
                        (ha) =
                                     2.05
                                                   0. 23
    Dep. Storage
Average SI ope
                                     1.00
                                                   5.00
                        (mm) =
                         (%)=
                                                   2.00
                                    1. 00
                                                  40.00
    Length
                         (m) =
                                   123. 29
    Manni ngs n
                                                  0.250
                                   0.013
```

TI ME hrs 0. 083 0. 167 0. 250 0. 333 0. 417 0. 500 0. 583 0. 667 0. 750 0. 833 0. 917 1. 000 1. 083 1. 167 1. 250 1. 333 1. 417 1. 500 1. 583 1. 667	RAIN mm/hr 0.00 0.00 0.00 0.74 0.74 0.74 0.74 0.74	TIME hrs 6. 167 6. 250 6. 333 6. 417 6. 500 6. 583 6. 667 6. 750 6. 833 6. 917 7. 000 7. 083 7. 167 7. 250 7. 333 7. 417 7. 500 7. 583 7. 667 7. 750	RAI N mm/hr 1. 08 1. 08 1. 22 1. 22 1. 22 1. 22 1. 22 1. 22 1. 22 1. 22 1. 25 1. 62 1. 62 1. 65 1. 35 1. 35 1. 35	D HYETOGR	RAIN mm/hr 82.74 9.74 9.73 9.73 9.73 9.73 5.14 5.14 4.87 4.87 4.87 3.79 3.79 3.52 3.52 2.97	TI ME hrs 18. 33 18. 42 18. 50 18. 58 18. 67 18. 75 18. 83 18. 92 19. 00 19. 08 19. 17 19. 25 19. 33 19. 42 19. 50 19. 58 19. 67 19. 75 19. 83 19. 92	RAIN mm/hr 1. 08 1. 08 1. 35 1. 35 1. 35 1. 35 1. 35 1. 35 1. 35 1. 35 1. 35 1. 35 1. 08 1. 35 1. 35 1. 08 1. 35 1
1. 750 1. 833 1. 917 2. 000 2. 083 2. 167 2. 250 2. 333 2. 417 2. 500 2. 583 2. 667 2. 750 2. 833 2. 917 3. 000 3. 083	0. 76 0. 73 0. 73 0. 73 0. 76 0. 76 0. 76 0. 87 0. 87 0. 89 0. 89 0. 89 0. 89 0. 87 0. 87 0. 87	7.833 7.917 8.000 8.083 8.167 8.250 8.333 8.417 8.500 8.583 8.667 8.750 8.833 8.917 9.000 9.083 9.167	1. 62 1. 62 1. 35 1. 35 1. 35 1. 89 1. 89 1. 62 1. 62 1. 62 1. 89 1. 89 1. 89	13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 500 14. 583 14. 667 14. 750 14. 833 14. 917 15. 000 15. 083 15. 167 15. 250	2. 97 2. 97 2. 70 2. 70 2. 16 2. 16 2. 16 1. 89 1. 89 1. 89 1. 89 2. 16 2. 16 2. 16	20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33	1. 08 1. 35 1. 35 0. 81 0. 81

Page 5

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EP POST MISSISSAUGA POND. out
                                      9. 250
                                                                     1.89
                              0.89
                                                 1.89
                   3. 167
                                                        |15. 333
                                                                              21.42
                                                                                         0.81
                   3. 250
                              0.89
                                      9.333
                                                 2. 16
                                                         15.417
                                                                     1.89
                                                                              21.50
                                                                                         0.81
                   3.333
                                      9. 417
                                                 2.16
                                                         15.500
                                                                              21.58
                              0.87
                                                                     1.89
                                                                                         0.81
                                                 2.16
                                                                     2.16
                   3.417
                              0.87
                                      9.500
                                                         15.583
                                                                              21. 67
                                                                                         0.81
                   3.500
                              0.87
                                      9. 583
                                                 2.16
                                                         15.667
                                                                     2.16
                                                                              21.75
                                                                                         0.81
                   3.583
                              0.89
                                      9. 667
                                                 2.16
                                                         15.750
                                                                     2.16
                                                                              21.83
                                                                                         0.81
                                                 2.16
                   3.667
                              0.89
                                      9.750
                                                         15.833
                                                                     1.89
                                                                              21. 92
                                                                                         0.81
                   3.750
                                      9.833
                                                 2.43
                                                         15. 917
                              0.89
                                                                     1.89
                                                                              22.00
                                                                                         0.81
                   3.833
                              0.89
                                      9. 917
                                                 2.43
                                                         16.000
                                                                     1.89
                                                                              22.08
                                                                                         0.81
                                                 2. 43
2. 43
                                                         16.083
                                                                              22. 17
22. 25
                   3.917
                              0.89
                                     10.000
                                                                     2.16
                                                                                        0.81
                                                                     2. 16
                   4.000
                              0.89
                                     10.083
                                                         16. 167
                                                                                         0.81
                                                         16. 250
16. 333
                   4.083
                                                  2.43
                                                                     2.16
                                                                              22.33
                              0.87
                                     10. 167
                                                                                         0.81
                                                 2. 43
                   4. 167
                              0.87
                                     10.250
                                                                              22. 42
                                                                     1.08
                                                                                         0.81
                   4. 250
                                                 3.24
                              0.87
                                     10.333
                                                         16.417
                                                                     1.08
                                                                              22.50
                                                                                        0.81
                   4.333
                              1.08
                                     10.417
                                                 3.24
                                                         16.500
                                                                     1.08
                                                                              22. 58
                                                                                         0.81
                                                 3. 24
                                                         16.583
                                                                     1.35
                                                                              22.67
                   4.417
                             1.08
                                     10.500
                                                                                         0.81
                   4.500
                             1. 08
                                                 2. 97
                                                         16.667
                                                                     1. 35
                                     10. 583
                                                                              22. 75
                                                                                         0.81
                                                 2.97
                   4.583
                              1.08
                                     10.667
                                                         16.750
                                                                     1.35
                                                                              22.83
                                                                                         0.81
                   4.667
                                                                     1.08
                                                 2.97
                              1.08
                                     10.750
                                                         16.833
                                                                              22. 92
                                                                                         0.81
                                                 4. 33
4. 33
4. 33
                   4.750
                              1.08
                                     10.833
                                                         16. 917
                                                                     1.08
                                                                              23.00
                                                                                         0.81
                                                         17.000
                   4.833
                              1.08
                                     10. 917
                                                                     1.08
                                                                              23.08
                                                                                         0.81
                                                         17.083
                   4.917
                              1.08
                                     11.000
                                                                     1.35
                                                                              23. 17
                                                                                         0.81
                   5.000
                                                         17. 167
                              1.08
                                     11.083
                                                 4.06
                                                                     1.35
                                                                              23.25
                                                                                         0.81
                                     11. 167
                   5.083
                              1.08
                                                 4.06
                                                         17.250
                                                                     1.35
                                                                              23.33
                                                                                         0.81
                                     11.250
                   5. 167
                              1.08
                                                 4.06
                                                         17.333
                                                                     1.08
                                                                              23.42
                                                                                         0.81
                   5. 250
                             1. 08
                                     11. 333
                                                         17. 417
                                                 6. 49
                                                                     1.08
                                                                              23.50
                                                                                         0.81
                                                 6. 49
                                                         17.500
                   5.333
                             1.08
                                     11. 417
                                                                     1.08
                                                                              23.58
                                                                                        0.81
                                                 6. 49
                                                                     1. 35
1. 35
                   5.417
                                     11.500
                                                         17.583
                                                                              23. 67
                              1.08
                                                                                         0.81
                   5.500
                              1.08
                                     11.583
                                                 6. 49
                                                         17.667
                                                                              23.75
                                                                                         0.81
                                                         17.750
                                                 6.49
                   5.583
                              1.08
                                     11. 667
                                                                     1.35
                                                                              23.83
                                                                                         0.81
                                                 6. 49
                                     11.750
                                                         17. 833
                   5.667
                              1.08
                                                                     1.08
                                                                              23. 92
                                                                                        0.81
                                                                              24.00
                   5.750
                              1.08
                                     11.833
                                                20.01
                                                         17. 917
                                                                     1.08
                                                                                        0.81
                                                         18.000
                   5.833
                             1.08
                                     11. 917
                                                20.01
                                                                     1.08
                                                                              24.08
                                                                                        0.81
                   5. 917
                             1.08
                                     12.000
                                                20.01
                                                         18.083
                                                                    1. 35
                                                                              24. 17
                                                                                        0.81
                   6.000
                              1.08
                                     12. 083
                                                82.73
                                                         18. 167
                                                                    1. 35
                                                                              24. 25
                                                                                         0.81
                                                82. 74 | 18. 250
                   6.083
                             1. 08 | 12. 167
                                                                     1. 35
                                  82. 74 46. 67

5. 00 10. 00

3. 12 (ii) 6. 29

5. 00 10. 00

0. 27 0. 15
     Max. Eff. Inten. (mm/hr)=
                   over (min)
     Storage Coeff.
                         (min) =
                                                        6.29 (ii)
     Unit Hyd. Tpeak (min)=
     Unit Hyd. peak (cms)=
                                                                       *TOTALS*
                         (cms) = 0.47
(hrs) = 12.25
(mm) = 66.60
(mm) = 67.60
ENT = 0.99
                                               0. 02
12. 25
31. 08
67. 60
     PEAK FLOW
                                                                         0.493 (iii)
     TIME TO PEAK
                                                                          12. 25
     RUNOFF VOLUME
                                                                         63.05
     TOTAL RAINFALL
                                                                          67.60
     RUNOFF COEFFICIENT =
                                                                          0.93
                                                        0.46
**** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
        (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
     CN* = 80.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

RESERVOIR (0004) **STORAGE** (ha. m.)

```
EP POST MISSISSAUGA POND. out
                                         0.0000
                             0.0000
                                                         0.0690
                                                                       0. 2160
                                                                       0. 2880
                             0.0080
                                          0.0650
                                                         0.0790
                                                         0.0890
                             0.0400
                                          0.0720
                                                                       0.3610
                                          0.1440
                                                         0.0900
                             0.0560
                                                                       0.3740
                                    AREA
                                              OPEAK
                                                          TPEAK
                                                                        R. V.
                                                          (hrs)
12.25
                                               (cms)
                                    (ha)
                                                                        (mm)
    INFLOW: ID= 2 (0001)
OUTFLOW: ID= 1 (0004)
                                                 0. 493
                                                                         63. 05
                                    2. 280
                                    2.280
                                                 0.044
                                                            12.83
                                                                         62.14
                     PEAK FLOW REDUCTION TIME SHIFT OF PEAK FLOW
                                    REDUCTION [Qout/Qin](%) = 8.87

PEAK FLOW (min) = 35.00

AGE USED (ha.m.) = 0.0889
                     MAXIMUM STORAGE
 *******
 ** SIMULATION NUMBER: 3 **
                           Filename: C:\Users\mark.sullivan\AppD
    READ STORM
                                      ata\Local \Temp\
                                      26b19c33-92b6-46d3-963b-4d66ac4f1477\1d16d696
                          Comments: 24-Hour 10-Year SCS Type II Storm Sarnia
 Ptotal = 77.60 mm
                  TIME
                            RAIN
                                     TIME
                                              RAIN | '
                                                         TIME
                                                                  RAIN
                                                                           TI ME
                                                                                     RAIN
                   hrs
                           mm/hr
                                      hrs
                                             mm/hr
                                                          hrs
                                                                 mm/hr
                                                                            hrs
                                                                                    mm/hr
                                                                        19.00
                                                      12.75
                   0.25
                            0.00
                                     6.50
                                              1.40
                                                                11. 17
                                                                                    1.24
                                                                         19. 25
                                                                 5.90
                  0.50
                            0.85
                                     6.75
                                              1.40
                                                      13.00
                                                                                    1.55
                                                                         19.50
                                                      13. 25
                                                                                    1.24
                  0.75
                            0.85
                                     7.00
                                              1.40
                                                                 5.59
                   1.00
                                                      13.50
                                                                         19.75
                                                                                   1.55
                            0.85
                                     7.25
                                              1.40
                                                                 4.35
                   1.25
                            0.85
                                     7.50
                                              1.86
                                                      13.75
                                                                 4.04
                                                                         20.00
                                                                                   1.24
                   1.50
                            0.84
                                     7.75
                                                      14.00
                                                                 3.41
                                                                         20.25
                                                                                   1.55
                                              1.55
                   1.75
                            0.87
                                     8.00
                                                      14. 25
                                                                 3.10
                                                                         20.50
                                                                                   0.93
                                              1.86
                   2.00
                            0.84
                                     8.25
                                              1.55
                                                      14.50
                                                                 2.48
                                                                         20.75
                                                                                   0.93
                  2. 25
2. 50
2. 75
                                     8. 50
8. 75
                                                                 2. 17
2. 17
                                                                         21. 00
21. 25
                            0.87
                                              2.17
                                                       14.75
                                                                                   0.93
                            0.99
                                              1.86
                                                                                    0.93
                                                       15.00
                            1.02
                                                                 2.48
                                                                         21.50
                                     9.00
                                                      15.25
                                                                                   0.93
                                              2.17
                   3.00
                            0.99
                                     9.25
                                              2.17
                                                      15.50
                                                                 2.17
                                                                         21.75
                                                                                   0.93
                            1.02
                   3.25
                                     9.50
                                              2.48
                                                      15.75
                                                                 2.48
                                                                         22.00
                                                                                   0.93
                                     9.75
                   3.50
                            0.99
                                              2.48
                                                      16.00
                                                                 2.17
                                                                         22.25
                                                                                   0.93
                                                                 2.48
                   3.75
                            1.02
                                              2.79
                                                                                   0.93
                                    10.00
                                                      16. 25
                                                                         22.50
                   4.00
                            1.02
                                    10.25
                                              2.79
                                                      16. 50
                                                                 1.24
                                                                         22.75
                                                                                   0.93
                   4.25
                            0.99
                                    10.50
                                              3.72
                                                                         23.00
                                                      16. 75
                                                                 1.55
                                                                                   0.93
                            1. 24
1. 24
                                                      17. 00
17. 25
                   4.50
                                    10.75
                                              3.41
                                                                         23.25
                                                                                   0.93
                                                                 1.24
                   4.75
                                              4.97
                                    11.00
                                                                 1.55
                                                                         23.50
                                                                                   0.93
                                                      17. 50
17. 75
                                    11. 25
11. 50
                   5.00
                            1.24
                                                                         23.75
                                                                 1.24
                                                                                   0.93
                                              4.66
                            1. 24
                   5.25
                                              7.45
                                                                 1.55
                                                                         24.00
                                                                                   0.93
                                   11. 75
                   5.50
                            1.24
                                              7.45
                                                      18.00
                                                                 1.24
                                                                         24.25
                                                                                   0.93
                   5.75
                                             22.97
                            1.24
                                    12.00
                                                      18. 25
                                                                 1.55
                                             94.98
                   6.00
                            1. 24
                                    12. 25
                                                      18.50
                                                                 1.24
                   6. 25
                            1. 24
                                   12.50
                                             11. 17
                                                      18. 75
                                                                 1.55
 CALIB
 STANDHYD (0001)
                         Area
                                   (ha) = 2.28
                         Total Imp(\%) = 90.00
ID= 1 DT= 5.0 min
                                                    Dir. Conn. (\%) = 90.00
                                 I MPERVI OUS
                                                  PERVIOUS (i)
```

Surface Area

(ha) =

2.05

Page 7

0.23

EP POST MISSISSAUGA POND. out

Dep. Storage	(mm)=	1. 00	5. 00
Average Slope	(%)=	1. 00	2.00
Length	(m) =	123. 29	40.00
Manni ngs n	=	0. 013	0. 250

		TD		N UVETACA	۸DU		
TIME hrs 0.083 0.167 0.250 0.333 0.417 0.500 0.583	RAIN mm/hr 0.00 0.00 0.00 0.85 0.85	TIME hrs 6. 167 6. 250 6. 333 6. 417 6. 500 6. 583	RAIN MM/hr 1.24 1.40 1.40 1.40	D HYETOGR   TI ME   hrs   12. 250   12. 333   12. 417   12. 500   12. 583   12. 667   12. 750	APH RAIN mm/hr 94.98   11.19 11.17 11.17 11.17 11.17	TI ME hrs 18. 33 18. 42 18. 50 18. 58 18. 67 18. 75 18. 83	RAIN mm/hr 1.24 1.24 1.55 1.55 1.55
0. 667 0. 750 0. 833 0. 917 1. 000 1. 083 1. 167 1. 250 1. 333 1. 417 1. 500	0. 85 0. 85 0. 85 0. 85 0. 85 0. 85 0. 85 0. 85 0. 84 0. 84	6. 667 6. 750 6. 833 6. 917 7. 000 7. 083 7. 167 7. 250 7. 333 7. 417 7. 500 7. 583	1. 40 1. 40 1. 40 1. 40 1. 40 1. 40 1. 40 1. 86 1. 86 1. 86	12. 833 12. 917 13. 000 13. 083 13. 167 13. 250 13. 333 13. 417 13. 500 13. 583 13. 667	5. 90 5. 90 5. 90 5. 59 5. 59 5. 59 4. 35 4. 35 4. 35 4. 04	18. 92 19. 00 19. 08 19. 17 19. 25 19. 33 19. 42 19. 50 19. 58 19. 67 19. 75	1. 24 1. 24 1. 55 1. 55 1. 24 1. 24 1. 25 1. 55 1. 55
1. 583 1. 667 1. 750 1. 833 1. 917 2. 000 2. 083 2. 167 2. 250 2. 333 2. 417	0. 87 0. 87 0. 84 0. 84 0. 84 0. 87 0. 87 0. 87 0. 99 0. 99	7. 667 7. 750 7. 833 7. 917 8. 000 8. 083 8. 167 8. 250 8. 333 8. 417 8. 500	1. 55 1. 55 1. 86 1. 86 1. 55 1. 55 1. 55 2. 17 2. 17	13. 750 13. 833 13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 500 14. 583	4. 04 3. 41 3. 41 3. 10 3. 10 3. 10 2. 48 2. 48 2. 48 2. 17	19. 83 19. 92 20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 20. 58 20. 67	1. 24 1. 24 1. 55 1. 55 1. 55 0. 93 0. 93 0. 93 0. 93
2. 500 2. 583 2. 667 2. 750 2. 833 2. 917 3. 000 3. 083 3. 167 3. 250 3. 333 3. 417	0. 99 1. 02 1. 02 1. 02 0. 99 0. 99 1. 02 1. 02 1. 02 0. 99 0. 99	8. 583 8. 667 8. 750 8. 833 8. 917 9. 000 9. 083 9. 167 9. 250 9. 333 9. 417 9. 500	1. 86 1. 86 1. 86 2. 17 2. 17 2. 17 2. 17 2. 17 2. 48 2. 48 2. 48	14. 667 14. 750 14. 833 14. 917 15. 000 15. 083 15. 167 15. 250 15. 333 15. 417 15. 500 15. 583	2. 17 2. 17 2. 17 2. 17 2. 17 2. 48 2. 48 2. 48 2. 17 2. 17 2. 17 2. 48	20. 75 20. 83 20. 92 21. 00 21. 08 21. 17 21. 25 21. 33 21. 42 21. 50 21. 58 21. 67	0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93
3.500 3.583 3.667 3.750 3.833 3.917 4.000 4.083 4.167 4.250 4.333	0. 99 1. 02 1. 02 1. 02 1. 02 1. 02 0. 99 0. 99 0. 99 1. 24	9. 583 9. 667 9. 750 9. 833 9. 917 10. 000 10. 083 10. 167 10. 250 10. 333 10. 417	2. 48 2. 48 2. 79 2. 79 2. 79 2. 79 2. 79 2. 79 2. 79 3. 72 3. 72	15. 667 15. 750 15. 833 15. 917 16. 000 16. 083 16. 167 16. 250 16. 333 16. 417 16. 500	2. 48 2. 48 2. 17 2. 17 2. 17 2. 48 2. 48 2. 48 1. 24 1. 24 1. 24	21. 75 21. 83 21. 92 22. 00 22. 08 22. 17 22. 25 22. 33 22. 42 22. 50 22. 58	0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93 0. 93
			Page 8				

```
EP POST MISSISSAUGA POND. out
                                                 16.583
            4.417
                       1. 24
                              10.500
                                          3.72
                                                            1.55
                                                                    22. 67
                                                                               0.93
            4.500
                       1.24
                              10.583
                                          3.41
                                                 16.667
                                                            1.55
                                                                    22.75
                                                                               0.93
                       1. 24
1. 24
                                                            1. 55
1. 24
                                                                     22.83
                                                                               0.93
            4.583
                              10.667
                                          3.41
                                                 16.750
                                                                               0.93
                                                                     22.92
            4.667
                              10.750
                                          3.41
                                                 16.833
                                          4.97
                       1.24
                                                                               0.93
            4.750
                              10.833
                                                 16.917
                                                            1.24
                                                                     23.00
            4.833
                       1.24
                              10.917
                                          4.97
                                                 17.000
                                                            1.24
                                                                     23.08
                                                                               0.93
                                          4.97
            4.917
                       1.24
                              11.000
                                                 17.083
                                                            1.55
                                                                    23.17
                                                                               0.93
            5.000
                                                            1.55
                       1.24
                              11.083
                                          4.66
                                                                    23.25
                                                                               0.93
                                                 17. 167
                                                                               0.93
            5.083
                       1.24
                              11. 167
                                         4.66
                                                 17.250
                                                            1.55
                                                                    23.33
            5.167
                       1.24
                              11. 250
                                          4.66
                                                 17.333
                                                            1.24
                                                                    23.42
                                                                               0.93
                       1.24
             5.250
                              11.333
                                          7.45
                                                 17.417
                                                            1.24
                                                                    23.50
                                                                               0.93
                       1. 24
1. 24
                                                 17.500
            5.333
                                          7.45
                                                            1.24
                              11.417
                                                                     23.58
                                                                               0.93
                                                 17. 583
                                          7.45
                                                            1.55
                                                                               0.93
            5.417
                              11.500
                                                                     23.67
                       1.24
            5.500
                              11.583
                                         7.45
                                                 17.667
                                                            1.55
                                                                    23.75
                                                                               0.93
                       1.24
            5.583
                              11.667
                                         7.45
                                                 17.750
                                                            1.55
                                                                    23.83
                                                                               0.93
                              11.750
                                         7.45
                                                 17.833
             5.667
                       1. 24
                                                            1.24
                                                                     23.92
                                                                               0.93
            5.750
                       1.24
                                        22.97
                                                 17.917
                                                            1.24
                                                                     24.00
                                                                               0.93
                              11.833
            5.833
                                                            1.24
                       1.24
                              11.917
                                        22.97
                                                 18.000
                                                                    24.08
                                                                               0.93
                              12.000
                                                                    24. 17
24. 25
                                                                               0.93
            5.917
                                        22.97
                                                 18.083
                                                            1.55
                       1.24
                                        94.97
            6.000
                       1.24
                              12.083
                                                 18. 167
                                                            1.55
                                                                               0.93
                                        94.98
            6.083
                       1.24
                              12. 167
                                                18. 250
                                                            1.55
                                94.98
Max. Eff. Inten. (mm/hr)=
                                                57.97
            over
                  (mi n)
                                 5.00
                                                10.00
                                 2.96 (ii)
                                                5.95 (ii)
Storage Coeff.
                   (min) =
                                                10.00
Uni t Hyd. Tpeak
                  (min) =
                                 5.00
Unit Hyd. peak
                  (cms) =
                                 0.28
                                                0.15
                                                               *TOTALS*
PEAK FLOW
                   (cms) =
                                 0.54
                                                0.03
                                                                 0.569 (iii)
                                               12. 25
38. 73
TIME TO PEAK
                   (hrs) =
                                12.25
                                                                 12.25
RUNOFF VOLUME
                                                                 72.81
                                76.60
                    (mm) =
TOTAL RAINFALL
                    (mm) =
                                77.60
                                               77.60
                                                                 77.60
RUNOFF COEFFICIENT
                                 0.99
                                                0.50
                                                                  0.94
```

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (Above)
- $CN^* = 80.0$  I a = Dep. Storage (Above TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORÁGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0004)     IN= 2> OUT= 1					
DT= 5.0 min	OUTFLOW	STORAGE	OUTFL	LOW STORAGE	
	(cms)	(ha.m.)	(cms	s) (ha.m.)	
	Ó. 00Ó0	0.0000	0.06	90	)
	0.0080	0.0650	0.07	'90 0. 2880	)
	0.0400	0.0720	0.08	390 0. 3610	)
	0.0560	0. 1440	0.09	0. 3740	)
			'		
	AF	rea qpi	EAK TPE	EAK R. V.	
	(1	na) (cr	ns) (hr	rs) (mm)	
INFLOW : ID= 2		280 (	). 569	2. 25 · 72. 8	1
OUTFLOW: ID= 1	(0004) 2.	280 (	0. 047 1	2. 83 71. 9	1
	` '				
Р	EAK FLOW F	REDUCTI ON	[Qout/Qi n] (	(%) = 8. 22	
Т	IME SHIFT OF F	PEAK FLOW		n) = 35.00	
M	AXIMUM STORAC	GE USED	(ha. m	ı. )=       0. 1027	

#### EP POST MISSISSAUGA POND. out

\*\*\*\*\*\* \*\* SIMULATION NUMBER: 4 \*\*

6. 25

1. 44

READ STORM Filename: C:\Users\mark.sullivan\AppD ata\Local\Temp\ 26b19c33-92b6-46d3-963b-4d66ac4f1477\6b7e5e22 Ptotal = 90.20 mm | Comments: 24-Hour 25-Year SCS Type II Storm Sarnia TIME RAIN TIME RAIN | ' TIME RAIN TI ME hrs mm/hr hrs mm/hr hrs mm/hr hrs mm/hr 0.00 6.50 12. 75 12. 99 19.00 0.25 1. 62 1.44 6.75 6. 86 0.50 0.99 1. 62 13.00 19. 25 1.80 0.75 0.99 13. 25 6.49 19.50 1.44 7.00 1. 62 0.99 5.05 1.80 1.00 7. 25 13.50 1. 62 19. 75 0.99 7.50 1.44 1.25 2. 16 13. 75 4. 69 20.00 14. 00 14. 25 3.97 1.50 0.97 7.75 1.80 20.25 1.80 1.75 20. 50 20. 75 1.01 8.00 2.16 3.61 1.08 2.00 0.97 8. 25 1.80 14.50 2.89 1.08 2. 25 8.50 2.53 1.01 2.53 14. 75 21.00 1. 08

2.50 8.75 1.15 2.16 15.00 2.53 21.25 1.08 2.75 2.53 2.89 1. 19 9.00 15. 25 21.50 1.08 3.00 1. 15 9. 25 2.53 15. 50 2.53 21.75 1.08 3.25 1. 19 9.50 2.89 15. 75 2.89 22.00 1. 08 3.50 22. 25 1. 15 9.75 2.89 16.00 2.53 1.08 10.00 16. 25 22.50 3.75 3. 25 1. 19 2.89 1.08 3.25 16.50 4.00 1.19 10.25 1.44 22.75 1.08 16. 75 17. 00 1. 08 4.25 23.00 1.15 10.50 4.33 1.80 1.08 10.75 3.97 23.25 4.50 1.44 1.44 4.75 11.00 5. 77 17. 25 1.80 23.50 1. 08 1.44 1.08 5.00 1.44 11. 25 5. 41 17.50 1.44 23.75 5.25 11.50 1.80 24.00 1.08 1.44 8. 66 17. 75 5.50 1.44 18.00 1.44 24.25 11. 75 8. 66 1.08 5.75 1.44 12.00 26. 70 18. 25 1.80 12. 25 12. 50 18. 50 18. 75 6.00 110. 40 12. 99 1.44 1.44

1.80

CALIB STANDHYD (0001) ID= 1 DT= 5.0 min	Area Total	(ha)= Imp(%)=	2. 28 90. 00	Dir. Conn.(%)=	90.00
Surface Area Dep. Storage Average SI ope Length Manni ngs n	(ha) = (mm) = (%) = (m) = =	I MPERVI ( 2. 0! 1. 00 1. 00 123. 29 0. 01:	5 ) ) 9	PERVIOUS (i) 0. 23 5. 00 2. 00 40. 00 0. 250	

		TRA	ANSFORME	D HYETOGI	RAPH		
TIME	RAIN	TIME	RAIN	' TIME	RAI N	TIME	RAI N
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr	hrs	mm/hr
0. 083	0.00	6. 167	1. 44	12. 250	110. 40	18. 33	1. 44
0. 167	0.00	6. 250	1. 44	12. 333	13. 00	18. 42	1. 44
0. 250	0.00	6. 333	1. 62	12. 417	12. 99	18. 50	1. 44
0. 333	0. 99	6. 417	1. 62	12. 500	12. 99	18. 58	1. 80
		F	Page 10	•			

	0. 500 0. 583 0. 667 0. 750 0. 833 0. 917 1. 000 1. 083 1. 167 1. 250 1. 333 1. 417 1. 500 1. 583 1. 667 1. 750 2. 083 2. 167 2. 083 2. 167 2. 250 2. 833 2. 917 3. 000 3. 083 3. 167 3. 250 3. 333 3. 417 3. 500 4. 083 4. 167 4. 250 3. 833 3. 417 4. 500 4. 333 4. 167 4. 250 5. 083 5. 167 5. 250 5. 333 5. 417 5. 500
	0.000.000.000.000.000.000.000.000.000.
	POST MI 6. 500 6. 583 6. 667 6. 583 7. 167 7. 000 7. 083 7. 167 7. 333 7. 417 7. 500 7. 833 7. 917 8. 000 8. 083 8. 167 8. 250 8. 333 8. 450 8. 833 8. 750 8. 833 8. 750 9. 000 9. 167 9. 250 9. 833 9. 750 9. 833 10. 167 10. 583 10. 667 10. 583 11. 500 11. 333 11. 500 11. 583 11. 500 11. 583 11. 667
Page 11	
	POND. ou 12. 583 12. 667 12. 750 12. 833 13. 167 13. 000 13. 083 13. 167 13. 583 13. 417 13. 500 13. 833 13. 417 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 583 14. 417 15. 000 15. 333 15. 167 15. 250 15. 333 15. 417 15. 500 15. 833 16. 167 17. 15. 500 16. 167 16. 583 17. 16. 000 16. 583 17. 16. 000 16. 583 17. 16. 000 17. 083 17. 16. 000 17. 083 17. 16. 000 17. 083 17. 16. 500 17. 000 17. 083 17. 16. 750 17. 250 17. 333 17. 16. 750 17. 333 17. 16. 750 17. 750 17. 750 17. 750 17. 750 17. 750
,	t 12.2.9.86.66.49.97.71.11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
	18. 67 18. 75 18. 83 18. 92 19. 00 19. 17 19. 25 19. 42 19. 50 19. 58 19. 67 19. 83 19. 92 20. 08 20. 17 20. 23 20. 58 20. 58 20. 58 20. 58 20. 58 21. 67 21. 83 21. 67 21. 83 21. 75 21. 83 22. 23. 33 22. 25 22. 25 22. 33 22. 25 22. 33 22. 25 22. 33 23. 67 24. 25 25. 26 26. 27 27 28. 28 28. 28 29. 28 29. 28 29. 28 29. 28 29. 28 29. 28 29. 29. 29 29. 29. 29. 29. 29. 29. 29. 29. 29. 29.
	1. 80 1. 80 1. 44 1. 44 1. 80 1. 80 1. 80 1. 44 1. 44 1. 80

1.99

```
EP POST MISSISSAUGA POND. out
                5.667
                         1.44
                               11. 750
                                         8. 66 | 17. 833
                                                           1.44
                                                                  23.92
                                                                           1.08
                5.750
                         1.44
                                11.833
                                         26.70
                                                17.917
                                                           1.44
                                                                  24.00
                                                                           1.08
                                                18.000
                5.833
                         1.44
                                11.917
                                         26.70
                                                           1.44
                                                                  24.08
                                                                           1.08
                         1.44
                                         26.70
                5.917
                               12.000
                                                18. 083
                                                                  24. 17
                                                           1.80
                                                                           1.08
                6.000
                         1.44
                               12.083
                                        110.39
                                                18. 167
                                                           1.80
                                                                  24. 25
                                                                           1.08
                6.083
                         1.44
                               12. 167
                                        110. 40 | 18. 250
                                                           1.80
                                110.40
                                               72.74
    Max. Eff. Inten. (mm/hr)=
                                  5.00
                over (min)
                                               10.00
    Storage Coeff.
                     (mi n) =
                                  2.78 (ii)
                                                5.60 (ii)
                                5. 00
    Unit Hyd. Tpeak (min) = Unit Hyd. peak (cms) =
                                               10.00
                                                0.15
                                  0. 28
                                                             *TOTALS*
    PEAK FLOW
                                                0.04
                                                               0.666 (iii)
                     (cms) =
                                  0.63
    TIME TO PEAK
                     (hrs)=
                                 12. 25
                                               12. 25
                                                               12.25
                      (mm) =
    RUNOFF VOLUME
                                               48.82
                                 89. 20
                                                               85. 16
                                  90. 20
                                                               90.20
                                               90. 20
    TOTAL RAINFALL
                      (mm) =
    RUNOFF COEFFICIENT
                                  0.99
                                                0.54
                                                                0.94
***** WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!
       (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
      THAN THE STORÁGE COEFFICIENT.
     (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

RESERVOIR (0004) | IN= 2---> OUT= 1 DT= 5.0 min OUTFLOW OUTFLOW STORAGE **STORAGE** (cms) (ha. m.) (cms) (ha. m.) 0.0000 0.0690 0.2160 0.0000 0.0790 0.0080 0.0650 0. 2880 0.0400 0.0720 0.0890 0.3610 0.0560 0. 1440 0.0900 0.3740 QPEAK **TPEAK** AREA R. V. (ha) (cms) (hrs) (mm) INFLOW: ID= 2 (0001) 2. 280 0.666 12. 25 85. 16 OUTFLOW: ID= 1 (0004) 2.280 0.051 12.83 84.26

PEAK FLOW REDUCTION [Qout/Qin](%) = 7.63 TIME SHIFT OF PEAK FLOW (min) = 35.00 MAXIMUM STORAGE USED (ha. m.) = 0.1208

\*\*\*\*\*\*\*\*

\*\* SIMULATION NUMBER: 5 \*\*

0.50

1. 10

READ STORM | Filename: C:\Users\mark.sullivan\AppD ata\Local\Temp\ 26b19c33-92b6-46d3-963b-4d66ac4f1477\a1e5d969 Comments: 24-Hour 50-Year SCS Type II Storm Sarnia Ptotal = 99.60 mm RAIN | nm/hr | TIME RAIN TIME TIME RAIN I nm/hr | hrs mm/hr | hrs 1.79 | 12.75 | 14.34 | 19.00 1.79 | 13.00 | 7.57 | 19.25 mm/hr mm/hr hrs hrs mm/hr 6.50 0.00 1. 79 0.25 1. 59

6.75

	EP	POST MIS	SSI SSAUGA	POND. out			
0. 75	1. 10	7.00	1. 79	13. 25	7. 17	19. 50	1. 59
1. 00	1. 10	7. 25	1. 79	13. 50	5. 58	19. 75	1. 99
1. 25	1. 10	7. 50	2. 39	13. 75	5. 18	20.00	1. 59
1. 50	1. 08	7. 75	1. 99	14. 00	4. 38	20. 25	1. 99
1. 75	1. 12	8. 00	2. 39	14. 25	3. 98	20. 50	1. 20
2. 00	1. 08	8. 25	1. 99	14. 50	3. 19	20. 75	1. 20
2. 25	1. 12	8. 50	2. 79	14. 75	2. 79	21. 00	1. 20
2. 50	1. 27	8. 75	2. 39	15. 00	2. 79	21. 25	1. 20
2. 75	1. 31	9. 00	2. 79	15. 25	3. 19	21. 50	1. 20
3. 00	1. 27	9. 25	2. 79	15. 50	2. 79	21. 75	1. 20
3. 25	1. 31	9. 50	3. 19	15. 75	3. 19	22. 00	1. 20
3. 50	1. 27	9. 75	3. 19	16. 00	2. 79	22. 25	1. 20
3. 75	1. 31	10.00	3. 59	16. 25	3. 19	22. 50	1. 20
4.00	1. 31	10. 25	3. 59	16. 50	1. 59	22. 75	1. 20
4. 25	1. 27	10.50	4. 78	16. 75	1. 99	23.00	1. 20
4. 50	1. 59	10.75	4. 38	17. 00	1. 59	23. 25	1. 20
4. 75	1. 59	11.00	6. 37	17. 25	1. 99	23. 50	1. 20
5.00	1. 59	11. 25	5. 98	17. 50	1. 59	23. 75	1. 20
5. 25	1. 59	11. 50	9. 56	17. 75	1. 99	24.00	1. 20
5. 50	1. 59	11. 75 12. 00	9. 56 29. 48	18. 00 18. 25	1. 59	24. 25	1. 20
5. 75 6. 00	1. 59	12.00	29. 48 121. 91		1. 99 1. 59		
6. 25	1. 59 1. 59	12. 25	14. 34	18. 50 18. 75	1. 39		
0. 23	1. 39	12.50	14. 34	16.73	1. 99		

```
CALIB
STANDHYD (0001)
ID= 1 DT= 5.0 min
                                   Area (ha) = 2.28
Total Imp(%) = 90.00
                                                                        Dir. Conn. (%) = 90.00
                                                                    PERVIOUS (i)
0.23
5.00
                                              I MPERVI OUS
      Surface Area
Dep. Storage
Average SI ope
Length
                                  (ha) =
                                                    2.05
                                  (mm) =
                                                     1.00
                                    (%) =
                                                                         2.00
                                                    1.00
                                    (m) =
                                                  123. 29
                                                                        40.00
      Manni ngs n
                                                   0.013
                                                                        0.250
```

NOTE: RAINFALL WAS TRANSFORMED TO 5.0 MIN. TIME STEP.

TRANSFORMED HYETOGRAPH							
TIME	RAIN	TIME	RAIN	' TIME	RAI N	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	' hrs	mm/hr	hrs	mm/hr
0. 083	0. 00	6. 167	1. 59	12. 250	121. 91	18. 33	1. 59
0. 167	0. 00	6. 250	1. 59	12. 333	14. 36	18. 42	1. 59
0. 250	0. 00	6. 333	1. 79	12. 417	14. 34	18. 50	1. 59
0. 333	1. 10	6. 417	1. 79	12. 500	14. 34	18. 58	1. 99
0. 417	1. 10	6. 500	1. 79	12. 583	14. 34	18. 67	1. 99
0. 500	1. 10	6. 583	1. 79	12. 667	14. 34	18. 75	1. 99
0. 583	1. 10	6. 667	1. 79	12. 750	14. 34	18. 83	1. 59
0. 667	1. 10	6. 750	1. 79	12. 833	7. 57	18. 92	1. 59
0. 750	1. 10	6. 833	1. 79	12. 917	7. 57	19. 00	1. 59
0. 833	1. 10	6. 917	1. 79	13.000	7. 57	19. 08	1. 99
0. 917	1. 10	7. 000	1. 79	13. 083	7. 17	19. 17	1. 99
1. 000	1. 10	7. 083	1. 79	13. 167	7. 17	19. 25	1. 99
1. 083	1. 10	7. 167	1. 79	13. 250	7. 17	19. 33	1. 59
1. 167	1. 10	7. 250	1. 79	13. 333	5. 58	19. 42	1. 59
1. 250	1. 10	7. 333	2. 39	13. 417	5. 58	19. 50	1. 59
1. 333	1. 08	7. 417	2. 39	13. 500	5. 58	19. 58	1. 99
1. 417	1. 08	7. 500	2. 39	13. 583	5. 18	19. 67	1. 99
1. 500	1. 08	7. 583	1. 99	13. 667	5. 18	19. 75	1. 99
1. 583	1. 12	7. 667	1. 99	13. 750	5. 18	19. 83	1. 59
			2000 12				

1. 667 1. 750 1. 833 1. 917 2. 000 2. 083 2. 167 2. 250 2. 333 2. 417 2. 500 2. 583 2. 667 2. 750 2. 833 2. 917 3. 000 3. 083 3. 167 3. 250 3. 333 3. 417 3. 500 3. 583 3. 667 3. 750 3. 833 3. 917 4. 000 4. 083 4. 167 4. 250 4. 333 4. 417 4. 500 4. 583 4. 667 4. 750 4. 833 4. 417 5. 000 5. 083 5. 167 5. 250 5. 333 5. 417 5. 500 5. 583 5. 667 5. 750 5. 833 5. 917 6. 000 6. 083	1. 12 1. 08 1. 08 1. 08 1. 12 1. 12 1. 12 1. 12 1. 27 1. 27 1. 31 1. 59 1. 59	7. 750 7. 833 7. 917 8. 000 8. 083 8. 167 8. 250 8. 333 8. 417 8. 500 8. 583 8. 667 8. 750 8. 833 8. 667 9. 083 9. 167 9. 333 9. 167 9. 250 9. 3417 0. 083 0. 167 0. 250 0. 833 0. 917 1. 083 1. 167 0. 833 0. 917 1. 083 1. 1583 1. 1583 1. 1583 1. 1583 1. 1583 1. 167 1. 833 1. 167 1. 833 1. 167 1. 1833 1. 167 1. 1833 1. 167 1. 1833 1. 167 1. 1833 1. 167 1. 1833 1. 167 1. 1833 1. 167 1. 1	1. 99 2. 39 2. 39 1. 99 2. 39 1. 79 2. 39 1. 79 2. 39 2. 79 2. 30 3. 30 3. 30 3. 59 4. 38 4. 38 4. 38 5. 59 7. 50 7. 50	A POND. out   13. 833   13. 917   14. 000   14. 083   14. 167   14. 250   14. 333   14. 417   14. 500   14. 583   14. 667   14. 750   15. 083   15. 167   15. 250   15. 333   15. 417   15. 500   15. 833   15. 417   16. 000   16. 083   16. 167   16. 250   16. 333   16. 417   16. 583   16. 667   17. 750   17. 833   17. 167   17. 500   17. 083   17. 167   17. 500   17. 833   17. 417   17. 500   17. 833   17. 917   18. 000   18. 083   18. 167   18. 250   18. 250   18. 250   19. 333   19	4. 38 4. 38 4. 38 3. 98 3. 19 2. 79 2. 79 2. 79 3. 19 2. 79 3. 19 3. 19 3. 19 4. 38 3. 19 5. 79 79 79 79 79 79 79 79 79 79 79 79 79 7	19. 92 20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 20. 58 20. 67 20. 75 20. 83 20. 92 21. 00 21. 83 21. 25 21. 33 21. 42 21. 50 21. 58 21. 67 21. 75 21. 83 21. 42 22. 50 22. 83 22. 42 22. 58 22. 67 22. 75 22. 83 22. 42 22. 58 22. 75 22. 83 22. 42 23. 58 23. 75 23. 83 23. 42 23. 50 23. 75 23. 83 23. 92 24. 00 24. 08 24. 17 24. 25	1. 59 1. 59 1. 99 1. 99 1. 20 1. 20 20 20 20 20 20 20 20 20 20 20 20 20 2
Unit Hyd. Tpeak (mi		121. 91 5. 00 2. 68 5. 00 0. 29	(ii)	84. 03 10. 00 5. 38 (ii) 10. 00 0. 16	***	-A1 C*	
	ns) = rs) =	0. 69 12. 25 Pa	age 14	0. 05 12. 25	0.	ALS* 739 (iii) 2. 25	

RUNOFF VOLUME ( TOTAL RAINFALL ( RUNOFF COEFFICIENT	mm) = mm) =	98. 60 99. 60	Ç	. POND. ou <sup>.</sup> 56. 60 99. 60 0. 57	94 99	4. 40 9. 60 0. 95	
**** WARNING: STORAGE	COEFF. I	S SMALLE	R THAN	TIME STEP	·!		
(i) CN PROCEDURE CN* = 80. (ii) TIME STEP (D THAN THE STO (iii) PEAK FLOW DO	O Ia T) SHOUL RAGE COE	= Dep. S D BE SMA FFICIENT	Storage ALLER OR	(Above) EQUAL			
RESERVOIR (0004)     IN= 2> OUT= 1   DT= 5.0 min	(cms) 0.000 0.008	W STC (ha 0 0. 0 0. 0 0. 0 0.	DRAGE a.m.) 0000 0650 0720 1440	OUTFLO (cms) 0.069 0.079 0.089 0.090	W ST( (ha 0 ( 0 ( 0 ( 0 (	a.m.) D.2160 D.2880	
INFLOW: ID= 2 (00 OUTFLOW: ID= 1 (00	01) 04)	AREA (ha) 2. 280 2. 280	QPEAK (cms) 0.73 0.05	TPEA (hrs 39 12 54 12	K ) . 25 . 83	R. V. (mm) 94.40 93.50	
PEAK TIME MAXI	FLOW SHIFT O MUM STO	REDUCT F PEAK F RAGE L	TION [Qou FLOW JSED	ut/Qi n] (% (mi n (ha. m.	(a) = 7.27 (b) = 35.00 (c) = 0.13	7 ) 339 	
**************************************	6 **						
		ata\l 26b19	ocal \Ter 0c33-92b6	ó-46d3-96	3b-4d66a	ac4f1477\ Storm Sa	bc37ea81
Ptotal =108. 90 mm	RAIN   mm/hr   0.00   1.20   1.20   1.18   1.22   1.18   1.22   1.39   1.44   1.44   1.39   1.44   1	TIME hrs 6.50 6.75 7.00 7.25 7.50 7.75 8.00 8.25 8.50 9.25 9.50 9.75 10.00 10.25 10.50	RAIN mm/hr 1.96 1.96 1.96 1.96 2.61 2.18 2.61 3.05 2.61 3.92 3.92 5.23	TI ME hrs 12. 75 13. 00 13. 25 13. 75 14. 00 14. 25 15. 50 15. 25 15. 50 16. 25 16. 50 16. 75	RAIN mm/hr 15. 68 8. 28 7. 84 6. 10 5. 66 4. 79 4. 36 3. 48 3. 05 3. 48 3. 05 3. 48 3. 05 3. 48 1. 74 2. 18		RAIN mm/hr 1.74 2.18 1.74 2.18 1.74 2.18 1.31 1.31 1.31 1.31 1.31 1.31 1.31 1

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```
1.74
4.50
                                                 1.74
                                                          23. 25
                                                                     1. 31
                                      17. 25
17. 50
17. 75
         1. 74
1. 74
1. 74
                                                 2. 18
1. 74
2. 18
                                                          23. 50
23. 75
4.75
                             6.97
                  11.00
                                                                     1. 31
                  11. 25
11. 50
                                                                     1. 31
1. 31
5.00
                             6.53
5. 25
                                                          24.00
                            10.45
5.50
         1.74
                  11.75
                                      18.00
                                                 1.74
                                                          24. 25
                                                                     1.31
                            10.45
5.75
         1.74
                  12.00
                            32. 23
                                      18. 25
                                                 2. 18
                           133.29
                                      18.50
6.00
         1.74
                  12. 25
                                                 1.74
                  12.50
6. 25
          1.74
                            15.68
                                      18. 75
                                                 2. 18
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CALIB
STANDHYD (0001)
ID= 1 DT= 5.0 min
                                    (ha) = 2.28
                          Area
                          Total Imp(\%) = 90.00
                                                      Dir. Conn. (%) = 90.00
                                   I MPERVI OUS
                                                   PERVIOUS (i)
     Surface Area
                         (ha)=
                                       2.05
                                                       0.23
     Dep. Storage
                                       1.00
                                                       5.00
                         (mm) =
                                     1. 00
123. 29
0. 013
                                                       2.00
     Average Slope
                          (%)=
     Length
                          (m) =
                                                      40.00
                                                      0.250
     Mannings n
```

TI ME hrs 0. 083 0. 167 0. 250 0. 333 0. 417 0. 500 0. 583 0. 667 0. 750 0. 833 1. 167 1. 250 1. 333 1. 417 1. 500 1. 583 1. 417 1. 500 1. 583 1. 667 1. 750 1. 833 1. 917 2. 000 2. 083 2. 167 2. 250 2. 333 2. 417	RAIN mm/hr 0.00 0.00 0.00 1.20 1.20 1.20 1.20 1.20	TIME hrs 6. 167 6. 250 6. 333 6. 417 6. 500 6. 583 6. 667 6. 750 6. 833 7. 167 7. 250 7. 333 7. 417 7. 500 7. 583 7. 667 7. 750 7. 833 7. 917 8. 000 8. 083 8. 167 8. 250 8. 333 8. 417	NSFORME RAIN mm/hr 1.74 1.96 1.96 1.96 1.96 1.96 1.96 1.96 1.96	TIME hrs 12. 250 12. 333 12. 417 12. 500 12. 583 12. 667 12. 750 12. 833 12. 917 13. 000 13. 083 13. 167 13. 250 13. 333 13. 417 13. 500 13. 583 13. 667 13. 750 13. 833 13. 917 14. 000 14. 083 14. 167 14. 250 14. 333 14. 417 14. 500	RAIN mm/hr 133. 29 15. 70 15. 68 15. 68 15. 68 15. 68 15. 68 8. 28 8. 28 7. 84 7. 84 6. 10 6. 10 5. 66 5. 66 4. 79 4. 79 4. 36 4. 36 3. 48 3. 48 3. 48 3. 48	TIME hrs 18. 33 18. 42 18. 50 18. 58 18. 67 18. 75 18. 83 18. 92 19. 00 19. 08 19. 17 19. 25 19. 33 19. 42 19. 50 19. 58 19. 75 19. 83 19. 75 19. 83 19. 92 20. 00 20. 08 20. 17 20. 25 20. 33 20. 42 20. 50 20. 58	RAIN mm/hr 1. 74 1. 74 1. 74 2. 18 2. 18 2. 18 1. 74 1. 74 2. 18 2. 18 2. 18 1. 74 1. 74 1. 74 2. 18 2. 18 1. 74 1
2. 083	1. 22	8. 167	2. 18	14. 250	4. 36	20. 33	1. 31
2. 167	1. 22	8. 250	2. 18	14. 333	3. 48	20. 42	1. 31
2. 250	1. 22	8. 333	3. 05	14. 417	3. 48	20. 50	1. 31

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EP POST MISSISSAUGA POND. out
                       1. 39
            2.917
                               9.000
                                          3.05
                                                15.083
                                                             3.48
                                                                     21. 17
                                                                               1. 31
             3.000
                       1.39
                               9.083
                                          3.05
                                                             3.48
                                                                     21.25
                                                 15. 167
                                                                               1. 31
                                                 15. 250
             3.083
                       1.44
                               9. 167
                                          3.05
                                                             3.48
                                                                     21.33
                                                                               1.31
                               9.250
                                                 15.333
                       1.44
                                          3.05
            3. 167
                                                             3.05
                                                                     21. 42
                                                                               1.31
            3.250
                       1.44
                               9.333
                                          3.48
                                                 15.417
                                                             3.05
                                                                     21.50
                                                                               1.31
            3.333
                       1.39
                                                 15.500
                                                                     21.58
                               9.417
                                          3.48
                                                             3.05
                                                                               1. 31
            3.417
                       1.39
                               9.500
                                          3.48
                                                 15.583
                                                             3.48
                                                                     21.67
                                                                               1.31
                                          3.48
                                                             3.48
            3.500
                       1.39
                               9.583
                                                 15. 667
                                                                     21.75
                                                                               1. 31
            3.583
                       1.44
                               9.667
                                          3.48
                                                 15.750
                                                            3.48
                                                                     21.83
                                                                               1. 31
             3.667
                       1.44
                               9.750
                                          3.48
                                                 15.833
                                                             3.05
                                                                     21.92
                                                                               1. 31
                               9.833
             3.750
                       1.44
                                          3.92
                                                 15.917
                                                             3.05
                                                                     22.00
                                                                               1. 31
                                          3.92
             3.833
                       1.44
                              9. 917
                                                 16.000
                                                             3.05
                                                                     22.08
                                                                               1. 31
            3.917
                                          3.92
                       1.44
                              10.000
                                                                     22. 17
                                                 16.083
                                                             3.48
                                                                               1.31
                       1.44
                                                            3.48
            4.000
                              10.083
                                          3.92
                                                 16. 167
                                                                     22. 25
                                                                               1. 31
                       1.39
            4.083
                              10. 167
                                          3.92
                                                 16.250
                                                            3.48
                                                                     22.33
                                                                               1.31
            4.167
                                          3.92
                                                                               1. 31
                       1. 39
                              10.250
                                                 16. 333
                                                            1.74
                                                                     22. 42
            4. 250
                       1.39
                                                                     22. 50
                                          5.23
                                                 16. 417
                                                            1.74
                              10. 333
                                                                               1. 31
                       1.74
                                                                     22. 58
            4.333
                              10.417
                                          5.23
                                                 16.500
                                                            1.74
                                                                               1. 31
                                          5. 23
4. 79
            4.417
                              10.500
                                                             2. 18
                       1.74
                                                 16.583
                                                                     22.67
                                                                               1.31
                                                            2. 18
2. 18
1. 74
            4.500
                       1.74
                              10.583
                                                                     22.75
                                                 16.667
                                                                               1. 31
                                          4.79
            4.583
                       1.74
                              10.667
                                                 16.750
                                                                     22.83
                                                                               1. 31
1. 31
                                         4. 79
                       1.74
                                                                     22.92
            4.667
                              10.750
                                                 16.833
                                         6. 97
                                                                               1.31
            4.750
                       1.74
                              10.833
                                                 16.917
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                              11. 417
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                                                            1.74
                                                                     23.58
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            5.417
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            6.083
                                                18. 250
Max. Eff. Inten. (mm/hr)=
                               133. 29
                                                95.39
                          5. 00
2. 58
5. 00
0. 29
            over (min)
                                               10.00
                                 2.58 (ii)
                                                5.19 (ii)
Storage Coeff.
                  (min) =
                                               10.00
Unit Hyd. Tpeak (min)=
Unit Hyd. peak (cms)=
                                                0. 16
                                                               *TOTALS*
                           0. /6
12. 25
107. 90
                                                               0.811 (iii)
12.25
PEAK FLOW
                   (cms) =
                                                0.05
TIME TO PEAK
                                               12. 25
                   (hrs)=
RUNOFF VOLUME
                                                                103.56
                                               64. 49
                    (mm) =
TOTAL RAINFALL
                    (mm) =
                               108.90
                                              108. 90
                                                              108. 90
RUNOFF COEFFICIENT
                                 0.99
                                                 0.59
                                                                  0.95
```

\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

<sup>|</sup> RESERVOIR (0004) |

# EP POST MISSISSAUGA POND. out

I N= 2> OUT= 1     DT= 5.0 min	OUTFLOW (cms) 0.0000 0.0080 0.0400 0.0560	STORAG (ha. m. 0. 000 0. 065 0. 072 0. 144	0 0	OUTFLOW (cms) 0.0690 0.0790 0.0890 0.0900	STORAGE (ha. m.) 0. 2160 0. 2880 0. 3610 0. 3740
INFLOW: ID= 2 (000 OUTFLOW: ID= 1 (000 PEAK	(I 1) 2. 4) 2.		PEAK cms) 0.811 0.057	TPEAK (hrs) 12.25 12.92	R. V. (mm) 103. 56 102. 65

PEAK FLOW REDUCTION [Qout/Qin](%) = 6.98 TIME SHIFT OF PEAK FLOW (min) = 40.00 MAXIMUM STORAGE USED (ha.m.) = 0.1473

-----

FINISH

# Stage-Storage-Discharge Tables

Cooling Tower Storage area is 73.3 m long by 17.6 m wide. There is additional storage in the Pump House and Connection Trench

Total Surface Area = 1442.0 m2 From Dillon Report (April 26, 2007)

Max Height = 1.0 m

Orifice Size = 300.0 mm Orifice Area = 0.0707 m2

Cd = 0.6200 orifice plate

Stage (m)	Storage (m3)	Discharge (m3/s)
0.0	0.0	0.000
0.1	144.2	0.061
0.2	288.4	0.087
0.3	432.6	0.106
0.4	576.8	0.123
0.5	721.0	0.137
0.6	865.2	0.150
0.7	1009.4	0.162
8.0	1153.6	0.174
0.9	1297.8	0.184
1.0	1442.0	0.194

# 25 mm Rainfall Event Determine Amount of Runoff

Rainfall (mm) 25

Total Area (ha) 2.28

Drainage Area Area (ha) CN

Developed 2.166 98 Undeveloped 0.114 80

Area Weighted CN 97.1

Runoff Amount (mm) 20

Runoff Volume (m3) 456

# 25 mm Rainfall Event

Determine Drawdown time in Cooling Tower Basin

T, detention tim, sec =  $(2 \times Ap \times (h1^0.5 - h2^0.5)) / (C \times Ao \times (2g)^0.5)$ 

surface area of pond, m2 = with Ap =1369 starting water elevation, m = hi = 0.33 h2 = ending water elevation, m = 0.01 dischage coefficient = C = 0.63 Ao = area of orifice, m2 = 0.004418 gravity, m/s^2 9.81 g =

Orifice dia, m = 0.075

T = 90619.5 seconds 25.2 hours

# **Green Electron Project ESRR**

17.6 APPENDIX 17.6 - Archaeological Assessment East Site



## STAGE 1 ARCHAEOLOGICAL ASSESSMENT (Revised Sept. 28, 2012)



# Green Electron Power Plant E. ½, Lot 26, Concession 2, Moore Twp., Lambton Co., ON.

Dave Riddell, M.A.
Archaeological Assessments and Mitigation
Box 791, Grand Bend, ON. NOM 1T0
(Ph)519-238-6966

Email: aam@davidriddell.ca PIF #:PO77-006-2012

Contact: Matthew DeVuono
Eastern Power Limited
Greenfield South Power Corporation
1796 Mattawa Ave.,
Mississauga, On. L4K 1K1
(Ph) 416-451-8603 / 416-234-1301
mdevuono@easternpower.on.ca

September 28, 2012

David Riddell, M.A.
Professional Archaeological Licence (Ontario)



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Archaeological Assessments and Mitigation Box 791, Grand Bend, ON. NOM 1T0

August 8, 2012

## Dear Ministry of Tourism and Culture,

- 1. a) David Riddell
  - b) # PO77
  - c) Box 791, Grand Bend, ON.

N0M 1T0

aam@davidriddell.ca

519-238-6966, 250-418-5109

d) Archaeological Assessments and Mitigation

e)



- 2. a) # PO77- 006- 2012
  - b) Stage 1
  - c) Green Electron Power Plant
  - d) Lambton County, Moore Twp., E. 1/2 Lot 26, Con. 2
- 3. a) Eastern Power Limited
  - b) Matthew DeVuono
  - c) 1796 Mattawa Ave,

Mississauga, On., L4K 1K1

(PH) 416-451-8603 / 416-234-1301

Email: mdevuono@easternpower.on.ca

- d) Plan 24 RP25R 1585
- 4. a) County of Lambton Planning and Development Services
  - b) Dave Posliff, Manager

789 Broadway St., Box 3000, Wyoming, ON. NON 1T0 519-845-0801

Email:

- c) N/A
- d) Planning Act
- e) Plan 24 RP25R 1585
- 5. a) 08/10/2012
  - b) "I the undersigned hereby declare that, to the best of my knowledge, the information in this report and submitted in support of this report is complete and accurate in every way, and I am aware of the penalties against providing false information under section 69 of the *Ontario Heritage Act*"
  - c) original
  - d) N/A
  - e) N/A
  - f) N/A



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Acknowledgements Matthew DeVuono, Eastern Energy Corp.

Project Director, Archaeologist David Riddell, M.A.

**Background Research** David Riddell

**Bob Smith** 

**Report Preparation** David Riddell

Maureen Erb

Ministry of Tourism and Culture Robert Von Bitter



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## 1.0: Executive Summary

In early August of 2012, Archaeological Assessments and Mitigation was contacted by the proponent, Eastern Energy Limited, to undertake a Stage 1 Archaeological Assessment on the "Lambton East" property, an approximately 75 acre tract of the eastern half of Lot 26, Concession 2, Moore Township. (proposed development is referred to as "Green Electron Power Plant").

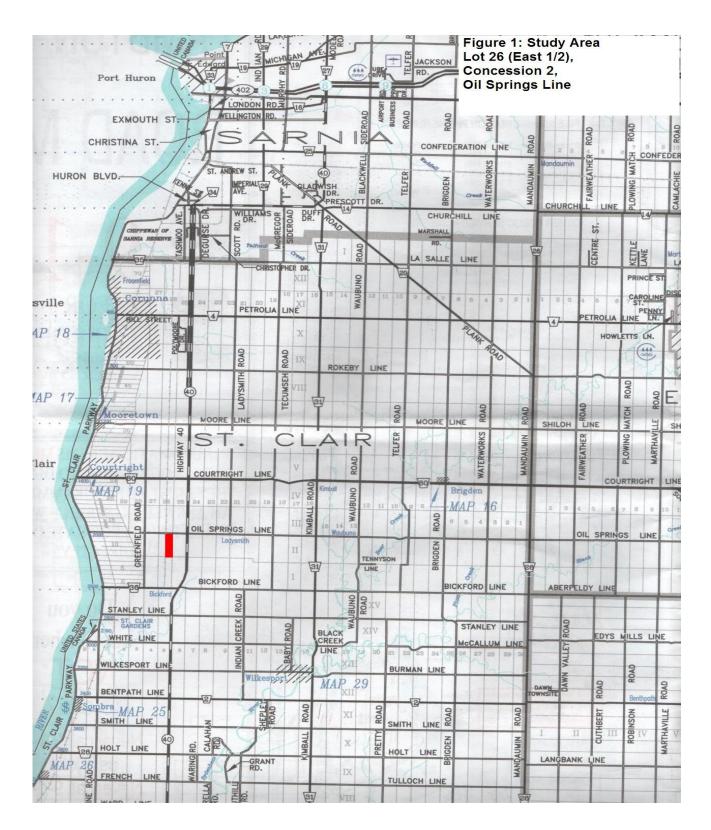
The contract between these two parties was signed on August 4<sup>th</sup>, 2012, and Stage 1 research was completed the following week. The results are submitted herein, and summarized as follows.

The study area consists of cultivated agricultural field, and woodlot in the southern most portion of the property. There are no topographic features or watercourses present, indicating low pre-contact First Nations settlement potential. Additionally, there were no Euro-Canadian records of evidence of settlement on the property.

It is therefore recommended that the subject property be issued a standard condition of development approval.



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## 2.0: Background Research - Development Context

The proposed development, "Green Electron Power Plant" will be a facility generating steam energy. The construction will be exposing subsurface soil stratigraphy and geomorphology (see expedite letter, development map). A class environmental assessment was therefore designated, resulting in the necessity of an archaeological assessment.

In compliance with the provincial regulations stipulated in the "Archaeological Assessment Technical Guidelines" the Stage 1 Archaeological Background Study included:

- a. A review of the land use history, including pertinent historic maps
- b. An examination of the National Site Registration database to determine the presence of known archaeological sites within and surrounding (250 meters) the project area.



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## 2.1: Study Area Physiography, Site Potential

The study area, as is the case with much of Lambton County in proximity to the St. Clair River, is contained within an expansive, flat clay plain, providing little topography and poor drainage. As the Historical Atlas of Lambton County explains (referring to Moore Township): "The topographical characteristics of the territory are almost the exact counterpart of those of most of the other townships of the low, alluvial district of the Western peninsula, and more particularly of Lambton County, …" (page 16).

Again, citing from the Historical Atlas, the preoccupation with turning the flat heavy land into a farmable proposition is related: "From the fact that there are nearly \$20,000 of outstanding drainage debentures against the township, it is but fair to suppose that energetic efforts have been commenced to convert the former impenetrable swamp, covering the central portion of the township, into a valuable and fertile section..." (page 16).

Since there are no watercourses within the 300 meter limit of the study area, combined with poorly drained, heavy clay soils and low topography, the potential for First Nations settlement in particular is low. The archaeological site database indicates that there are no registered archaeological sites within the 250 meter radius of the study area.

Distance to modern or ancient water sources is generally accepted as the most important determinant of past human settlement patterns and, considered alone, may result in a determination of archaeological potential. However, any combination of two or more other criteria, such as well-drained soils, or topographic variability, may also indicate archaeological potential.

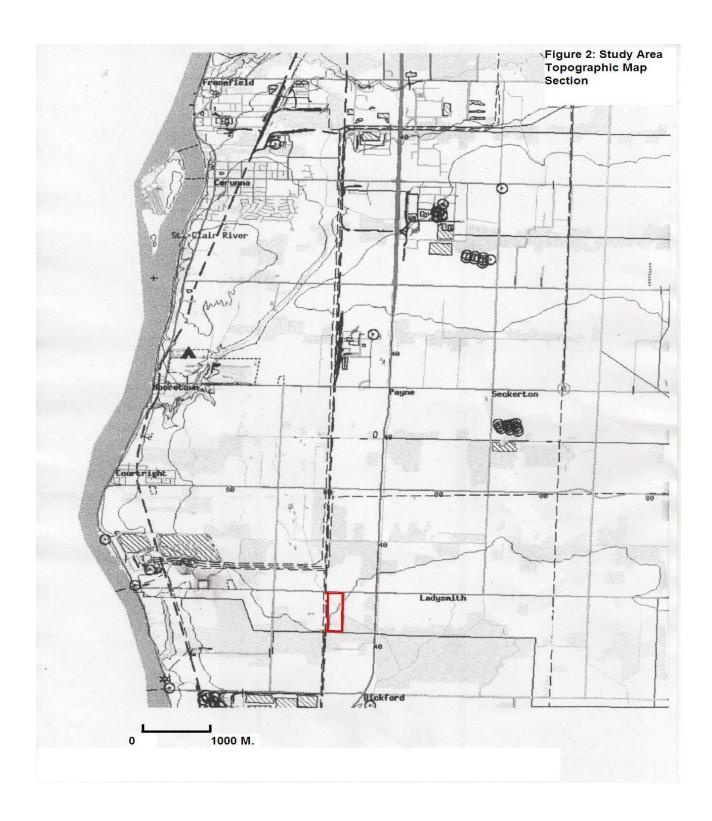
The property itself is primarily composed of cultivated field (approximately 65 acres), and the southernmost portion of the lot is in woodlot (approximately 10 acres). A drainage ditch cuts across the property in the north half section running from northwest to southeast. The ditch is part of a larger drain which eventually drains into a watershed, but is not itself a natural feature of this watershed.

There is a spur railway line which runs from Sarnia to Port Lambton bordering the lot on the west side.

The criteria used by the Ontario Ministry of Tourism and Culture to determine potential for historic archaeological sites includes the presence of: 1. particular, resource-specific features that would have attracted past subsistence or extractive uses; 2. areas of initial, non-aboriginal settlement; 3. early historic transportation routes; 4. properties designated under the Ontario Heritage Act. In terms of specific historic aboriginal records, Treaty No. 27 &1/2 and Treaty No. 7 were the transactions which occurred between the British crown and the Chippewa bands within the study area (Appendix B).

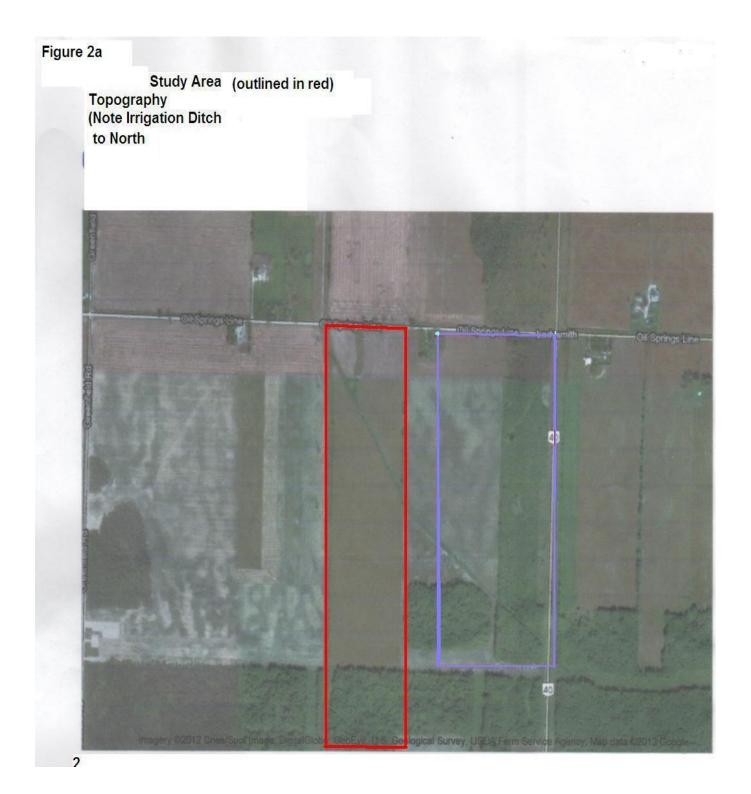


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## 2.2: Historical Research: Nineteenth Century Land Records

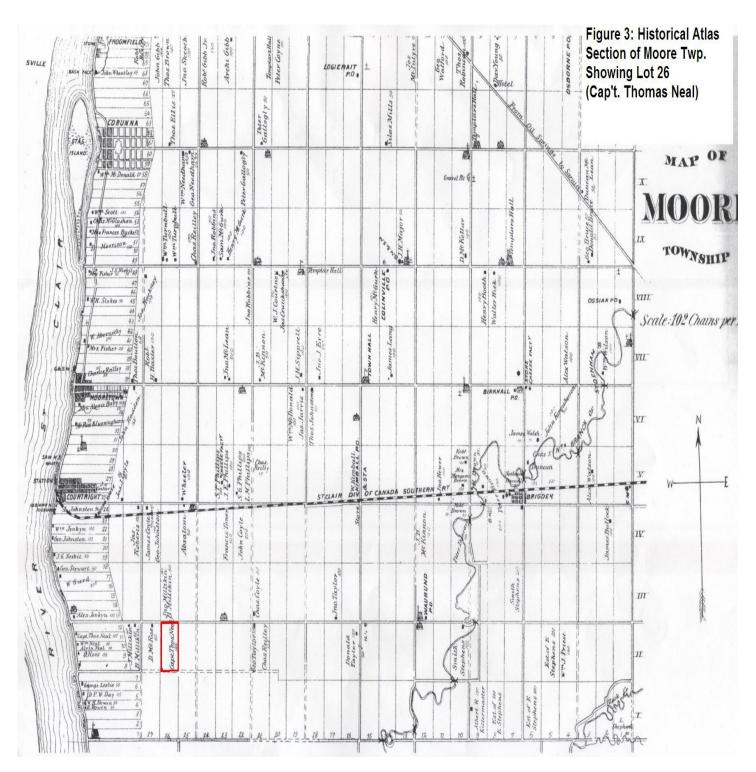
The nearest commercial center to the subject property in the nineteenth century was the village of Courtright, located approximately 5km. to the northwest, on the shores of the St. Clair River. Aside from a local post office in Ladysmith, located about 3 km. to the east of the property, Courtright would have provided the bulk of services for the inhabitants of the property. The village itself was a terminus for the Canada Southern Railway line, and boasted two groceries, general store, several blacksmith shops, wagon and cooperage, two steam planning mills, two hotels, a school and Methodist church.

The earliest transaction recorded on the property (the east <sup>3</sup>/<sub>4</sub>) is in 1855, where a Hugh Johnston, the initial ("grantor") "discharged" 150 ac. to Charles Middleton. There is a gap in the records from 1857 (T. Forsyth is listed as the landholder at this time) to 1866, where Hugh Johnston once again appears on the ledger as the grantor, the transaction to a George B. Johnston (again, the east <sup>3</sup>/<sub>4</sub>). The Atlas shows the Johnstons as owning tracts of land near Courtright. In the same owning tracts of land near Courtright. In the same year, the latter grants the parcel to John Miller, and in 1869, the parcel is in the hands of Robert Gurd. Gurd is shown as the grantor in the same year of the parcel to Thomas Neal. This name is on the study area property in the Historical Atlas (Figure 2), as "Captain Thomas Neal". This family is of some prominence in the region, as "subscribers" to the county atlas. Neal's residence is situated on the shores of the St. Clair River due west of Lot 26, as is his son's, Alvin Neal, who settled in Moore Twp. From Detroit in 1860. They are shown as owning 226 acres. The Neals (Thomas, Alvin and William) are involved in various transactions of this parcel of land (including between themselves) from this period up until 1887, when Alvin Neal grants the land back to John Ferguson. Ferguson's name is on the ledger in several places from 1885 to 1889. One of these transactions is with the "Lambton Loan & I. Company" (1887), with Ferguson as the grantor to the latter of 76 acres and a mortgage of \$835. Another business/company name appears on the ledger at an earlier date (1885), that of the "North of Scotland C.M. Company", but this referring to the west 1/4 of the lot and a smaller mortgage. Both these companies appear on the list in several instances from 1885 to 1890, both as "grantors" and "grantees". This leads one to believe that there was a business boom in the nearby settlements at this time.

Meanwhile, in the latter decade of the nineteenth century, a name of considerable noteworthiness, Raymond Baby (as in the "Baby House" in Windsor) appears on the scene as a grantee and grantor in the same year (1890). The land then reverts back to John Ferguson, who remains the grantee well into the 20<sup>th</sup> century.



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## 3.0: Results, Interpretation

The parcel of land, east ½ of Lot 26, Concession 2, Moore Township in Lambton County appears to have offered no attraction to that of First Nations settlement throughout history. It is situated far enough to the east of the major waterway, the St. Clair river, a major transportation/trade/ settlement corridor for numerous First peoples, and not within proximity to other water sources, to have been undesirable for these groups to settle in.

As far as Euro-Canadian settlement of the property goes, again the desirable place of residence was along the shores of the St.Clair River, with the allocation of lands further inland left for the purpose of agricultural use. This pattern gradually shifted towards the latter part of the nineteenth century, with residences becoming more prevalent along the concession roads and railway lines. An inspection of the north section of the property along the concession road however, has not revealed any evidence of 19<sup>th</sup> century occupation here. Farm structures are present, however, both to the east and west of the study area property, indicative of those locations as the residences throughout the historical period.



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## 4.0: Recommendations

Based on the lack of both First Nations and Euro-Canadian settlement on the subject property, it is recommended that the property be issued a letter of clearance for the development plans as provided.

Should deeply buried cultural remains be encountered during the development process, however, the proponent should contact the Ministry of Tourism, Culture and Sport, Archaeological office at 416-314-7174.

In the event that human remains are encountered, the proponent should contact both the Ministry of Tourism, Culture and Sport at the above number, and the Registrar or Deputy Registrar of Cemeteries Unit of the Ministry of Consumer and Commercial Relations at 416-326-8392.



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## 5.0: References Cited

- 1. Historical Atlas of Lambton County, 1849 Beldon, Sarnia 1880.
- 2. Lambton County Archives, Central Library, Wyoming, Ontario
- 3. Morris, J.L. 1943 Indians of Ontario (1964 reprint). Department of Lands and Forests, Government of Ontario



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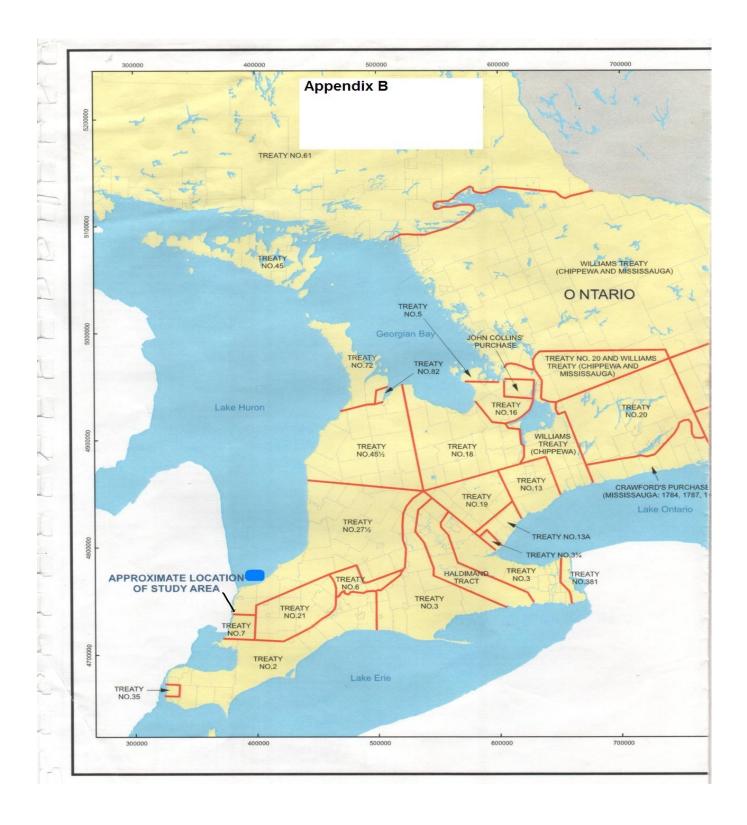
## Appendix A

## **Cultural Chronology**

Period	Characteristics	Time	Comments
Early Paleo-Indian	Fluted Projectiles	9000 - 8400 B.C.	spruce parkland/caribou hunters
Late Paleo-Indian	Hi-Lo Projectiles	8400 - 8000B.C.	smaller but more numerous sites
Early Archaic	Kirk and Bifurcate Base Points	8000 - 6000 B.C.	slow population growth
Middle Archaic	Brewerton-like points	6000 - 2500 B.C.	environment similar to present
Late Archaic	Lamoka (narrow points)	2000 - 1800 B.C.	increasing site size
	Broadpoints	1800 - 1500 B.C.	large chipped lithic tools
	Small Points	1500 - 1100B.C.	introduction of bow hunting
Terminal Archaic	Hind Points	1100 - 950 B.C.	emergence of true cemeteries
Early Woodland	Meadowood Points	950 - 400 B.C.	introduction of pattery
Middle Woodland	Dentate/Pseudo-Scallop Pottery	400 B.C A.D.500	increased sedentism
	Princess Point	A.D. 550 - 900	introduction of corn
Late Woodland	Early Ontario Iroquoian	A.D. 900 - 1300	emergence of agricultural villages
	Middle Ontario Iroquoian	A.D. 1300 - 1400	long longhouses (100m +)
	Late Ontario Iroquoian	A.D. 1400 - 1650	tribal warfare and displacement
Contact Aboriginal	Various Algonkian Groups	A.D. 1700 - 1875	early written records and treaties
Historic	Euro-Canadian	A.D. 1796 - present	European settlement



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## **Green Electron Project ESRR**

17.7 APPENDIX 17.7 - Public Consultation Report

# **Green Electron Power Project Environmental Screening Process**

# Public Consultation Report

November 5, 2012

Prepared By: Monika Vogt, BSc Reviewed By: Bruce Holbein, Ph.D. Approved By: Hubert Vogt, P.Eng

# GREENFIELD SOUTH POWER PROJECT Public Consultation Report

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## 1. Introduction

This report documents the public consultation process required as part of the environmental screening process for the Green Electron Power Project. The environmental screening process is applicable to the Green Electron Power Project because it is a Category B electricity project under Ontario Regulation 116/01 of the Environmental Assessment Act.

The proponent of the Green Electron Power Project is Greenfield South Power Corporation.

The Green Electron Power Project is part of the Ontario Government's initiative to improve air quality in Ontario by phasing out the use of coal-fired electricity generation. The purpose of the public consultation process is to "allow the proponent to identify and address public concerns and issues and to provide the public with an opportunity to receive information and make meaningful input into the project review and development." This report describes all of the steps taken by the proponent of the project to comply with the public consultation requirements set out in Ontario Regulation 116/01 together with explanations and analyses supporting this compliance, as well as a listing of all of the concerns and issues raised by the public consultation process matched with the response of the proponent to these issues.

The major components of the public consultation process for the Green Electron Power Project included:

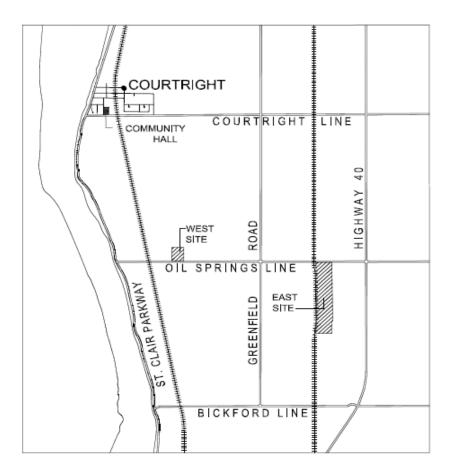
- 1. Public notices that were published in the local newspapers, delivered to local residents and businesses and interested members of the public;
- 2. Written information that was delivered, mailed or e-mailed to local residents and businesses and interested members of the public:
- 3. Two public open house events for the project held on August 16, 2012 and September 12, 2012;
- 4. Questionnaires completed by attendees of open house events;
- 5. Correspondence received from concerned members of the public; and
- 6. The placement of the environmental screening report in the public library, in local municipal offices and on a project web site for 30 days of review.

The public consultation process presented both the East and West candidate sites together (see Section 2 - Project Description) so this report addresses both sites. In parallel with the public consultation process a separate consultation process was undertaken with affected government departments and public agencies at the federal, provincial and municipal levels, as well as potentially affected First Nations. The results of the government agencies consultation are reported on separately and therefore are not addressed in this report.

## 2. Project Description

The Green Electron Power Project involves the construction and operation of an electricity generating plant that was proposed in response to the Ontario Ministry of Energy's Request for Proposals for new clean energy supply to facilitate the phasing-out of coal-fired electricity generation in Ontario. The project was selected by the Ontario Ministry of Energy and is expected to be in-service by 2014. The plant will have a capacity of about 300 MW configured as a combined cycle power plant to be fueled only with natural gas. The project will be located in St. Clair Township at one of two sites on Oil Springs Line near Greenfield Road (see Fig. 2.1) on land that is in each case zoned for power generation uses. The sites are located adjacent to one of Hydro One's 230 kV transmission corridors.

Figure 2.1 - Location of Proposed Green Electron Power Project



The configuration of the power plant will utilize one gas turbine generator set and the exhaust gas from the gas turbine will be ducted to a water-tube, heat recovery steam generator (HRSG) equipped with a duct burner fuelled by natural gas. The steam from the HRSG will drive a steam turbine generator set. The plant will also include steam condensing equipment, steam condensate and boiler feedwater equipment, as well as boiler make-up water treatment system.

## 3. Public Notices and Information

The environmental screening process mandates a public notice of the commencement of an environmental screening, notice of commencement of entering the environmental review stage and notice of completion of the screening/environmental review.

Public notification of the Green Electron Power Project began with publication, in the Sarnia Observer, on July 30 and 31, 2012, and the Wallaceburg Courier on August 9, 2012, of the Notice of Commencement of Environmental Screening and Review. A copy of the notice was also sent to the clerks of St. Clair Township. A copy of the Notice of Commencement that was published on July 30, 31 and August 1 and 9, 2012 is in Appendix A2.

The Wallaceburg Courier and the Sarnia Observer were chosen for publication of the notices because the project site is located in St. Clair Township. Both the Sarnia Observer and the Wallaceburg Courier are paid circulation news papers that have subscribers and other readers in the vicinity of the proposed project sites.

The Minister of Energy announced the relocation to St. Clair Township of the Green Electron Power Plant on July 10, 2012 by press release that was widely distributed to the news media and was extensively reported on as a result. The press release is attached in Appendix A1. Following the public announcement of the relocation of the Green Electron Power Plant there was additional consultation with key government and public agencies in preparation of the continuation of the public consultation process.

The regulations allow a proponent of a project to decide to proceed directly to the environmental review stage without issuing a screening report if there are potential environmental effects or public concerns that require further assessment and resolution. The potential impact of air emissions and noise impacts from the project were identified as requiring further assessment and resolution, and this was indicated as is required on the public notices.

Between August 2, 2012 and August 9, 2012 copies of the notice were delivered by mail to local residents and businesses within a 1600 meter radius of the project.

The notices gave the prospective locations and a brief description of the project, gave notice that the project would be going through the environmental screening process, invited members of the public to attend open house events on August 16 and September 12, 2012 and also provided contact information for anyone to obtain further information on the project.

Upon conclusion of the report on the Environmental Review, a notice of completion is to be published in the local papers and delivered to local residents and businesses. The notice will be published in the same newspapers and delivered to the same residents and business owners as the August 9, 2012 notice and additionally will be delivered or emailed to those members of the public who have indicated an interest in the project either by attending the open house or by contacting the proponent. This will also include any members of the public whose interest in the project was made aware to the proponent by a government body such as the Ministry of the Environment.

A copy of the Notice of Completion of Environmental Screening and Environmental Review, which is to be sent out, can be found in Appendix A2.

## 4. Open House

On August 16, 2012 and September 12, 2012 open houses for the Green Electron Power Project were held at the Courtright Community Hall, 1594 Third St., Courtright, Ontario, about 3 km north of the west project site and about 5 km north of the east project site.. Both events ran for 4 hours from 4 - 8 pm. At each event it was made clear that two sites were under consideration, gave each of their locations, and indicated that only one site would be chosen as the location of the project.

The purpose of the open house information session was to introduce and familiarize nearby residents, business owners and other interested citizens with the Green Electron Power Project, and to seek comments and concerns at this early stage of the environmental screening process in order that they be properly addressed in the environmental review

The general format of the open house was that upon arriving in the room in which the open house was held, members of the public were greeted and signed in by open house staff. This allowed the proponent to keep a record of how many individuals arrived and to create a database of attendees by collecting their contact information to ensure continued dispersal of information. At the time of sign-in open house attendees were given a one page summary of environmental impacts of the project and a questionnaire and told that they could read the environmental impact sheets, view the display boards spread around the room, ask questions and make comments to one of the experts available around the display boards. The attendees were also asked fill out and return the questionnaire before leaving by handing the completed questionnaire back to the open house staff. Several individuals requested to email, mail or fax their survey to allow them more time for comments.

An informal open house format was chosen over a lecture format because it would allow members of the public greater scheduling flexibility as it allowed the public to drop in to obtain information at their convenience. Also, this format provides a welcoming atmosphere for people without extensive expertise in electricity generating plants to become better informed about the project and to offer honest feedback. Many people would feel intimidated by having to ask questions and make comments at a microphone in front of a large gathering. The open house format was specifically designed to allow one-on-one contact between project experts and attendees. This method allowed the experts to respond to questions in detail and at length as well as allowing for all of an individual's questions to be addressed. The experts staffing the open house included four professional engineers, one biologist (Ph.D.), one architect, one geoscientist and one engineering student who were carefully briefed on the anticipated impacts of the project and also briefed on fostering reasonable dialogue with members of the general public who did not have as much knowledge or experience with electrical power plants similar to the one being proposed.

Generally the open houses ran smoothly with a high degree of cooperation by the public, with a frank and thorough discussion of the impacts of the project on their neighborhood and on the environment and with several exit surveys being substantially filled out. Approximately 36 individuals signed in and 24 completed surveys were handed in. Typical attendance time ranged from 15 minutes to over 1 hour. Several local politicians attended, including Mayor Steve Arnold, Deputy Mayor Peter Gilliland, Councillor Pat Carswell-Alexander and Councillor Darrell Randell.

Some of the issues raised by members of the public tended to center on their opinion that there might be better sites for such power plant and the affects that the plant would pose on the employment ratings. The most prevalent concerns expressed were about air quality impacts, noise impacts, visual impacts, distance to nearby residents and property value impacts. Otherwise the atmosphere of the open houses was positive with questions pertaining to general information about Green Electron and previous endeavors made by Eastern Power.

The display materials, summary of environmental impacts sheet and questionnaire are shown in Appendix A3.

## 5. Correspondence

As of October 19, 2012 only one piece of correspondence was received by the proponent from a member of the public. The letter writer indicated concerns about the construction traffic, construction personnel and noise involved with the project. The writer also indicated concern that he hoped the facility would not be built "close to the river" since "we have little environment left concerning waterfront". Finally the letter writer suggested that he would be open to the proponent purchasing his property so as to "eliminate concerns as Shell did". The concerns raised in the letter are all reasonably addressed by the Environmental Screening and Review Report. The Project will not be built on waterfront property and thus will not result in the disappearance of any natural waterfront areas. Construction workers will be supervised while on-site and thus will not pose any material safety risk for local residents. The traffic during construction can be reasonably accommodated by the existing roads and any noise from the project will be mitigated to meet the stringent night time limits.

•

## 6. Discussion of Issues Raised at the Open Houses

A full set of comments received from the 24 open house questionnaires is in Appendix A4.

The following is a summary of answers to the open house questionnaires. The question asked is shown in italics. The percentages shown are based on the 24 questionnaires handed in. The numbers in parenthesis after some comments indicate that substantially the same comment or concern as share by that number of exit survey respondents.

## General:

- 1. How did you hear about this Open House?
  - 50% of people heard about the open house by newspaper.
  - 4% of individuals heard about the open house by a notice at their door.
  - 4% of individuals heard about the open house by a website
  - 63% of individuals heard about the open house by an "other" method.
    - >by the radio
    - ➤ from a co-worker
    - >by email notice
    - > from a county council
    - > from the sign out front the community hall
- 2. Have you received/read the General Information sheet?
  - 96% of individuals had read the General Information sheet.
  - 4% had not read the General Information sheet
- 3. Are you familiar with the site for the Greenfield St. Clair Plant?
  - 92% of individuals responded that they were familiar with this.
  - 13% said that no, they weren't familiar with this.
- 4. How close to either Green Electron candidate site do you live or work? (please indicate H for home and W for work)

	West Site	East Site
0.5 km or less	21%	8%
0.6-0.9 km	8%	13%
1-2 km	29%	13%
Over 2 km	42%	46%

- 5. Did this Open House improve your familiarity with the various environmental emissions from the power plant?
  - 63% of the individuals responded that the Open House did improve it.
  - 38% of the individuals responded that they were not.
    - ➤ I was already informed due to previous exposure
    - Understand things better now
- Do you regard some options for electricity production as significantly worse from the environment or human health than others? If so, please indicate which ones you feel are worse.
  - 67% of the individuals indicated that they did regard it as significantly worse.
  - 25% of the individuals indicated that they did not regard it as significantly worse.

## Comments included:

- nuclear dangerous
- > coal, potentially hydro and wind
- > wind
- > coal, nuclear
- > coal, oil
- 7. Do you feel it is important to connect new power plants to the existing transmission lines so as to avoid running new high voltage lines through rural or urban areas and to also save on power costs?
  - 92% of the individuals answered yes.
  - 8% of the individuals answered no.

## Comments included:

- decreasing cost, efficiency, health
- I would expect new high voltage lines to be required sooner rather than later
- > If the current ones are adequate
- Put the damn thing in the GTA

## **Green Electron Power Plant Site:**

- 8. Are you aware that the Green Electron Power Plant must meet provincial noise and air emission regulations?
  - 96% of individuals indicated that they were aware of this.
  - 8% of respondents indicated that they were not aware of this.

#### Comments included:

- Not concerned with any emissions (3)
- > Should not meet, should Exceed (1)
- Provincial and federal regulated (1)

9. Are you concerned that the Green Electron Power Plant will have significant negative impacts? Please indicate your concerns.

## Air Quality:

- 17% of responses indicated that they were concerned with the air quality.
- 83% of responses indicated that they were not concerned with air quality.

#### Comments included:

- Traffic, dust, noise during construction (4)
- People in the area being subject to loss of sleep, peace of mind and heavy traffic (1)
- > minimal, clean energy (1)

#### Water Quality:

- 8% of responses indicated that they were concerned with water quality.
- 79% of responses indicated that they were not concerned with water quality.

## Comments included:

- Increases in water temperature (1)
- ➤ Where is the outtake into the river located? (1)
- ➤ Maybe? (1)
- Not sure, no information provided (1)

## Noise Emission:

- 17% of responses indicated that they were concerned with noise emissions.
- 79% of responses indicated that they were not concerned with noise emissions.

## Comments included:

- ➤ Will be in immediate area of my house/shop (2)
- > minimal, few residents (1)
- > not a significance (2)
- Steam from Greenfield is too loud (1)
- will see later when open/running (2)

#### Other:

- Young women will be close to construction and subject to crime from transient workers (1)
- Price (1)
- Loss of employment from OPG (1)
- Loss of employment from present plant (3)

## Economy:

- 10. Should Ontario be able to supply all of the electricity it consumes?
  - 92% of individuals responded yes to this question.
  - 8% of individuals responded no to this question.

## Comments included:

- > maintain the level of maximum capacity output and surplus (1)
- they are currently have too much and very expensive (1)
- 11. Are you concerned about electricity it consumes?
  - 46% of individuals indicate that they were concerned.
  - 54% of individuals indicated that they were not concerned.

#### Comments included:

- due to an overloaded transmission system, hydro give frequent blips (3).
- not at present but as economy picks up and industry ramps up, different story (2)
- Ontario has an abundance of power which we are selling to the US at a loss according to recent news paper article we have read (1)
- 12. Are you concerned about the cost of electricity rising?
  - 96% of respondents were concerned with this.
  - 4% of responses were not concerned with this.

#### Comments included:

- > I don't believe we should be overloaded with wind turbines (1)
- > Too expensive (2)
- 13. Are you in favor of economic growth and industry growing?.
  - 92% of respondents indicated that they are in favor.
  - 4% of respondents indicated that they are not in favor.

#### Comments included:

- > Yes, if property planned and not purchased through any cost (1)
- We have enough in southwest Ontario (2)
- 14. Do you feel that a cleaner secure energy supply will promote economic development and prosperity for St. Clair, Lambton and Ontario in general?
  - 83% of individuals responded that they did.
  - 17% of individuals responded that they did not.

## Comments included:

- > yes but not wind (2)
- in short term likely, buy maybe not in the long term (4)
- > the energy supply is already in place (3)

## **Information Provided:**

- 15. Do you feel that this open house and the information provided has been helpful to you?
  - 96% of the responses indicated that information was helpful.
  - 4% of the responses indicated that the information was not helpful.

#### Comments included:

- Yes, very informative (4)
- Very professional staff (4)
- 16. Do you have other concerns or comments at this time?
  - 13% of individuals indicated that there were no other comments.
  - 75% of individuals indicated that they did have additional concerns.

#### Comments included:

- ➤ I am a supporter of a construction site that has room for adding addition capacity (1)
- > time will tell (2)
- surface water/extracting infrastructures/prefer west site (4)
- will running these types of plants result in a reduction in the administrative costs pm electricity bills due to Ontario hydro (1)
- 17. Would you like additional information?
  - 46% of individuals indicated that they would like additional information.
  - 50% of individuals indicated that they would not like additional information.

## Comments included:

- ➤ Where, when start/finish (6)
- Anything about your company history or press releases concerning this particular site would be appreciated (6)
- Contact information for those requesting engineering service or construction support (1)
- > which site will you choose and why? (6)

## APPENDIX - A1

## MNISTRY OF ENERGY PRESS RELEASE

## **Statement from Ontario Minister of Energy**

http://news.ontario.ca/mei/en/2012/07/statement-from-ontario-minister-of-energy.html

July 10, 2012 3:00 PM

Today, Chris Bentley, Minister of Energy, issued the following statement on the Greenfield South Power natural gas plant:

"Last year, after listening to the community's concerns, our government made a commitment to residents in Mississauga and Etobicoke to relocate the Greenfield South Power natural gas plant. The commitment was supported by both opposition parties.

Today, I am pleased to announce that the Ontario Power Authority (OPA) has reached an agreement with Greenfield to relocate the plant. The government has accepted the OPA's recommendation to relocate the 300 megawatt natural gas plant on part of Ontario Power Generation's Lambton Generating Station site.

The new site will take advantage of existing transmission and other infrastructure, as well as the expertise of local workers. The construction of the plant is expected to provide up to 200 jobs over the next two years.

I would like to thank the OPA and Greenfield Power for the work they have done over the past several months to reach this agreement.

The total cost of relocation is approximately \$180 million. This includes a settlement agreement with EIG, the financier of the Greenfield South Power project, on behalf of Greenfield, the OPA and the Province. The settlement is necessary in order to relocate the plant and resolves all outstanding legal proceedings. The total relocation cost also includes all payments made in relation to the original site, including construction costs, design costs, and permitting costs.

Today's announcement helps support Ontario's plan to modernize the Province's electricity infrastructure, clean up the air we breathe and end the use of coal by 2014."

## **CONTACTS**

- For media inquiries call:
- Jennifer Kett
   Minister's Office
   416-327-6747
   jennifer.kett@ontario.ca
- Georgina Kourakos
   Communications Branch

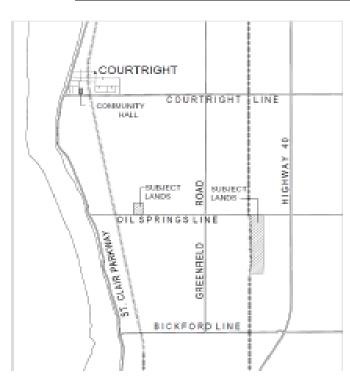
416-325-0294

georgina.kourakos2@ontario.ca For public inquiries call: TTY: 1-800-239-4224 1-888-668-4636

Ministry of Energy

## APPENDIX - A2 - PUBLIC NOTICES AND INFORMATION

## NOTICE OF COMMENCEMENT OF ENVIRONMENTAL SCREENING AND REVIEW



Greenfield South Power Corporation, an affiliate Eastern Power Limited, is planning to construct and operate a fueled. natural gas electricity generating facility (nominal capacity 300 MW) at one of two sites on Oil Springs Line., St. Clair Township (see map). This power project will improve electricity supply in Ontario.

The main components of this combined cycle facility will be a gas turbine, heat recovery boiler, a steam turbine, cooling tower and an electrical substation. The facility will be connected to the 230 kV

Hydro One electricity transmission grid adjacent to the site and receive natural gas from nearby supply lines. The facility will be operated by qualified stationary engineers and will meet all applicable regulations, by-laws and legislation.

This project is subject to the Ontario Ministry of the Environment's environmental assessment requirements for electricity projects. The Environmental Screening of the project will be directly entering the Environmental Review stage in which the air and noise emissions will be subject to more detailed study. You are invited to attend open houses to obtain further information and to discuss this project:

Thurs., August 16th and/or Wed., September 12, 2012 from 4 – 8 pm at the Courtright Community Hall 1594 Third St. Courtright ON NON 1HO

To comment on this project, or for more information, please contact:

Hubert S. Vogt, Vice President Eastern Power Limited 2275 Lake Shore Boulevard West, Suite 401 Toronto, Ontario M8V 3Y3

Tel: 416-234-1301 Fax: (416) 234-8336 E-mail: hvogt@easternpower.on.ca

## NOTICE OF COMPLETION OF ENVIRONMENTAL REVIEW



Greenfield South Power Corporation, an affiliate of Eastern Power Limited, is proposing to construct and operate a natural gas fueled electricity generating facility (nominal capacity 300 MW) at one of two sites on Oil Springs Line, St. Clair Township (see map). This power project will improve electricity supply and facilitate phasing out of coal-fired electricity generation in Ontario.

The main components of this combined cycle facility will be a gas turbine, heat recovery boiler, steam turbine, cooling tower and, electrical substation. The facility will be connected to the 230 kV Hydro One electricity transmission grid directly adjacent to each of the project site and receive natural gas from nearby supply lines. The facility will be operated by qualified stationary engineers and will meet all applicable regulations, by-laws and legislation.

This project is being reviewed under the Ontario Ministry of the Environment's environmental screening process for electricity projects, including an Environmental Review stage in which the air and noise emissions were subject to more detailed study.

The environmental screening and review has found that with the mitigation measures detailed in the Environmental Screening and Review Report, the project will not have Net Effects and the proponent intends to proceed with the project subject to mitigation and other approvals. The Environmental Screening and Review Report may be viewed at <a href="www.greenelectron.ca">www.greenelectron.ca</a> or at the following locations:

St. Clair Township Municipal Offices 1155 Emily Street, Mooretown ON (519) 867-2021 Lambton Library Corunna Branch 417 Lyndoch Street, Corunna, ON (519) 862-1132

If there remain environmental concerns regarding the project, please raise them with the proponent in writing:

Hubert S. Vogt, Vice President, or Bruce E. Holbein Ph.D., Environmental Manager Eastern Power Limited 2275 Lake Shore Boulevard West, Suite 401 Toronto, Ontario M8V 3Y3 Tel: 416-234-1301 Fax: (416) 234-8336

E-mail: info@greenelectron.ca Web Site: www.greenelectron.ca

If the matter is not reasonably resolved, a written request may be made to the Director of the Environmental Assessment and Approvals Branch, Ontario Ministry of the Environment, (2 St. Clair Ave West, Floor 12A, Toronto, M4V 1L5), to elevate the project to an individual environmental assessment. An elevation request must be made in accordance with the provisions set out in the MOE's Environmental Screening Process for Electricity Projects, with a copy sent to the proponent. The last day that comments or elevations requests will be received is December 6, 2012.

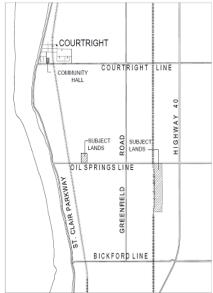
## APPENDIX <u>A3</u> OPEN HOUSE MATERIALS

## **Green Electron Power Plant**

First Open House August 16, 2012



## NOTICE OF COMMENCEMENT OF ENVIRONMENTAL SCREENING AND REVIEW



Greenfield South Power Corporation, an affiliate of Eastern Power Limited, is planning to construct and operate a natural gas fueled electricity generating facility (nominal capacity 300 MW) at one of two sites on Oil Springs Line., St. Clair Township (see map). This power project will improve electricity supply and facilitate phasing out of coal-fired electricity generation in Ontario.

The main components of this combined cycle facility will be a gas turbine, heat recovery boiler, a steam turbine, cooling tower and an electrical substation. The facility will be connected to the 230 kV Hydro One electricity transmission grid

diagram to the project site and receive natural gas from nearby supply lines. The facility will be operated by qualified stationary engineers and will meet all applicable regulations, by-laws and legislation.

This project is subject to the Ontario Ministry of the Environment's environmental assessment requirements for electricity projects. The Environmental Screening of the project will be directly entering the Environmental Review stage in which the air and noise emissions will be subject to more detailed study. You are invited to attend open houses to obtain further information and to discuss this project:

Thursday, August 16th and/or Wednesday, September 12, 2012 from 4 – 8 pm at the Courtright Community Hall 1594 Third St. Courtright ON NON 1HO

To comment on this project, or for more information, please contact:

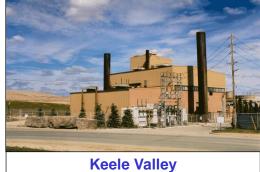
Hubert S. Vogt, Vice President Eastern Power Limited 2275 Lake Shore Boulevard West, Suite 401 Toronto, Ontario MBV 3Y3 Tel: 416-234-1301 Fax: (416) 234-8336

E-mail: hvogt@easternpower.on.ca

### **Eastern Power – Over 20 Years Successfully Serving Ontario's Power Needs**



**Renewable Power for Pickering** since 1991



**Renewable Power for Vaughan** since 1995

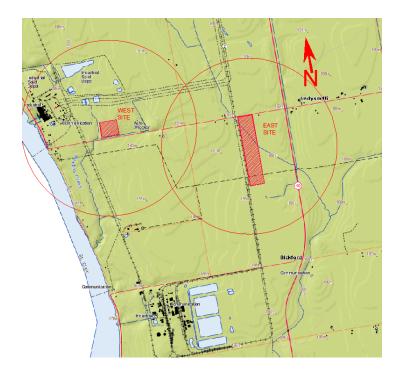


### **Green Electron - Eastern Power**

- > Since 1985
- > 100% Ontario-owned
- > Ontario based
- > Principals are Professional Engineers
- > Build, own and operate power plants
- > Environmental and Engineering Awards



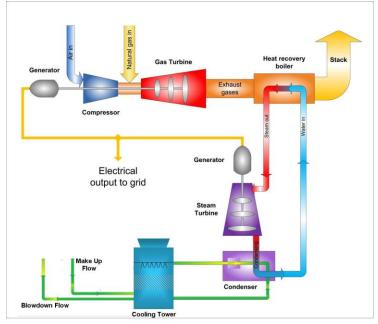
### **Green Electron Power Plant Location**



County of Lambton



### **Green Electron Power Plant Process**



Combined Cycle Process Diagram

http://www.knottingleypower.co.uk/wp-content/uploads/2011/01/CCGT-Diagram-Updated.jpg



### **Green Electron Power Plant Process**

- Compact, approx. 300 MW size
- Similar to Industrial Neighbours
- Clean; releases very low amounts of pollutants and clean water vapour
- High Efficiency Combined Cycle
- Beside existing electrical transmission line
- Beside existing natural gas supply



### **Green Electron Power Plant Construction**

- 24 months construction
- Net positive environmental impact
- Improved energy supply for Ontario
- A new clean generation facility
- Economic benefits to St. Clair, Lambton



# **Green Electron Noise Mitigation Features**

- Designed to meet urban setting
- Stack and Air Inlet Silencers
- Gas Turbine Indoors
- Acoustically Insulated Building
- Steam Vented to Condenser



# **Green Electron Natural Gas Power Emissions Comparison**

Emission	Natural Gas Reduction vs. Coal
NO <sub>2</sub>	78% ↓
SO <sub>2</sub>	95% ↓
Particulates	99% ↓
Mercury	100% ↓
CO <sub>2</sub>	<b>52%</b> ↓

NREL 2000, Life cycle assessment of a natural gas combined-cycle power generation system (NREL/TP-570-27715)



## GREEN ELECTRON POWER PROJECT GENERAL INFORMATION

The Green Electron Power Project provides a new, clean, high-efficiency, compact, electricity generating facility for Ontario. This project is part of the Ontario government's program to improve air quality by phasing out coal-fired electricity generation in Ontario. To be located in St. Clair Township at one of two sites on Oils Springs Line near Greenfield Road, the new plant will be fueled by natural gas. This plant is expected to operate only during periods of high and intermediate electricity demand, (eg. daytimes on non-holiday weekdays).

The new facility will be similar in appearance and quality to its other nearby industrial neighbours and its flue gas stack will only be about 43 meters high.

This new facility will be clean because its emissions will be just a fraction of those from a coal-fired facility of similar size. Toxic mercury emissions from coal burning, that have been a human health concern for many years, will be completely eliminated. Particulates, sulphur dioxide and nitrogen dioxide emissions that greatly affect our air quality, will be reduced by about 80% - 95%. In fact, the highest projected concentration of NO<sub>2</sub> emission from the new facility will be less than 10% of the maximum permitted under Ontario's Environmental Protection Act. Greenhouse gas emissions will be reduced by about 50%, therefore contributing to Canada's commitments on climate change. The construction of this project will facilitate the complete phasing out of Ontario's coal-fired generating stations. It is estimated that the phase out of these coal fired stations will in each year prevent an average of 660 premature deaths, 920 hospital admissions and 1,090 emergency room visits, and will save about \$ 371 million annually in environmental related damages.

The new generating facility will use modern, high-efficiency, low NOx, combined-cycle technology, consisting of a gas turbine-driven electricity generator, heat recovery boiler, steam turbine driven electricity generator, and condenser/cooling tower. The facility will be designed to reduce noise emissions so as to meet municipal and provincial standards. Noise reduction features include inlet air silencing for the gas turbine, enclosure of major plant equipment, either inside buildings or within acoustical enclosures, and sound absorbing insulation for the heat recovery boiler.

A key reason for locating the facility in St. Clair Township is the close proximity to an existing high-voltage electrical transmission line and natural gas pipeline for direct interconnections. The plant will also make excellent use of industrially zoned lands which allow electricity generation.

Construction of the facility is expected to last about 24 months and will involve typical medium industrial construction methods. Best practical techniques will be used to prevent negative off-site impacts. The facility will result in only minor long-term changes in vehicle traffic density due to the plant staffing of about 6 persons on weekdays and 2 on weekends, nights and holidays, as well as from occasional deliveries of maintenance and operating supplies.

The project will bring to St. Clair Township and Lambton County highly skilled jobs, increased industrial property tax revenues, improved energy supply stability and other local area economic benefits. The local purchase of supplies and services, as well as other local spending, is expected to inject over \$3.8 million dollars annually into the local economy and create economic spin-off benefits of up to 4 times this amount.

### APPENDIX A4: IMAGES OF THE OPEN HOUSE ON AUGUST 16, 2012







### **Green Electron Project ESRR**

17.8 APPENDIX 17.8 - Government Agency Consultation Report

# **Green Electron Power Project Environmental Screening and Review Process**

# **Government Agency Consultation Report**

November 5, 2012

Prepared by: Monika T. Vogt, BSc Reviewed by: Bruce E. Holbein, Ph.D. Approved by: Hubert S. Vogt, P.Eng

## **GREEN ELECTRON POWER PROJECT Government Agency Consultation Report**

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	NOTICES AND INFORMATION PROVIDED TO GOVERNMENT ICIES

#### 1. Introduction

This report documents the public consultation process required as part of the environmental screening process for the Green Electron Power Project (the project). The environmental screening process is applicable to the Green Electron Power Project because it is a Category B electricity project under Ontario Regulation 116/01 of the *Environmental Assessment Act*.

The proponent of the Green Electron Power Project is Greenfield South Power Corporation.

The Green Electron Power Project is part of the Ontario Government's initiative to improve air quality in Ontario by phasing out the use of coal-fired electricity generation. To offset this loss of generating capacity in Ontario, the Ministry of Energy issued a Request for Proposals (RFP) in August 2004 for offers of "clean energy supply" and demand management projects. The Green Electron Power Project is a result of that process.

The purpose of government agency consultation is to "inform and receive input from all government agencies with jurisdiction or a program interest related to a particular electricity project". The proponent, in consultation with government agencies, identified twenty one (21) government agencies that might reasonably have jurisdiction over the project or might have a program interest in the project, and they are listed in Appendix H-A1. This report documents the steps taken by the proponent of the project to seek consultative input and also comply with the agency consultation set out in Ontario Regulation 116/01.

The major components of the government agency consultation process for the Green Electron Power Project included:

- 1. Meetings with government bodies and agencies;
- 2. A specific outreach/consultation process with First Nations
- Written information that was mailed or e-mailed to various government bodies and agencies, depending on the contact information that was provided, as per O.Reg 116/01;
- 4. Public open house events for the project held on August 16, 2012 and September 12, 2012 which were attended by some representatives from government bodies and agencies;
- 5. Copies of public notices that were sent to government bodies and agencies;
- 6. Correspondence between the government agencies and the proponent;
- 7. The provision of a draft of the Environmental Screening and Review Report to the Ministry of the Environment (MOE) for review;
- 8. The provision of the completed Environmental Screening and Review Report to various government agencies, i.e., as had requested receipt of a copy of this report.

Twenty one agencies were identified within federal, provincial, regional and municipal jurisdictions for consultation as per O.Reg 116/01. These agencies have been provided

with copies of the mandatory notices as well as all information as given to the public. First Nations with potential interest in consultation about the project were identified through meetings and discussions with St. Clair Township officials, Ontario Power Authority officials and officials of the Ministry of Environment. Greenfield South Power Corporation understands that the MOE has Crown responsibility for First Nation consultation (to be carried out by the proponent) for this project.

### 2. Project Description

The Green Electron Power Project involves the construction and operation of an electricity generating plant that was proposed in response to the Ontario Ministry of Energy's Request for Proposals for new clean energy supply to facilitate the phasing-out of coal-fired electricity generation in Ontario. The project was selected by the Ontario Ministry of Energy and is expected to be in-service by 2014. The plant will have a capacity of about 300 MW configured as a combined cycle power plant to be fueled with natural gas. The project will be located in St. Clair Township on one of two sites on Oil Springs Line near Greenfield Road (see Fig. 2.1) on land that is zoned for power generation uses. The sites are each located adjacent to one of Hydro One's 230 kV high voltage electricity transmission corridors.

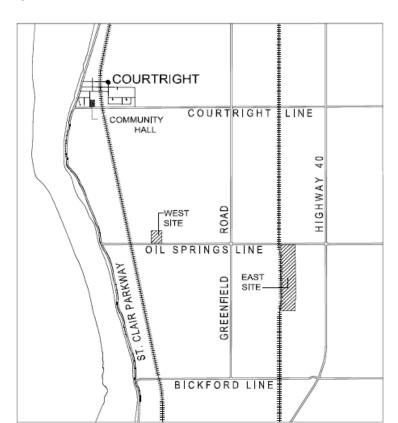


Figure 2.1 - Location of Proposed Green Electron Power Project

The configuration of the power plant will utilize one gas turbine generator set and the exhaust gas from the gas turbine will be ducted to a water-tube, heat recovery steam generator (HRSG) equipped with a duct burner fuelled by natural gas. The steam from the HRSG will drive a steam turbine generator set. The plant will also include steam condensing equipment, steam condensate and boiler feed water equipment, as well as a boiler make-up water treatment system, associated electrical and control equipment and a high voltage transmission interconnection.

# 3. Notices and Information Provided to Government Agencies

The Notice of Commencement of an Environmental Screening was sent to the clerk of the St. Clair Township on August 9, 2012. This notice was also published on July 30, 31, and August 1, 2012 in the Sarnia Observer and on August 9, 2012 in the Wallaceburg Courier. The notice gave the location and a brief description of the project, gave notice that the project would be going through the environmental screening process, invited interested individuals to attend either or both of two open house information sessions on August 16, 2012 or September 12, 2012 and invited individuals to contact the proponent for additional information as desired.

Representatives of the proponent met with the Mayor, Deputy Mayor and key planning and development staff of the St. Clair Township and Lambton County on July 16, 2012, to inform the Township about the proposed project and to seek advice as to requirements under the Planning Act that would apply to the project, and to seek advice as to which other municipalities and/or planning authorities should be advised of the project. On August 13, 2012 the proponent also gave a presentation about the project at the August 13, 2012 meeting of the full St. Clair Township Council.

On July 25, 2012 a representative of the proponent attended a meeting with the development staff of St. Clair Township to discuss the need for minor variances in regards to set backs and height limits and to determine what would be acceptable to the Township. An application for minor variances for the east site was filed with the Township shortly thereafter and on August 27, 2012 the Committee of Adjustment for St. Clair Township approved the minor variances.

Shortly after the relocation of the Green Electron Power Project was announced, the notice of commencement of screening was published in the local newspapers which also indicated that the project would be directly entering the environmental review stage of the environmental screening process. The regulations allow a proponent of a project to decide to proceed directly to the environmental review stage without issuing a screening report if there are potential environmental effects or public concerns that require further assessment and resolution. The potential impact of air emissions and noise impacts from the project were identified as requiring further assessment and resolution, and this was indicated as is required on the public notices. This notice was also sent on July 26, 2012 to the Chiefs of the two First Nations located closest to the sites (Aamjiwnaang First Nation and Walpole Island First Nation) and more recently on August 29, 2012 to the Kettle and Stoney Point First Nation and Oneida First Nation, and on September 11,

2012 to the Chippewas of the Thames First Nation, Munsee-Delaware First Nation, Moravian of the Thames First Nation and Caldwell First Nation. On September 25, 2012, a letter was sent by courier to the to the respective Chiefs of the Aamjiwnaang First Nation, the Kettle and Stoney Point First Nation, Oneida First Nation, Chippewas of the Thames First Nation, Munsee-Delaware First Nation, Moravian of the Thames First Nation and Caldwell First Nation. These letters informed the recipients that the Environmental Screening Report was being finalized and requested that if there were any final environmental concerns with respect to the Green Electron Power Project for them to forward these to the proponent, and also offering to meet with any First Nation. The Walpole Island First Nation chief received a separate letter, sent on September 25, 2012, by courier, speaking of points brought up in a meeting that was held between them and senior representatives of the proponent. This letter additionally requested that if there were any additional concerns regarding the Green Electron Power project to contact the president of the proponent company.

On October 15, 2012 the president of the proponent telephoned all the First Nations that had not responded to the earlier letters to request a meeting with the Chiefs in order to discuss the Green Electron Power Project.

Upon contacting each of the First Nations, Mr. Vogt requested to speak with the Chief directly. Details of each telephone call by Mr. Vogt to each First Nations can be seen on Table 3.1 of Appendix A3 on pages 65-72.

On August 9, 2012 the Notice of Commencement of Screening was emailed, or mailed if an email address was not available, to all government agencies listed in Section 4 of this report asking that they respond in writing before September 15, 2012 so that the comments and concerns be properly addressed in the environmental screening process. The comments that were received from the government agencies are summarized in Section 4 of this report. A copy of the letter is in Appendix A2 of the Public Consultation Report.

On September 25, 2012 a letter was sent by email or mail to all government agencies listed in Section 4 of this report, who had not yet responded to the previous letter. This letter indicated that the Environmental Screening Report was being finalized, and if there were any concerns about the Green Electron Power Project to respond as soon as possible.

All responses from Government Agencies received by the proponent by November 2, 2012 have been addressed in this report.

In addition, senior company officials visited the office of the St. Clair Region Conservation Authority (SCRCA) on August 13, 2012 to review the project with SCRCA officials and seek input as to any comments or concerns they might have.

Senior company officials also met personally with Chief Kewayosh of the Walpole Island First Nation and other senior First Nation officials to review the project with them, invite them to the two open house events and to seek any comments they might have on the project.

On November 2, 2012 a draft of the Environmental Screening and Review Report (ESRR) was couriered to the Walpole Island First Nation for their review and any

comments or concerns they might have. The transmittal letters can be found in Appendix A3.

The possibilities for local employment of community members including First Nation residents was discussed in particular.

A first meeting was held with the MOE on July 30, 2012 where representatives of the EAAB and representatives of both the MOE district and regional offices met with the proponent and discussed the project. This was then followed by various telephone conferences, meetings and exchanges of information leading to submission of a draft ESRR on Sept 20, 2012 for additional MOE consultative review input prior to finalization and issuance of a statement of completion to the MOE, and, leading to the 30 day public review phase.

Upon completion of the Environmental Screening and Review Report, a notice of completion is to be published in the local newspapers and mailed and emailed to all affected government agencies. A copy of the Notice of Completion of Environmental Screening and Environmental Review, which is to be sent out, can be found in the Public Consultation Report.

### 4. Meetings with Government Agencies

AGENCY	DATE	COMMENTS
St. Clair Township and Lambton County	July 16,2012	Attended by the Mayor and Deputy Mayor of St. Clair Township, as well as key development staff of St. Clair Township and Lambton County
St. Clair Township	July 25 2012	Meeting with the development staff of St. Clair Township regarding minor variances
Ministry of the Environment (at Southwest Region offices in London, Ontario0	July 30, 2012	Attended by EA Coordinator for Southwest Region and Senior Program Support Coordinator of the Environment Assessment and Approvals Branch [Bruce to complete and check] as well as By teleconference from Toronto
Ministry of the Environment	July 30, 2012	Meeting in London with EAAB , Regional and District MOE officials
St. Clair Region Conservation Authority (SCRCA)	August 13, 2012	Attended by staff of the SCRCA Environmental and Permit planning officials as well a technical officials
St. Clair Township Council	August 13,2012	Gave a presentation and answered questions posed by several members of council

### **5. Summary of Government Agency Comments and Responses**

Agency/comment date	Comment see Appendix A2 for copies of correspondence	Response see Appendix A2 for copies of correspondence
Ministry of Tourism, Culture and Sport October 4, 2012	Thank you for your follow up email. Our apologies for the delay in response time.  As this is a review, it does not fall within our Ministry's jurisdiction. Please contact the Ministry of the Environment or else the Environmental Commissioner of Ontario.	The Ministry of the Environment has been consulted as suggested.
Ministry of Energy and Infrastructure	Thank you for circulating Infrastructure Ontario (formerly the Ontario Realty Corporation) on your notice for a proposed clean electricity generating station. Infrastructure Ontario (IO) is the strategic manager of the government's real estate property with a mandate of maintaining and optimizing value of the portfolio, while ensuring real estate decisions reflect public policy objectives of the government.  **As you may be aware, IO is responsible for managing real estate property that is owned by the Ministry of infrastructure (MOI). Our preliminary review of your notice and supporting information indicates that IO-managed property is directly in the study area. As a result, your proposal may have the potential to impact this property and/or the activities of tenants present on IO-managed lands. Please note that Hydro One managed lands, on behalf of IO, are also in the study area and are subject to the same requirements as those directly managed by IO. Attached please find a map that identifies these properties to assist you in identifying and avoiding potential impacts on IO-managed lands.	The map provided by IO will be used to identify and avoid potential impacts on IO-managed lands.

### **Potential Negative Impacts to IO Tenants and Lands General Impacts**

Negative environmental impacts associated with the project design and construction, such as the potential for dewatering, dust, noise and vibration impacts, and impacts to natural heritage features/habitat and functions, should be avoided and/or appropriately mitigated in accordance with applicable regulations best practices and Ministry of Natural Resources (MNR) and Ministry of the Environment (MOE) standards. Avoidance and mitigation options that characterize baseline conditions and quantify the potential impacts should be present as part of the EA project file. Details of appropriate mitigation, contingency plans and triggers for implementing contingency plans should also be present.

Any negative environmental impacts associated with the project design and construction, such as the potential for dewatering, dust, noise and vibration impacts, and impacts to natural heritage features/habitat and functions, will be avoided and/or appropriately mitigated in accordance with applicable regulations best practices and Ministry of Natural Resources (MNR) and Ministry of the Environment (MOE) standards. Avoidance and mitigation options that require characterization of baseline conditions and quantification of the potential impacts will form part of the EA project file. Where required, details of appropriate mitigation, contingency plans and triggers for implementing contingency plans will also form part of the project file.

#### **Impacts to Land holdings**

Negative impacts to land holdings, such as the taking of developable parcels of IO managed land or fragmentation of utility or transportation corridors, should be avoided.

If the potential for such impacts is present as part of this undertaking, you should contact the undersigned to discuss these issues at the earliest possible stage of your study.

If takings are suggested as part of any alternative these should be appropriately mapped and quantified within EA report documentation. In addition, details of appropriate mitigation and or next steps related to compensation for any required takings should be present.

The project will not require the taking of any IO managed land or require any fragmentation of utility or transportation corridors.

#### Potential Triggers Related to MOI's Class EA

IO is required to follow the MOI Class Environmental Assessment Process for Realty Activities Not Related to Electricity Projects (MOI Class EA). The MOI Class EA

applies to a wide range of realty and planning activities including leasing or letting, planning approvals, disposition, granting of easements, demolition and property

maintenance/repair. For details on the MOI Class EA please visit the Environment and Heritage page of our website found at the following internet link:

http://www.infrastructureontario.ca/What-We Do/Buildings/Realty-Services/Environmental-Management/Class-EAs/. If the MOI Class EA is triggered, and deferral to another ministry's or agency's Class EA or individual EA is requested, the alternative EA will be subject to a critical review prior to approval for any signoff of a deferral by the proponent. The alternative EA needs to

fulfill the minimum criteria of the MOI Class EA. When evaluating an alternative EA there must be explicit reference to the corresponding

Although no MOI Class EA is expected to be triggered, should any MOI Class EA be required the actions recommended by MOI will be followed.

undertaking in the MOI Class EA ( <i>e.g.</i> , if the proponent identifies the need to acquire land owned by MOI, then "acquisition of MOI-owned land", or similar statement, must be referenced in the EA document). Furthermore, sufficient levels of consultation with MOI's/IO's specific stakeholders, such as the Ontario Ministry of Natural Resources, must be documented with the relevant information corresponding to MOI's/IO's undertaking and the associated maps. In addition to archaeological and heritage reports, a Phase I Environmental Site Assessment (ESA), on IO lands should also be incorporated into the alternative EA study. Deficiencies in any of these requirements could result in an inability to defer to the alternative EA study and require completing MOI's Class EA prior to commencement of the proposed undertaking.	
Green Energy Act and Associated Projects Undertakings that involve the planning, designing, establishing, constructing, operating, changing, expanding or retiring of a renewable energy generation facility or renewable energy testing facility is exempt from following the MOI Class EA process. To obtain approval, these projects have a specific EA process that exempts these projects from the IO, MOI EA process.	The project does not involve the planning, designing, establishing, constructing, operating, changing, expanding or retiring of any renewable energy generation facility or renewable energy testing facility.
Deferral to an alternative EA including the Renewable Energy EA Once a renewable energy approval has been granted, or deferral to another EA, for a project that will impact IO managed lands meets all MOI requirements, the proponent will be required to complete IO's "Application of Client Ministry or Agency's Class EA or Declaration Order" form. All documentation, backup information, approvals and any required permits, associated with the Green Energy Act or alternative EA approval is to be provided to IO, prior to any development or construction, on the proposed lands,	The project does not involve the planning, designing, establishing, constructing, operating, changing, expanding or retiring of any renewable energy generation facility or renewable energy testing facility.

	managed by IO.	
	Additional Studies Outside of an EA Process Gaps may still exist, that are not necessarily evaluated by the Green Energy Act or the alternative EA. IO may require additional reports, or studies to satisfy any due diligence concerns. For example, should the proposed activities impact cultural heritage features on IO managed lands, a request to examine cultural heritage issues, which can include the cultural landscape, archaeology and places of sacred and secular value, could be required prior to commencement of the renewable energy project. This requirement may be independent and outside of any EA process.	The project will not impact any cultural heritage features of any IO managed lands.
	Concluding Comments  If the project directly affects all or in part any IO-managed property, please send the undersigned a copy of the DRAFT EA report and allow sufficient time (minimum of 30 calendar days) for comments and discussion prior to finalizing the report. Thank you for the opportunity to provide initial comments on this undertaking. If you have any questions on the above I can be reached at the contacts below.	The project will not directly affect any IO-managed property.
Canadian Environmental Assessment Agency	RE: Greenfield South Power Corporation's natural gas-fired electrical generating facility (300 MW), St. Clair Township, near Sarnia, Ontario  I am writing in response to your letter dated September 4 about the	Meetings were held with the CEAA/MOE Sept 21, 2012, information including a draft CEAA-compliant project description, the Green Electron project draft ESRR
September 17, 2012	above-noted project.  As part of the Government of Canada's plan for Responsible Resources	and draft public and the ESRR appendices government agency consultation reports were provided
	Development which seeks to modernize the regulatory system for project	for review.

reviews, the former *Canadian Environmental Assessment Act* was repealed when the new *Canadian Environment Assessment Act*, 2012 (CEAA 2012) can into force on July 6, 2012.

Under CEAA 2012, a federal environmental assessment may be required for those project listed in the *Regulations Designating Physical Activities* (the Regulations). The construction, operation, decommissioning and abandonment of a fossil fuel-fired electrical generating station, with a production capacity of 200 MW or more, is listed in the Regulations.

Subsection 8. (1) of CEAA 2012 required the proponent of a designated project to submit a description of the project to the Agency. The information that must be included in a project description is set out in the *Prescribed Information for the Description of a Designated Project Regulation*. Based on that information, the Agency would determine whether a federal environment assessment is required and, if so, ensure that such an assessment is conducted.

For more information about CEAA 2012, including how to prepare and submit a project description, please refer to the Agency's website at: <a href="https://www.ceaa-acee.gc.ca">www.ceaa-acee.gc.ca</a>

Staff in our office would be pleased to meet with Greenfield South Power Corporation and/or Eastern Power Limited to discuss CEAA 2012, the Regulations and proposed project. Please do not hesitate to contact me at 416-952-1576 or via email at Anjala.Puvananatha@ceaa-acee.gc.ca to set up meeting.

Sincerely Anjala Puvananatha, Director Canadian Environmental Assessment Agency, Ontario Region Formal submission of a project description for CEAA review was made on October 16, 2012 after discussion with CEAA officials and CEAA review of draft materials

Ministry of the Environment October 12, 2012	Green Electron Power Project Oil Springs Road, St. Clair Township, Ontario <u>Draft Environmental Screening And Review Report, Dated September 20<sup>th</sup>, 2012</u>	
	Section 4.1, Surface Water, Pgs. 15-16	
	This ministry has noted that the exact means of sewage effluent discharge is not fully defined as yet for this project. One alternative, identified in the Draft Environmental Review Report, is to route sewage to the Courtright Waste Water Treatment Plant. Other alternatives identified include: treating sewage on-site and routed to the Government Drain No. 10 adjacent to the facility, or to the drainage canal at CF Industries, or to a new outfall in the St. Clair River.	Subsequent to the draft dated Sept 15, 2012 the proponent has decided after consultation with the MOE to no longer pursue discharge of treated wastewater to Government Drain No. 10 for the East site or Hawkins drain for the West site.
	Section 1.6.4.2 of the 2005 Provincial Policy Statement states that:  "Municipal sewage services and municipal water services are the preferred form of servicing for settlement areas. Intensification and redevelopment within settlement areas on existing municipal sewage services and municipal water services should be promoted wherever, feasible."	The option of a discrete new outfall to the St. Clair River has been determined to likely require longer term multi-jurisdictional approvals and is not being further pursued at this time. Nonetheless it remains a potentially viable future option.
	On Pg 32, in Section 3.1 Community Services or Infrastructure of the Draft Environmental Review Report, it is stated that:  "Lambton Area Water Supply staff and CF Industries officials have both indicated that existing water supply systems can accommodate the water supply requirements with the existing infrastructure. Additionally, St. Clair Township officials have confirmed that the Courtright WWTF has capacity to receive and treat the Green Electron project wastewater."	with treated water discharge to the canal at CF industries both remain

With respect to the option of directing sewage effluent to the Courtright Waste Water Treatment Plant, has the municipality confirmed to the proponent whether the two proposed sites for the Green Electron Energy Project are located within the current approved sanitary sewage service area associated with the Courtright Waste Water Treatment Plant? If one or the other of the two proposed sites is not located in the current approved sewer service area, is the Municipality willing to undertake an Addendum (as applicable) to the Courtright Waste Water Treatment Plant Class EA to facilitate expansion of the current sanitary sewage service area to service either one of the sites? Can the anticipated effluent generated by this proposed project meet the municipality's sewer use bylaw requirements? Has the proponent, in concert with the municipality, confirmed that the expected quality and quantity of effluent to be treated at the Courtright Waste Water Treatment Plant will not compromise the current performance and capacity of the Waste Water Treatment Plant? Is there sufficient "uncommitted" reserve capacity it the Courtright Waste Water Treatment Plant to service either site?

This ministry recommends that written confirmation with respect to all of Both options are assessed to have no the foregoing be sought by the proponent from the municipality including but not limited to confirmation that the municipality is willing to accept all the industrial / sanitary sewage waste water generated by this proposed facility at its municipal sewage treatment works. If the answer to all of the foregoing questions is "Yes", and given the content of Section 1.6.4.2 of the 2005 Provincial Policy Statement, is there any need for the proponent to further explore any other industrial / sanitary sewage treatment options with respect to this proposed project? Please advise this ministry accordingly.

With respect to the other surface water discharge options presented in the

wastewater and both options are subject to additional ongoing commercial considerations with the respective municipal and industrial service providers.

In the case of the Courtright WWTF it has been confirmed that their approvals presently do not permit receipt of the project's wastewater as this is outside of their present service area.

A draft services usage contract has been provided to the proponent for the use of the CF Industries (Terra Canada) outfall for wastewater discharge.

net negative impacts based on established performance for other similar power projects with similar treatment needs and especially with similar discharge routes in the case of use of the CF canal.

It is understood that municipal treatment would not require separate MOE compliance approvals.

Draft Environmental Review Report, water quality information should be provided with respect to the expected influent to be treated. The majority It is also understood that of this ministry's comments on surface water and this proposed project will be provided to the proponent once the proposed industrial sewage discharge information is provided to this ministry by the proponent. Ideally, this information should be provided to, reviewed and commented upon by ministry staff prior to the proponent issuing the Notice of Completion of the Environmental Review Report for this project. There is concern that process wastewater (including cooling water, blowdown from boilers and recycled flows) may be contaminated with oil/grease, TSS, metals, chlorine, sulphates, nitrates, high values of hardness, potentially low pH values and high temperature. Such potential contaminants need to be analyzed and if needed addressed with adequate treatment and the assimilative capacity analysis on the receiver and a defined mixing zone.

In short, the proponent should decide upon, define, and provide their rationale for the "actual means of sewage effluent discharge and treatment" that is being proposed for this project, including but not limited to the provision of all necessary technical background support studies for the option chosen. Ideally, this information should be reviewed and commented upon by ministry staff prior to the proponent issuing the Notice of Completion for this project.

Section 4.1 of the Draft Environmental Review Report also briefly describes the stormwater management strategy for this proposed project. The potential for accidental spills and leaks during both the construction and operational stages of this project that could conceivably allow contaminated runoff to enter Government Drain #10 should be addressed including appropriate mitigation measures during both stages (i.e. constriction / operation) in the Final Environmental Review Report.

treatment/discharge at CF industries would require MOE compliance approval. GSPC recognizes for this approval an application would be made detailing the water quality for treatment, the treatment process train and treated water quality in relation to establishing approval conditions.

The option of a discrete new outfall to the St. Clair River has been determined to likely require longer term multi-jurisdictional approvals and is not being further pursued at this time. Nonetheless it remains a potentially viable future option.

The proponent has received written confirmation from the Township for the willingness and capacity to accept the industrial sewage generated by the facility. This document is available in Appendix A4 page 132.

A draft services usage contract has been provided to the proponent for the use of the CF Industries (Terra Canada) outfall for wastewater discharge.

Due to an ongoing economic and logistical feasibility concerns, both options for discharge are still under consideration by the proponent

The process wastewater will not be contaminated with oil or grease. The process waste water will meet sewer use limts of the local municipality.

The potential contaminants mentioned have been reviewed, as has the assimilative capacity on the receiver and a defined mixing zone. This review has shown that the process waste water flow comprises less than 0.0004% of the flow of the St Clair River and thus is well with the assimilative capacity of the receiver within a reasonable mixing zone. The need for specific temperature and contaminant mitigation will be addressed in the

application for an Environmental Compliance Approval. Subsequent to the draft dated Sept 15, 2012 the proponent has decided to no longer pursue discharge of process blow down water to Government Drain No. 10. The need for specific temperature and contaminant mitigation will be addressed in the application for an **Environmental Compliance** Approval should this option be utilized. It is understood that municipal treatment would not require separate MOE compliance approvals. The additional Appendices 17.9 and 34.9 of the ERR provide an environmental management plan which includes provision for spill prevention and mitigation strategies for the project.

Section 4.3, Sedimentation and Soil, Shoreline or Riverbank Erosion	<u>.</u>
This ministry recommends that the proponent identify which Conservation Authority(ies) are active in this area and provide a record their consultation, if any, with these Conservation Authority(ies) pertaining to sedimentation and soil, shoreline or riverbank erosion.	Consultation with the SCRCA has occurred early in the project planning Section 4.3 has been revised to reference key responses of the St. Clair Region Conservation Authority as set out in greater detail in Table 5 of the Government Agency Consultation Report (Appendix 17.8./34.8 ##)
Section 4.4, Accidental Spills, Pg. 17	
There is no reference in this section of any transformer / electrical substation needed and how secondary spill containment will be provided. This should be addressed and explained by the proponent in the Final Environmental Review Report.	Section 4.4 has been revised to include description of the secondary spill containment for the transformers
Sections 5.4 & 22.4 Impact on Hazardous, Unstable or Contaminate	
<u>Lands, Pg. 21 &amp;71:</u>	MOE's June 1991 Waste Disposal Site Inventory for all sites listed in
Staff of this ministry reviewed the list of active and former waste dispossites presented in the MOE's June 1991 Waste Disposal Site Inventory	Lambton County (now known as St.
(refer to attachment). There are waste disposal sites listed in MOE's Jun 1991 Waste Disposal Site Inventory situated nearby to both the proposed	<u> </u>
East and West Sites. Generally speaking, MOE considers the most significant contaminant discharges to be normally within 500 meters of	sites of significance to the project: The ash and sludge disposal site still
the perimeter of a fill area. Depending upon the soil type, the presence of underground utilities, pipelines etc. are all factors that could conceivably act as a conduit for the migration of methane gas and leachate from thes	of operated by OPG at their Lambton Generating Station (# A31802)
waste sites.	West site, and an aluminum catalyst

The proponent should, prior to finalizing the Environmental Review Report, review the waste sites listed in the MOE June 1991 Waste Site Inventory, and make a determination as to the potential impact, if any, on the two proposed sites, and the need, if any, for any methane gas and/or leachate studies, as well as the applicability of Section 46 of the Environmental Protection Act for the subject properties. It should be noted that the aforementioned June 1991 waste disposal site listings have not been updated since the early 1990's. If the Owner and/or the Municipality are aware of any other waste disposal sites on or within 500 meters of the properties the subject of these two proposed development sites, the proponent should make a determination on potential impacts, if any, the potential need, if any, for any methane gas and/or leachate studies, as well as the applicability or not of Section 46 of the Environmental Protection Act for such sites on the subject properties as well.

Section 46 of the Environmental Protection Act states that:

No use shall be made of land or land covered by water which has been used for the disposal of waste within a period of twenty-five years from the year in which such land ceased to be so used unless the approval of the Minister for the proposed use has been given.

With respect to environmental site suitability, MOE noted in its review of this proposal, that an independent environmental site assessment ESA Phase I study/report is reportedly underway for completion by LVM in late Sept, 2012. This ESAI will reportedly be completed in accordance with CSA 768/01 of Ontario Regulation 153/04 under the Environmental Protection Act. The findings of this assessment, and any recommendations contained therein, should be presented in the Final

disposal site (# A 31803) once operated by Du Pont Canada (closed in September 1980) that is about 400m west of the East Site. Neither waste disposal site poses any significant impact on the site since these sites do not contain any organic matter that could produce methane gas. The proponent has commissioned an ESA Phase 1 Study as per CSA 768/01 for both the East site and the West site found the potential for leachate from these sites impacting the project to be not material

Neither the East site or the West site has been utilized for waste disposal in the last 25 years.

Environme	ental Review Report.	
Air:		
the Green	s some inconsistency in this report on the nominal capacity of Electron Project, with the nominal capacity stated as being MW or 330 MW.	Sections 17.2 and 34.2 have been updated to the correct nominal capacity of about 300 MW
Power Fac	3.1 Simplified Process Flowsheet Diagram of Green Electron cility: This figure is not legible and could be replaced by a Chapters 17.2 and 34.2.	Figure 3.1 and Figure 3 in Sections 17.2 and 32.4 have been updated for better resolution .
Coal: The reported in and 34.2. do not agral a) NO <sub>2</sub> : 8 Chaptersth b) SO <sub>2</sub> : 20 Chapters c) CO <sub>2</sub> : 2 CO <sub>2</sub> : 3 CO <sub>2</sub> : 3 CO <sub>2</sub> : 4 CO <sub>2</sub> : 5 CO <sub>2</sub> : 5 CO <sub>2</sub> : 5 CO <sub>2</sub> : 5 CO <sub>2</sub> : 6	4 tonnes in the ESSR and 94.9 tonnes in Table 10 in the 0 tonnes in the ESSR and 0.90 tonnes in Table 20 in the 31 kilotonnes in the ESSR and 336 kilotonnes (339 kilotonnes ent) in 8 in the Chapters	Table 6.3 has been updated to reflect the correct annual emissions and these are now consistent with the annual emissions in Chapters 17.2 and 34.2
	gh details of emissions calculations and dispersion calculations presented, it was noted that the maximum ground level	The maximum ground level

concentrations of oxides of nitrogen, the most significant air contaminant of gas power generation, were only 6.2% and 2.9% of Ministry 1-hour limit and 24 hour limit respectively	concentration of oxides of nitrogen as presented in Table 6.1 are correct. The sample emission calculations can be found in Appendix B of Sections 17.2 and 34.2
Section 6.5 Pg. 25 & Section 23.5 Pg. 75, Noise Impacts:	
Noise Limits: The reported noise limit for the West Site is 40 dBA. The noise limits reported in the Noise Feasibility Study Report for the West Site are 40 dBA for the east residence and 45 dBA for the west residences. The noise limits should be based on the Noise Feasibility Study Reports.	Sections 6.5 and 23.5 have been updated to reflect the correct noise limit of 45 dBA for the West Site
Noise Control Measures: The recommended noise control measures for the East and West Sites are not the same as the corresponding noise control measures recommended in the Noise Feasibility Study Reports. The recommended noise control measures should be based on the Noise Feasibility Study Reports.	These sections have been updated based on the Noise Feasibility Study Reports
Section 8.3, Wetlands, Pg. 28:	
	Subsequent to the draft dated Sept 15, 2012 the proponent has decided to no longer pursue discharge of process blow down water to Government Drain No. 10 and thus the discharge of blowdown will not
	affect the Bickford Oak Woods
There is mention of possible in water work for replacement of culverts	Complex.
including use of coffer dams. If the proponent takes more than 50,000	
litres a day during construction of the culverts a Permit to Take Water	Comment noted and proponent will

(PTTW) is necessary from this ministry.	apply for a PTTW if necessary.
Should process water not come from a municipal source, Eastern Power is reportedly exploring the possibility of utilizing water from CF-Terra Industries. An amendment to CF-Terra Industries existing PTTW may be required, or Easter Power may need to obtain its own PTTW.	Comment noted and proponent will apply for a PTTW or amendment to CF Industries' existing PTTW if this water source is utilized for the project.
Appendix 17.2 & Appendix 34.2 Air Quality Impact Study Green Electroject (East Site) & (West Site), Township of St. Clair, Ontario, Date	
Because of the high degree of similarity between these two draft air quality impact study appendices, the following comments apply to both Appendix 17.2 and 34.2:	y
1. In these appendices, the project is sometimes referred to as the "Greenfield South Power Project", instead of the newer name of "Green Electron Project".	The project name has been corrected where necessary.
2. The appendices meet most, but not all, of the requirements for the Emission Summary and Dispersion Modelling (ESDM) report as stipulated in section 26 of <i>Ontario Regulation</i> 419/05 – Local Air Quality (O.Reg. 419/05). Before submitting this report in support of an Environmental Compliance Approval (ECA) application, the missing information will need to be added. The following comments contain details on the additional information that is required.	The proponent will ensure that all of the requirements of an ESDM are met for the ECA application.
Additional guidance on preparing an ESDM report is given in the MOE document <i>Guideline A-10: Procedure for Preparing an Emission Summary and Dispersion Modelling (ESDM) Report</i> ( <a href="http://www.ene.gov.on.ca/stdprodconsume/groups/lr/@ene/@resources/documents/resource/std01_079006.pdf">http://www.ene.gov.on.ca/stdprodconsume/groups/lr/@ene/@resources/documents/resource/std01_079006.pdf</a> ).	

3. Section 1.1 Project Description:	
a. Although Figure 2 (Site Plan) is said to show the location of the emission stack, the stack is not clearly identified on the plan.	Figure 2 has been revised to include the stack locations
<ul> <li>b. According to section 26(1)(9) of <i>O.Reg. 419/05</i>, the site plan will also need to include</li> <li>"i. the property boundary,"</li> <li>"ii. the co-ordinates for sufficient points on the property boundary to accurately describe the boundary,"</li> <li>"iii. each source of contaminant identified … "</li> <li>"iv. the location, dimensions and elevation of every structure on</li> </ul>	The proponent will ensure that the ESDM report, in support for an ECA application, will include the required information in accordance with section 26(1)(9) of O.Reg. 419/05
the property"  c. No information is provided to support the stated electrical generation efficiency of 48%.	Further information to support the generation efficiency of 48% has been added.
4. <u>Section 2.1 Existing Climate Conditions:</u> Reference is made to a Figure 10 which consists of a wind rose for the area but this figure is missing	Figure 9 (revised from Figure 10) has been included.
5. Section 2.2 Existing Air Quality and Table 2 Summary of MOE Ambient Air Quality in Sarnia:  a) The text states that the 90 <sup>th</sup> percentiles shown are based on 3 MOE air sampling stations, but a reference was also made to the SLEA air sampling stations. It is not clear from which three stations the data were obtained since the MOE only had one monitoring station in the Sarnia area for the time period of the data (2006 to 2010). The specific SLEA monitoring stations and the specific parameters obtained from these stations needs to be provided.	The text has been modified to include only the MOE Sarnia monitoring station and the SLEA monitoring station in River Bend, Corruna. This data is now presented in Tables 2 and 2a, respectively. For the SLEA data the 90th percentile were calculated based on the data received.

b) While the averaging period for the maximum concentrations is provided in Table 2, the averaging period for the 90 <sup>th</sup> percentiles was not clearly stated.	Table 2 has been updated to indicate the averaging period of 1 hr for the 90th percentile emissions
c) For nitrogen dioxide and sulphur dioxide, the 1-hour maximum is also relevant since criteria are available for this averaging period but was not included in Table 2.	Table 2 has been updated to include the 1-hour nitrogen dioxide and sulphur dioxide criteria
6. Section 4 Operating Scenarios:	
a) The text refers to a "Table xx" which summarizes the emission rates. However, this table was not included in this section.	The text has been updated to include Table 9, which summarizes the various start-up emission rates
b) Although the sources of the emission rates are given as either the manufacturer or the US EPA document AP-42, no supporting information is provided for the calculation of the various emission rates for the different operating scenarios. At a minimum, the original emission rate or factor provided by the manufacturer or the US EPA AP-42 document is required along with sample calculations. (See clause 26(1)(7) of <i>O.Reg.</i> 419/05.) This information could be included in an Appendix to the appendicie.	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with section 26(1)(7) of O.Reg. 419/05
7. Section 5 Greenhouse Gases: a) The emission rates used to calculate the greenhouse gas emissions and a sample calculation are required, preferably in an Appendix to the appendicie.	The text has been updated to include a sample calculation of the greenhouse gas emissions, which can be found in Appendix B to the respective appendices.
b) For the information of the proponent, this facility meets the federal	

facility will need to report its emi Environment Canada's Greenhou		The proponent will ensure that once the facility is in operation, the proponent will report the facility's greenhouse gases to Environment Canada's Greenhouse Gas Reporting Program
8. Section 6 Emission Limits for C	Gas Turbines:	
entitled "Guideline A-5, Atmospl	94" and "Ontario Regulation 419/05, Air	
Carbon monoxide and sulphur did Though details of emissions calcunot presented, it was noted that the	the emission limits of oxides of nitrogen, oxide required by Guideline A-5. In allations and dispersion calculations were see ground level concentrations of the compliance with the Regulation 419/05	The text has been updated to include the sample calculations for the emission rates and dispersion calculations. This can now be found in Appendix B to the respective appendices.
A-5 applied at all times (i.e. inclu 2010 Standards Branch & Approx	as of the position that the limits within des start-up and shut down). On June 8, vals Branch modified A-5 so that it only en applied to natural gas power plants	The proponent acknowledges the modified A-5 treatment for natural gas power plants.
		The "power output" and "heat input" have been included in the respective Appendix B to each appendix

c) The concentration of contaminants in the exhaust gas (i.e., $NO_x - 10.1$ ppm, $CO - 8.4$ ppm and $SO_2 - 0.086$ ppm) are provided for comparison to the calculated limits, but no information is provided in support of these concentrations.	Formula "C" has been re-formatted in Chapter 17.2  The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05
9. Section 7 Proposed Emissions Monitoring System:  This section notes that the facility "will require an emissions monitoring program that may include predictive/parametric emissions monitoring, continuous emissions monitoring, stack sampling, fuel analysis and/or comparison to published emission factors." A more definitive statement on what will be included in the monitoring program is preferable.	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05. However, the selection of an emissions monitoring program will depend on the specific approach of compliance with Guideline A-5 and O.Reg. 397/01.
10. Section 8.2 Methodology:  a) The air dispersion model (Aermod) was the appropriate model for this modelling exercise and the receptor grid and specific receptors chosen were appropriate.	The proponent acknowledges the MOE's concurrence with the appropriateness of the use of the AERMOD model, receptor grid, and chosen receptors.
b) While the text states that the London regional meteorological data set was used in the assessment, it is not clear which of the four available data sets was actually used. Three of the data sets have been pre-processed	The London regional meteorological data set for "crops" was used for the

assuming the surrounding land-use fits entirely into a specific category, namely "crops", "forest" and "urban" land-use. The fourth data set consists of unprocessed hourly surface and upper air data which would allow a modeller to specify the land use by sector around a facility when the meteorological data files are further processed. The meteorological data set that was used needs to be clarified.

assessment. The text has been updated to clearly state which data set was used for the assessment.

c) It does not appear that the surrounding terrain was incorporated into the modelling. This modelling decision may be appropriate, but this decision and the basis for the decision should be clearly stated in this appendicie.

The surrounding terrain was incorporated in the modelling. The text has been updated to list the appropriate terrain data.

d) While the text states that BPIP, the building downwash pre-processor, was used in the assessment, details of the BPIP analysis (*e.g.*, building heights, input and output files, scaled site map with location and heights of all buildings) were not included in this appendicie.

The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05

## 11. Section 8.4 Plume Visibility:

Similar facilities sometimes release a yellow plume during start up. Staff of this ministry's Sarnia District Office has reviewed data regarding these plumes and it seems to be due to elevated SOX & NOX that occur during start-up when the equipment is not operating at optimal efficiency. In the past, this yellow plume has been present and the site was still in compliance with the applicable limits. MOE requests that Company review and revise Section 8.4 as applicable.

Section 8.4 has been revised as appropriate. Final ESRR will indicate that at start up a yellow plume may be visible but startup emissions are included in the air mission assessments with the worst case emissions of startup followed by full load provided in the report

12. Section 9 Dispersion Modelling Results:	
Clause 26(1)(12) of <i>O.Reg.</i> 419/05 requires that an electronic copy of the input files used and the output files produced by the air dispersion model be included with the ESDM report. Since these files were not provided, a complete review of the air dispersion modelling could not be undertaken.	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05.
<ul> <li>13. Section 9.1 Summary of Emissions:</li> <li>a) As noted earlier in comment 6b, the emission factors used to develop the emission rates for the different scenarios as summarized in Tables 7 to 9 are needed as well as sample calculations.</li> </ul>	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05
b) Table 6 appears to be the equivalent of the "Source Summary Table" required by clause 26(1)(8) of <i>O.Reg. 419/05</i> . Some required parameters are missing from this table, however, namely, the averaging period for the emission rates and the volumetric flow rate for discharges ( <i>i.e.</i> , mass flow rate was provided instead).	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05
c) The data quality provided in Tables 6 to 8 is based on a scale from "A" to "E". For the purposes of <i>O.Reg. 419/05</i> , however, data quality needs to be classified as "Highest", "Above Average", "Average" or "Marginal/Uncertain". (See the Chapter 8 of the MOE document <i>Guideline A-10: Procedure for Preparing an Emission Summary and Dispersion Modelling (ESDM) Report</i> for more details on this classification method.) Although the data quality for the manufacturer's data is classified as "Average", without supporting information from the manufacturer, the data quality can only be classified as	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05

"Marginal/Uncertain".	
Treporting intesponds for some of the criteria air contaminants (1 0	The proponent will report its emission to the NPRI as required.
summary tables 11 and 12 also need to be included in the Executive Summary for this appendicie.	The proponent will ensure that the ESDM report, in support of an ECA application, will include the required information in accordance with Guideline A-10 and O.Reg. 419/05
TISOMETHS ARE SAID TO BE SHOWN IN FIGURES X INTOHOU X AND THE HIGHEST T	The corresponding isopleths have been included
17. Appendix A of Appendices 17.2 and 34.2, Cooling Tower Icing Study	Comment noted.

Though details of dispersion calculations were not presented, it was noted that the icing potential was almost negligible.	
<u>Air Summary</u>	
While the air dispersion modelling shows that the air quality criteria would be met, there was insufficient information in Appendices 17.2 and 34.2 to be able to fully assess either the emission rates or the air dispersion modelling. This ministry can therefore not confirm the conclusions from the modelling study.	Sample calculations, manufacturer's guaranteed emission rates, AERMOD input files have been includes in the Appendix B of the respective appendices.
When an application for an Environmental Compliance Approval is to be submitted for approval, the application should be prepared in accordance with the Ministry document entitled "Procedure for Preparing an Emission Summary and Dispersion Modelling Report, Version 2", providing details of emissions calculations and dispersion calculations as a minimum.	The proponent acknowledges the application requirements of the an ECA and will comply with the MOE document, "Procedure for Preparing an Emission Summary and Dispersion Modelling Report, Version 2",
Information on cumulative environmental impact assessment and consultation including public consultation, agency consultation, and consultation with First Nations and Other Aboriginal Communities should be updated and included in the application.	The proponent acknowledges these requirements for the ECA application for this facility.
Appendix 17.3 Draft Noise Feasibility Study Proposed Green Electron  East Site Power Project, Courtright, Ontario Dated September 14, 2012	,
Administrative Noise Control Measures: the operational restraints pertaining to the Gas Compressors, Cooling Tower and Set-Up	

Transformers should be included as administrative noise control measures in section 6.1 of the report.	
Acoustic Barriers: figures (to scale) should be provided to show the locations, lengths and heights of the recommended sound barriers for the Cooling Tower, Set-Up Transformers, and Ventilation Fans (Exhaust Openings).	label for the acoustic barriers around
Vacant Lots: the adjacent lands to the east and west are zoned Agricultural 'A1', where future residences may be located. Therefore, these lands should be included in the noise analysis as vacant lots.	
Zoning Map: the location of the site is not shown on the zoning map. The zoning map should show the location of the site and the surrounding land uses within 1,000 metres from the site in all cardinal directions.	

Sound Level Calculations: one full set of sound level calculations (Cadna-A output tables with 1/1 Octave Band Centre Frequencies) at the worst case (i.e. nearest and most exposed) point of reception should be included in the report.  Appendix 17.4 Draft Green Electron Power Project Township Of St. Clair, Lambton County, Ontario Natural Resources Baseline Report And Environmental Impact Study East Site, Dated September 2012	
Section 2.3, Aquatic Ecosystem, Pgs 13 to 15:	
The Government Drain #10 is classified as a Class C municipal drain, however sections of the report indicate that the drain was dry at the time of site visit. This may indicate the drain requires reclassification to an F. There is also the potential that the drain may provide spawning habitat for Northern Pike which should be further assessed. The results of this assessment may alter the classification as well.	This classification is provided by others including the SCRCA and the proponent is not responsible for any re-classification; while there was no observable flow at a site visit in July 2012, there was water in the system and it was therefore not dry.
There is no indication of total suspended solids in the Government Drain #10. This should be further explored before conclusions are drawn on surface water impacts due to the potential discharge containing elevated solids.	The option for potential discharge to Government Drain #10 is no longer being considered fot his project.
Appendix 17.5 Draft Conceptual Stormwater Management Plan Gree Power Project Township of St. Clair, Lambton County, Ontario, Date	
Section 2 Existing Conditions, Pg. 2-1:	
A very brief reference is made to "an ash disposal site" as being located to the north-east of the West Site. Please provide further details / elaboration on the nature of this "ash disposal site" in the Final	Further details on the ash disposal site to the north and west of the site have been included. No material

Environmental Review Report, the distance separation between it and the subject property; and what impact, if any, it will have on the Green Electron Energy Project	impact on the project is expected.
Section 3 Design Criteria, Pg. 3-1:	
Clarification is required regarding the anticipated amount of stormwater discharge and also an explanation why quality control would not be necessary. If there is any anticipated discharge during overflow situations, quality and quantity control would be necessary and included in an Environmental Compliance Approval application for this project. The proposed plan notes the use of the cooling tower basin as acting as a SWM Pond to provide quality and quantity controls to pre-development levels. Noting that this is a conceptual plan, details of the cooling tower basin are necessary including spillway, expected pond performance, spillway, outlet structure and elevation of the freeboard. For the SWM Plan detail design, it is recommended that the proponent confirm that the cooling tower basin will comply with the design parameters of this ministry's Stormwater Design Manual.	Any stormwater collected in the cooling tower basin will be used in the evaporative cooling process and thus there will be no need for a spillway or outlet structure and therefore quality control would not be necessary. The total capacity of the cooling tower basin is about 4440 m³, of which a freeboard of about 4200 m³ will be available to accommodate a 100 yr storm.  The proponent has reviewed the MOE's Stormwater Design Manual and notes that the Manual does not
	apply to the cooling tower basin. Quality control, retention time of 24 hrs, spillway, etc does not apply since all stormwater collected will be used in the evaporative cooling process.
Section 5 Proposed Cooling Tower Basin, Pg. 5-1 to 5-2:	p-00000
If there is to be any stormwater discharge there should be some form of quality control measures in the form of periodic sampling of the	There will be no discharge of stormwater from the cooling tower
discharge.	basin where it will be used in the

	cooling process.
It appears that stormwater would be mixing with process water. If this mixture is to be discharged to the natural drainage area (i.e. open the sluice gate) this discharge should be considered a wastewater effluent discharge and not a stormwater discharge.	Once the stormwater enters the cooling tower basin it will be treated as process water and any discharge via blowdown, etc. will be in accordance with the ECA and/or sewer use by-law of the municipality as applicable.
If the site is not considered a contaminated site it may be reasonable to address stormwater management only for the developed portion. However, if the site is contaminated or if there are other quality control issues with the site it may be necessary to capture and treat all of the runoff. Please provide clarification supporting the option to only capture and treat the developed portion of the site.	The East site is not contaminated as assessed in a site specific (ESA Phase I investigations) and thus only the stormwater runoff from the developed area will be captured and treated.  There is no history of contamination of the West site or visible evidence as to contamination. Additional assessment are being carried out to ensure that there has been no contaminants entering the West site from neighboring property land uses pertaining to waste treatment.
Appendix 17.6 Draft Stage 1 Archaeological Assessment Green Electron Plan	<u> </u>
Lot 26, Concession 2, Moore Twp, Lambton Co., On, Dated August 8th, 2012	
	The proponent's archaeological
Has the proponent approached staff of the Ministry of Culture and	consultant has submitted the Phase 1
Recreation with respect to archaeological assessment of this proposed	archaeological assessments reports
project? This ministry defers the Province's comments, if any, on	for both the East and the West sites

Appendix 17.6 to staff of the Ministry	of Culture & Recreation.  to the Ministry of Culture and Recreation	d
Appendix 17.7 Green Electron Power F Process Public Consultation Report, Da		
This ministry has no comments to offer Appendix 17.7.	er with respect to the contents of Comment noted.	
Appendix 17.8 Green Electron Power F Process Government Agency Consultat	· ·	
Section 3 Notices and Information Provide	<del>-</del> -	
Reference is made in this Section of A Environmental Review Report to Noti In an e-mail to this ministry dated Oct kindly put together a chart outlining the First Nations.	ces that were sent to First Nations. the First nations has been incober 2 <sup>nd</sup> , 2012, the proponent also the Government and Agencies	les with eluded in es ices er were
September 27 <sup>th</sup> , 2012, with the ex reportedly took place with Walpole August of 2012, based upon the information of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the expression of the september 27 <sup>th</sup> , 2012, with the se	delivery/receipt were obtained	vere fations at ces of
"meaningful" First Nations consultanotice, but also personally following	taff advised the proponent that ition includes not only providing up with First Nations with offers to include any includes not only providing offered to come to meet with Other than Walpole Island Figure 1.	in them.

concerns regarding impacts that the project has on rights or interests, and accepted this offer. One Chief then the proponent, demonstrating in the Final Environmental Review Report, specific details / information on what was discussed with First Nations, what concerns if any were raised, and how those concerns, if indicated that he was unsure if they any, were addressed. Sending notification letters alone to First Nations, without any subsequent personal follow-up and offers to personally meet with First Nations is not in and of itself considered First Nations Consultation.

indicated the prject was not in their traditional territory. One Chief intended to get involved.

Through an e-mail dated September 11<sup>th</sup>, 2012, listings of First Nations communities that need to be consulted with respect to this project were provided to the proponent by this ministry. Neither Draft Appendix 17.8, nor the Chart that accompanied the proponent's e-mail to this ministry dated October 2<sup>nd</sup>, 2012 indicate any acknowledgement letters or phone calls confirming that the First Nations actually received the proponent's notices and offers to meet. Does the proponent have any additional First Nation consultation initiatives planned for the future? Given the timelines and priority of this project, if Eastern Power is having difficulty obtaining responses from First Nations communities, this can be communicated to the Crown, and the Crown can assist where possible.

The proponent remains open to consultation with First Nations that chose to participate.

Section 5 Summary of Government Agency Comments and Responses, Pgs. 6 & 7:

Comment noted and a correction has been made.

Reference is made to the Ontario Ministry of Environment. The comments presented were not provided by the Ontario Ministry of Environment (Provincial), but rather, they appear to have been provided by Environment Canada (Federal). Please correct this error in the Appendix that accompanies the Final Environmental Review Report.

Appendix 34.3 Draft Noise Feasibility Study Proposed Green Electron West Site Power Project, Courtright, Ontario Dated September 14 <sup>th</sup> , 2	
Administrative Noise Control Measures: the operational restraints pertaining to the Gas Compressors, Cooling Tower and Set-Up Transformers should be included as administrative noise control measures in section 6.1 of the report.	This will be included in the Acoustic Assessment Report.
	Measurements and observations indicate that the receptors along St. Clair Parkway are in an urban acoustical environment. Sound from both the existing OPG site and a facility in the US are significant during all hours. Road traffic is dominant during daytime hours.
Zoning Map: the location of the site is not shown on the zoning map. The zoning map should show the location of the site and the surrounding land uses within 1,000 metres from the site in all cardinal directions.	The project location will be noted.
Sound Level Calculations: one full set of sound level calculations (Cadna-A output tables with 1/1 Octave Band Centre Frequencies) at the worst case (i.e. nearest and most exposed) point of reception should be included in the report.	Will be included in the final report.
Appendix 34.4 Draft Green Electron Power Project Township Of St. Clair, Lambton County, Ontario Natural Resources Baseline Repo And Environmental Impact Study West Site, Dated September 2012	ort
Figure 2-2 West Site Aquatics Assessment Summary Map, Pg. 24:  It appears that Bowens Creek was only assessed upstream of the project. Downstream assessment will be necessary to determine potential affects	The proponent no longer intends to discharge process waste water into Bowens Creek.

on surface water features.			
	Appendix 34.6 Draft Stage 1 Archaeological Assessment Green Electron Plant Lot 13, Concession 2, Moore Twp, Lambton Co., On, Dated August 2012		
		The proponent's archaeological consultant has submitted the Stage 1 archaeological assessments reports for both the East and the West sites to the Ministry of Culture and Recreation.	
Other General Comments:			
Project to the USA/Canada border could conceivably cross the USA proponent needs to notify Environ this proposed facility since the since the since the since the since the since the contact person from boundary emissions was Ms. And Division, Environmental Protection Ontario Region, Phone (416) 739 understanding that the information Environment Canada is document the USA.  2) The Great Lakes Charter since the USA.	speaks to the principle of prior notice and		
consultation to bordering States a	and Provinces of any new or increased the water resources of the Great Lakes	negligible impact on air quality in the USA, and if the contribution of	

	the Great Lakes Charter. This has been included in the final revision of the Environmental Screening and Review Report for the Project.
sponse received; General information provided to consultants ring as to SAR in region of sites during preparation of reprts in indices 17.4 and 34.4	SAR were not found during field studies of site and provisions have been made in Appendices 17.4 and 34.4 should SAR be found later during project phases.
he East Site:  ority staff have reviewed the submitted topographic survey and site and the following response is based on discussion between staff of CRCA (Girish Sankar, Water Resources Engineer - Dallas Cundick, ations Officer - and Michelle Fletcher, Natural Heritage and	GSPC is in the process of establishing and refining the Regional Floodline through consulting engineers that have experience with floodline mapping in St. Clair Township. GSPC will be seeking the referenced permission
h a	ing as to SAR in region of sites during preparation of reprts in dices 17.4 and 34.4  e East Site:  rity staff have reviewed the submitted topographic survey and site nd the following response is based on discussion between staff of RCA (Girish Sankar, Water Resources Engineer - Dallas Cundick,

for the East site. This is not The subject property is traversed by Government Drain No. 10 and its applicable to the West site. associated floodplain. The regulated area of the Authority includes those areas susceptible to flooding and erosion, as well as the Provincially Significant Wetlands, plus all lands within 120 metres of the wetland boundary. The area regulated by the Authority is depicted on the attached map. For the East Site: Based on current hazard mapping, on-site investigation completed We are in the process of establishing August 21, 2012, and review of the attached topographic survey, the the regional flood line and will be Authority can confirm that the majority of the subject property is seeking the referenced permission identified as being susceptible to flooding during a regional storm for the East site. This is not flooding event. The property, and specifically the proposed location of applicable to the West site. the Eastern Energy Power Project as depicted on the attached site plan, is therefore, impacted by the hazards land regulation of the Authority, GSPC is in the process of implemented pursuant to Section 28 of the Conservation Authorities Act. establishing and refining the The regulation is entitled "Development, Interference with Wetlands and Regional Floodline through Alterations to Shorelines and Watercourses" (O.R. 171/06). This means consulting engineers that have experience with floodline mapping in that the proponent must obtain permission from the Authority prior to the commencement of a development activity on the subject property. St. Clair Township. GSPC will be Development activities include: construction, reconstruction or seeking the referenced permission placement of a structure; placement or removal of fill; re-grading, or for the East site. This is not altering a watercourse. applicable to the West site.

	In your email you inquired about proposed ground floor elevations being established for the proposed development. The ability to establish ground floor elevation requirements for the proposed development on the property is premature from a floodplain hazard perspective. For this area the Authority has received estimated engineered floodline mapping derived from coarse 1:10,000 OBM mapping obtained in the 1980's. The floodplain analysis depicts the entire property as being floodprone under Regional storm conditions. The regional storm flooding event is equivalent to flooding that would be expected during a Hurricane Hazel storm event. The greatest hazard limit on the subject property is the Regional floodline. A detailed Regional/1:100 year floodline mapping study is necessary to establish a building envelope outside the Regional flood level. The Regional flood level is the regulatory standard at this location. Any building envelope must be situated outside the erosion hazard as well. A list of engineering firms that can carry out these works is attached. Any engineering questions should be directed to Girish Sankar at Ext. 247 gsankar@scrca.on.ca.	We are in the process of establishing the regional Floodline and will be seeking the referenced permission for the East site. This is not applicable to the West site.  GSPC is in the process of establishing and refining the Regional Floodline through consulting engineers that have experience with floodline mapping in St. Clair Township. GSPC will be seeking the referenced permission for the East site. This is not applicable to the West site.
Canadian Environmental Assessment Agency		Letter received Sept 17, 2012 as to new CEAA 2012 notification rules; in consultation with CEAA as to satisfying any additional requirements beyond MOE EAAB requirements
Aboriginal Affairs and Northern Development September 4, 2012	Thank you for your notice of the Green Electron Power Project Environmental Review. Our department does not have any concerns or comments at this time. For future notifications please direct them to <a href="EACoordination_ON@aandc.gc.ca">EACoordination_ON@aandc.gc.ca</a> .	No response was required for this email.
September 4, 2012	Thank you.	

	Received the following advice regarding the movement of wood in a regulated	The Project is not expected to involve
Inspection Agency	Emerald Ash Borer (EAB) zone:	cutting of any Ash materials (as defined
August 21, 2012		in the CFIA regulations). In the event
	an EAB perspective would be that any Ash materials moved from the site stay within the current regulated zone for EAB, which can be found online at:  -Natalie Avoledo	that any cutting of Ash materials is required for the project, the regulations restricting the movement of Ash materials to within the EAB Zone will be complied with.