



NATURAL GAS DEMAND SIDE MANAGEMENT TECHNICAL RESOURCE MANUAL

Version 2.0

Date: December 22, 2017

ONTARIO NATURAL GAS DEMAND SIDE MANAGEMENT TECHNICAL RESOURCE MANUAL

Introduction

This TRM is a document that provides essential information and source materials underpinning prescribed energy savings assumptions and/or calculations for a number of energy efficient technologies that are or may be in the future promoted by the Ontario gas utilities' energy efficiency programs.

The efficiency measures addressed by the TRM are prescriptive and quasi-prescriptive measures that lend themselves to standardized assumptions and algorithms, and for which estimated average savings can be determined to be reasonably accurate.

The assumptions and algorithms represent accepted engineering practice and have been substantiated with third party sources and data specific to Ontario and/or geographic areas with similar climates, to the extent possible and when applicable.

Natural gas savings are reported in gross cubic meters (m³) of natural gas. Additional impacts of electric and water savings have been included where applicable. Measure life and incremental cost have also been provided. The measures are organized by market, measure category, and end-use.

This TRM includes measures that have been considered by the utilities, or might be considered in the future. It should be noted that the TRM is a technical reference document and as such inclusion in the TRM does not imply that it is appropriate to include a measure in the utilities' portfolio in a given program year.

Version History

The TRM is a dynamic document that will be periodically updated with new information supported by substantiated references. The TRM Version Date and Revision History table presented below briefly summarizes the history of the evolution of the introductory sections of the TRM. Similar tables summarize the development of assumptions for each individual measure in the technical sections of the TRM.

Date	Version	Reasons for Update
December 21, 2016	1.0	Original developed by Energy and Resource Solutions (ERS) and filed with the OEB. The TRM was commissioned by the Technical Evaluation Committee (TEC) ¹ , and was managed by a sub-committee of the TEC.
December 22, 2017	2.0	Update by the OEB's Evaluation Contractor (DNV GL and Dunsky) with input from the Evaluation Advisory Committee (EAC) ² ; the following measures were updated or added: <ul style="list-style-type: none"> • Commercial Incremental Energy Recover Ventilator (ERV), 55% Efficiency Baseline • Commercial Incremental ERV, No ERV Baseline • Commercial Incremental Heat Recovery Ventilation (HRV), 55% Efficiency Baseline • Commercial Incremental HRV, No HRV Baseline • Commercial Pedestrian Air Curtains with Vestibule

Purpose of the TRM

The objectives of the TRM are as follows:

- ❑ Provide transparent, standardized (where applicable), and substantiated assumptions and/or calculation algorithms for efficiency measure savings, costs and lifetimes, as well as their underlying sources.
- ❑ For each measure, establish the conditions under which the savings or other assumptions apply.
- ❑ Provide a basis from which stakeholders, such as utility/program administrators and independent third parties, can estimate the savings achieved for the Ontario energy efficiency portfolios.
- ❑ Support cost-effectiveness calculations for projects undertaken and funded by the utility efficiency programs.³
- ❑ Provide access to a chronology of the changes over time to measure assumptions – including the rationale used to support changes.

¹ The TEC consisted of utility representatives from each of Union Gas and Enbridge Gas Distribution as well as intervenor representatives and independent members with technical expertise. In its role to establish DSM technical and evaluation standards for natural gas utilities in Ontario, the TEC commissioned the development of the original TRM.

² The OEB outlined a structure to evaluate the results of Natural Gas Demand Side Management (DSM) programs from 2015 to 2020. The EAC will provide input and advice to the OEB on the evaluation and audit of DSM results. The committee will consist of representatives from non-utility stakeholders, independent experts, staff from the Independent Electricity System Operator (IESO), and observers from the Environmental Commissioner of Ontario and the Ministry of Energy, all working with OEB staff.

³ The TRM includes several, but not all of the key inputs to be used in such calculations. Specifically, annual savings (gas, electric and water), incremental costs and measure lives are included, but net-to-gross ratios, non-measure (program) costs and avoided costs are not included.

The purpose of the TRM does not include:

- Determination of free ridership or spillover values as they are more a function of program design than they are of technology specific factors.
- Recommendation of potential energy efficiency measures to utilities.
- Recommendation of program design structures or features.
- Methodologies for determining the potential savings for custom measures.

Measure Outline

Each measure follows a consistent format that includes the following components.

Version Date and Revision History

This section tracks the history of the measure development, including when the measure documentation was filed and approved by the OEB as well as classification for its application (see table below).

Version Date and Revision History	
Version	
OEB Filing Date	
OEB Approval Date	
Sector → End Use → Technology → Measure Category	

Sector

“Sector” refers to the market categories (Residential, Multi-Residential, Commercial⁴) for which the measure substantiation document applies.

- **Commercial:** A location providing goods and services such as businesses or institutions, e.g. retail, hospitals, universities, etc. Industrial facilities are also included in this category, however, industrial process improvements are typically custom measures and not addressed by the TRM.
- **Multi-residential:** According to Ontario Regulation 282/98, the multi-residential property class is property used for residential purposes that has seven or more self-contained units,⁵
- **Residential:** According to Ontario Regulation 282/98, the residential property class is property used for residential purposes that has less than seven self-contained units.⁶ Typically this includes single detached, semi-detached, row house and/or duplex.

⁴ All Commercial sub docs apply to the Industrial market unless otherwise noted.

⁵ <https://www.ontario.ca/laws/regulation/980282#BK4>

⁶ Ibid

Though Low-Income is a market type and not a market sector, it is appropriate to provide a definition for clarity as all substantiation documents apply to the Low-Income market unless otherwise noted.

Low-Income: Low income residential utility customers face a much higher ‘energy burden’ (i.e. percent of household income devoted to energy costs) than median and higher income households. The OEB Guidelines (EB-2014-0134) provide additional detail around eligibility criteria for low-income utility customers in Section 6.4 on page 11.

End Use

“End Use” refers to service provided by the equipment (e.g. space heating, water heating, or food service).

Technology

“Technology” refers to the type of equipment (e.g. Adaptive Thermostat).

Measure Category

“Measure category” refers to the general decision types outlined in the OEB Filing Guidelines to the Demand Side Management Framework for Natural Gas Distributors (2015-2020). These decision types characterize how savings and costs are estimated relative to a frame of reference or “base case” that specifies what would have happened in the absence of the utility program. The decision types are defined as follows:

- **Early Replacement** – a measure category where a utility energy efficiency program has caused a customer to replace operable equipment with a higher efficiency alternative (also referred to as advancement).⁷

Example: An operating unit heater is replaced with a more efficient radiant heater.

- **Natural Replacement** –

a measure category where the equipment is replaced on failure or where a utility energy efficiency program has not influenced the customer decision to replace but once the decision has been made, the utility program influences a higher efficiency alternative.

Example – An operational gas water heater is replaced because of visible rust, and a more efficient water heater, promoted by the program, is installed.

- **New Construction** – efficiency measures in new construction or major renovations, whose baseline would be the relevant code or standard market practice.

⁷ Some customers replace equipment when their existing equipment fails. For a variety of reasons (e.g. concern about energy or maintenance costs, better integration with other building systems, a desire to be able to plan for downtime rather than react to an emergency, etc.), other customers replace equipment before it fails. The key to an “early replacement” designation is that the utility program caused something to be replaced before it otherwise would have been.

Example – A project design team, influenced by the program, specifies a high efficiency boiler rather than the least cost code compliant, or predominant industry practice, option.

• **Retrofit** – a measure category that includes the addition of an efficiency measure to an existing facility such as insulation or air sealing to control air leakage.

Example – An ozone treatment system is added to an existing commercial laundry system in order to facilitate using lower water temperatures.

Note - A single substantiation document may be applicable to multiple categories, and will be identified as such.

Substantiation Document Summary Table

Each substantiation document includes a summary table (see Table 1) outlining critical prescribed savings values or quasi-prescriptive savings factors, key measure parameters, incremental cost, measure life, and applicability factors.

Table 1. Measure Key Data

Parameter	Definition
Measure Category	Retrofit, early replacement, new construction, or time of natural replacement. These terms are defined in the Measure Categorization section.
Baseline Technology	The existing condition, code compliant, or standard practice measure depending upon the measure category.
Efficient Technology	The installed high efficiency measure as described in the substantiation document
Market Type	Commercial, Residential, Multi-Residential
Annual Natural Gas Savings	Expressed in cubic meters for prescriptive measures. Expressed as a savings factor (e.g. m ³ /lb) for quasi-prescriptive measures.
Annual Electric Savings	Expressed in kWh for applicable measures.
Annual Water Savings	Expressed in litres for applicable measures.
Measure Life	The length of time that a measure is expected to be functional and performing as predicted.
Incremental Cost (\$)	The incremental cost is the difference in cost between the high efficiency technology and the baseline technology. The incremental cost includes incremental installation costs where appropriate.
Restrictions	Describes any limitations to the applicability of the measure’s prescribed savings or relationships, such as minimum size or applicable building types.

Overview

This section introduces the technology, describes the energy savings strategy of the measure, and lists other descriptive details.

Application

This section describes market sector or other parameters where the technology in question may be applied. For example, it could address the history of code changes and why the substantiation document savings only apply to homes of a certain vintage or businesses of a certain size. It commonly relates to the restriction section in the summary table.

Baseline Technology

This section provides a definition of the efficiency level of the baseline equipment used to determine energy savings beyond baseline, including any standards or ratings if appropriate. The baseline also may include statements regarding the presumed type of equipment that will be replaced or upgraded. For example, the baseline equipment for commercial infrared heaters is presumed to be a unit heater as opposed to a central system. It may also include statements regarding part-load conditions.⁸

Table 2 for each measure summarizes the baseline technology.

Table 2. Baseline for Energy Conservation Measure

Scenario	Requirement
Type of measure	Baseline Efficiency

Efficient Technology

This section provides a definition of the criteria for the efficient equipment used to determine the delta energy savings including any standards or ratings if appropriate.

Table 3 for each measure summarizes the efficient technology.

Table 3. Efficient Technology for Energy Conservation Measure

Scenario	Requirement
Type of measure or equipment	Minimum level of efficiency

Energy Impacts

⁸ Part-load performance is the ability of the system to handle energy use at conditions lower than the rated capacity of equipment. For example, a boiler may be sized to meet a maximum capacity to meet the load during the coldest day of the year. However, during warmer temperatures, the equipment will operate at some part-load depending on its ability to turn down to a lower firing rate. The operation and efficiency of the boiler will vary depending on the load conditions.

This section identifies the type of energy impacts resulting from implementing the measure (e.g. natural gas savings, electric savings/penalties), and explains how this measure causes the change, in narrative form.

Natural Gas Savings Algorithm

This section presents the algorithm(s) utilized to estimate the natural gas savings for the measure. In some cases the algorithms are used to derive an average natural gas savings for the measures, while for other measures (i.e. quasi-prescriptive) the algorithm(s) represent the derivation of a gas savings factor to be used given certain project assumptions.

Electric and/or Water Savings Algorithm

This section outlines the approach for determining any secondary impacts on other resources, such as electricity and water, and is included as needed.

Assumptions

This section provides a reference table listing key assumptions that impact the measure savings analysis (e.g. hours of operation, equivalent full-load hours, weather criteria, load factors). For some measures, additional assumptions regarding hours of operation or the amount of time equipment or appliances are being used is provided, as applicable. It also provides references for the assumptions used in the measure analysis.

Savings Calculation Example

This section provides an example of a savings calculation. In the case of a quasi-prescriptive measure, application of the associated savings factor is explained.

Uses and Exclusions

This section outlines circumstances where a prescribed savings value is not appropriate.

Measure Life

This section provides the technology's measure life and any qualifying circumstances (e.g. evidence of regular maintenance).

Incremental Cost

This section describes the technology's incremental cost and any additional considerations pertaining to its determination. Incremental cost is dependent on the measure category. The utilities follow the OEB Guidelines' (EB-2014-0134) direction regarding the application of incremental costs as outlined in Section 9.1.1- Net Equipment Costs (pg. 26/27). The incremental cost has been indexed to 2015 and is expressed in Canadian dollars.

References

This TRM aims to provide best available and substantiated information collected at the time of its production. References (many available online) to documents are provided for each key assumption. Examples of references deemed appropriate for this TRM include:

- Efficiency program evaluations conducted both in Ontario and other jurisdictions within Canada and United States;
 - Government studies on the performance and/or cost of efficiency technologies – within Ontario, other parts of Canada, the U.S. or outside North America when applicable;
 - Other published research on the performance and cost of efficiency measures; within Ontario, other parts of Canada, the U.S. or outside North America when applicable;
- Information collected directly from key technology manufacturers and/or other parts of the supply chain for the technology in Ontario (e.g. distributors, contractors, etc.)

Additional TRM Notes

This TRM includes prescribed (prescriptive and quasi-prescriptive) savings estimates that are expected to serve as average, representative values for the province of Ontario. All information is presented on a per-measure basis. In using the measure-specific information in this TRM, it is important to keep the following notes in mind:

- Measure lives serve to represent the Ontario market and include measure persistence unless otherwise noted.
- In general, the baselines included in the TRM are intended to reflect average practices and conditions in Ontario.

Common Assumptions Table

Where assumptions are shared between multiple technologies, they have been gathered in a Common Assumptions table. Among these common assumptions, London, Ontario was selected as a default climate zone, due to its elevation and annual average temperature cycle.

In addition to weather-related assumptions, the common assumptions include efficiencies for different types of equipment, common conversions, local conditions that would impact measures like average water temperature, heat content of natural gas, etc.

Gas Properties/Physics Properties/Energy Conversions				
Input Variable	Assumption	Units	Source / Comments	Affected Subdocs
Energy density of natural gas	35 738	Btu/m ³ mmBtu/m ³ m ³ /mmBtu MJ/m ³	RATE CHANGE #94, EB-2011-0354/EB-2013-0295 The source of the heat content for natural gas is the rate case as approved by the OEB	All Measures
Conversions				
Conversion of Btu/KWh	3.412	Btu/kWh	https://www.extension.iastate.edu/agdm/wholefarm/pdf/c6-96.pdf	All Measures
Conversion of KW/HP	0.7457	kW/HP	https://www.extension.iastate.edu/agdm/wholefarm/pdf/c6-96.pdf	All Measures
Physics Properties				
Acceleration due to gravity	32.2 ft/sec ² (9.8 mps)	ft/sec ²	http://www.engineeringtoolbox.com/acceleration-gravity-d_340.html	Commercial Air Curtains

Fluid Properties				
Property	Assumption	Units	Source / Comments	Affected Subdocs
Specific heat capacity of water	1.00	Btu/lb °F	CSA P.3-04 Standard, Testing Method for Measuring Energy Consumption and Determining Efficiencies of Gas-Fired Storage Water Heaters.	Residential Tankless Water Heater Commercial ENERGY STAR Dishwasher Residential High Efficiency Water Heater
Density of water (@ 100 F)	8.29	lb/gal (US gallons)	http://www.engineeringtoolbox.com/water-specific-volume-weight-d_661.html	Residential Tankless Water Heater Commercial ENERGY STAR Dishwasher Residential High Efficiency Water Heater
Density of exhaust air (@ 72 F, 50% RH)	0.074	lb _m /ft ³	Air density calculated based on space temperature temperature setpoint in the common assumptions below. Exhaust air will be at the space conditions. Based on approach in ASHRAE Systems and Equipment Handbook 2012, Chapter 26	Commercial ERV Commercial HRV

Building Use and Occupancy				
Input Variable	Assumption	Units	Source / Comments	Affected Subdocs
Average single family residential household size	2.9	residents/household	Enbridge, Results of "Residential Market Survey 2013" <a "="" href="http://www12.statcan.ca/census-recensement/2006/dp-pdb/tot/Pp-eng.cfm?LANG=E&APATH=3&DETAIL=0&DIM=0&FL=A&FREE=0&GC=0&GID=837983&GK=0&GRP=1&PID=89071&PRID=0&PTYPE=89971.97154&S=0&SHOWALL=0&SUB=0&Temporal=2006&THEME=69&VID=0&VNAMEF=&VNAMEF=">http://www12.statcan.ca/census-recensement/2006/dp-pdb/tot/Pp-eng.cfm?LANG=E&APATH=3&DETAIL=0&DIM=0&FL=A&FREE=0&GC=0&GID=837983&GK=0&GRP=1&PID=89071&PRID=0&PTYPE=89971.97154&S=0&SHOWALL=0&SUB=0&Temporal=2006&THEME=69&VID=0&VNAMEF=&VNAMEF=" Enbridge, Results of "Residential Market Survey 2013" (Calculated by determining the weighted average between buildings over 5 stories and buildings of five stories or less)	Residential Showersheads (Single and Multiresidential) Residential Faucet Aerators (Kitchen and Bathroom) Residential High Efficiency Water Heater
Average multi-residential household size	1.96	residents/household	Enbridge, Results of "Residential Market Survey 2013" (Calculated by determining the weighted average between buildings over 5 stories and buildings of five stories or less) <a "="" href="http://www12.statcan.ca/census-recensement/2006/dp-pdb/tot/Pp-eng.cfm?LANG=E&APATH=3&DETAIL=0&DIM=0&FL=A&FREE=0&GC=0&GID=837983&GK=0&GRP=1&PID=89071&PRID=0&PTYPE=89971.97154&S=0&SHOWALL=0&SUB=0&Temporal=2006&THEME=69&VID=0&VNAMEF=&VNAMEF=">http://www12.statcan.ca/census-recensement/2006/dp-pdb/tot/Pp-eng.cfm?LANG=E&APATH=3&DETAIL=0&DIM=0&FL=A&FREE=0&GC=0&GID=837983&GK=0&GRP=1&PID=89071&PRID=0&PTYPE=89971.97154&S=0&SHOWALL=0&SUB=0&Temporal=2006&THEME=69&VID=0&VNAMEF=&VNAMEF="	Residential Showersheads (Single and Multiresidential)
Food service days per year	312.0	days	http://www.fishnick.com/equipment/techassessment/Appliance_Tech_Assessment.pdf , (typical operating hours of equipment 6 days per week, 52 weeks per year)	Commercial Cooking Measures (Underfired Broilers, Steamers, Fryers, and Convection Ovens) Commercial ENERGY STAR Dishwasher

Weather/Water Assumptions				
Input Variable	Assumption	Units	Source / Comments	Affected Subdocs
Average city or inlet water temperature	9.39 C (48.9 F)	deg C (deg F)	Average of findings in two studies, adjusted for Toronto water inlet temperature. Mayer, P. W. et al Residential Indoor Water Conservation Study, Evaluation of High Efficiency Indoor Plumbing Fixture Retrofits in Single-Family Homes in East Bay Municipal Utility District Service Area, 2003 and Skeel, T. and Hill, S. Evaluation of Savings from Seattle's "Home Water Saver" Apartment/Condominium Program, 1994. Both cited in: Summit Blue (2008) From Faucet Aerator (Residential Bathroom)	Commercial Pre-Rinse Spray Nozzle Residential Tankless Water Heater Residential Faucet Aerators (Kitchen and Bathroom) Residential High Efficiency Water Heater Commercial Ozone Laundry

Water Heating Assumptions/Setpoints					
Input Variable	Assumption	Units	Source / Comments	Affected Subdocs	
Domestic hot water factory set tank temperature	Commercial (for some facility types)	60 C (140F)	deg C (deg F)	http://www.nrcan.gc.ca/sites/oeenrcan.gc.ca/files/pdf/publications/inforesource/pub/home/Heating_With_Gas.pdf , page 20	Commercial Pre-Rinse Spray Nozzle Commercial ENERGY STAR Dishwasher Residential Tankless Water Heater
	Residential	48.9 C (120F)	deg C (deg F)	EGD contacted manufacturers in 2014 regarding the High Efficiency Water Heating sub-doc hot water temperature factory setting. They state residential storage water heaters are preset at 120 deg F.	Residential Faucet Aerators (Kitchen and Bathroom) Residential High Efficiency Water Heater Residential Faucet Aerators (Kitchen and Bathroom)
Natural gas storage tank water heater	Recovery Efficiency (Residential)	78.68%		Average from all models listed on NRCAN. (2014).	Residential Pipe Wrap
	Thermal Efficiency (Commercial)	83.0%		Average of standard efficiency of units shipped in 2009, Caneta Research Inc., "Report For Baseline Information - TRM Development, page 5," Caneta Research, Inc, Mississauga, Ontario, August 19, 2013	Commercial ENERGY STAR Dishwasher Commercial Ozone Laundry Commercial Pre-Rinse Spray Nozzle

Space Conditioning Assumptions/Setpoints				
Input Variable	Assumption	Units	Source / Comments	Affected Subdocs
Commercial heating system efficiency (Air Systems)	80%	Thermal Efficiency	ASHRAE 90.1-2004, ASHRAE 90.1-2007, ASHRAE 90.1-2010, for units below 225 MBH (Table 6.8.1E)	Commercial Kitchen DCV Commercial DCV Commercial Destratification Fans Commercial Air Curtains Commercial ERV Commercial HRV
Heating System Enabled (F)	12.78 C (55 F)	deg C (deg F)	Based on engineering judgement, professional experience with building design, and discussion from both ASHRAE Handbook 2013 and the Nexant ERV-HRV 2010 report: "Historically, heating degree days were reported on a 65°F basis (HDD65) due to poor insulation and low internal gains in a space... A newer building will have an even lower balance temperature with the current value of 50°F, since it will have improved insulation resulting in less heatloss." (Nexant ERV-HRV 2010 report pg. 6-40) ERS assumed a 55F balance temperature to be representative of all building types.	Commercial DCV
OA temperature heating system enabled	33.03°F (0.6°C)	deg C (deg F)	Average London, ON outside dry bulb temperature when temperature drops below 55F based on TMY3 weather data. Relative to a 55F balance point.	Commercial Air Curtains Commercial ERV Commercial HRV
Heating Hours per year*	5 567	hours	Relative to a 55F balance point. Heating hours per year is the number of hours during the year when a heating system may be enabled due to the outdoor temperature being below the balance point. The balance point is the outdoor temperature at which the heating system will be enabled because the internal gains and the building losses are at equal. Below this temperature, heat must be added to the building to maintain the indoor temperature.	Residential Pipe Wrap Commercial Destratification Fans Commercial HRV Commercial ERV
Heating days per year	232	days	Relative to a 55F balance point	Commercial Air Curtains
Effective full load heating hours commercial New Construction*	1 500	hrs	25%Oversized_Infrared Analysis (Agviro Replicated) - with notes and Toronto March 4 2009 -.xls The full load heating hours is the number of hours during the year for which a heating system must operate at full load under design conditions or the peak capacity, in order for the system to satisfy the annual heating requirements of a new building.	Commercial Condensing Unit Heater Commercial Infrared Heaters
Effective full load heating hours commercial Retrofit*	2 000	hrs	25%Oversized_Infrared Analysis (Agviro Replicated) - with notes and Toronto March 4 2009 -.xls The full load heating hours is the number of hours during the year for which a heating system must operate at full load under design conditions or the peak capacity, in order for the system to satisfy the annual heating requirements of an average existing building.	Commercial Condensing Unit Heater Commercial Infrared Heaters
Rooftop Unit Cooling System Efficiency	13 SEER (3.81 COP - Converted to COP by dividing SEER by 3.412 Btu/W)	Btu/Watt	Ministry of Municipal Affairs and Housing-Building and Development Branch, "Supplemental Standard SB-10 (Energy Efficiency Supplement)," Ministry of Municipal Affairs and Housing, Toronto, 2011	Commercial Air Curtains Commercial Kitchen DCV
Space Temperature Setpoint	22.2 C (72 F)	deg C (deg F)	Accepted based on engineering judgement. Typical conditions used in design projects. (Based on technical bulletin, ASHRAE 55-2013 notes that for thermal comfort purposes, temperature could range from between approximately 67 and 82 °F - https://www.ashrae.org/File%20Library/docLib/Technology/FAQs2014/TC-02-01-FAQ-92.pdf) is used in examples. (http://www.climate-master.com/downloads/lc1019-ashrae-journal-climate-master-gshp-vs-VRV_article.pdf , p.7) (Energy Management Handbook, Wayne C. Turner, Steve Doty, p. 335)	Commercial Condensing Make-Up Air Unit Commercial DCV Commercial Destratification Fans Commercial Air Curtains Commercial HRV Commercial ERV
OA temperature cooling system enabled	77.2°F (25.1°C)	deg C (deg F)	Average London, ON outside dry bulb temperature when temperature is above 72F based on TMY3 weather data	Commercial Air Curtains
Inside enthalpy for cooling season	22.7 Btu/lb	Btu/lb	Enthalpy at 72°F and 30% R.H. (ASHRAE Standard 62.1-2013 recommends that relative humidity in occupied spaces be controlled to less than 65% to reduce the likelihood of conditions that can lead to microbial growth. https://www.ashrae.org/File%20Library/docLib/Technology/FAQs2014/TC-02-01-FAQ-92.pdf)	Commercial Air Curtains
Outside enthalpy for cooling season	27.4 Btu/lb	Btu/lb	Average hourly London, ON enthalpy June-August based on TMY3 weather data. Link: http://climate.weather.gc.ca/climate_normals/normals_documentation_e.html?docID=1981 (Under the Data menu dropdown, "Canadian Weather year for Energy Calculation")	Commercial Air Curtains

This Update includes the following Measure Assumptions:

- Residential Adaptive Thermostat (New Construction/Retrofit)
- Residential High Efficiency Condensing Furnace (New Construction/Time of Natural Replacement)
- Residential High Efficiency Water Heaters (New Construction)
- Residential Low-Flow Showerheads
- Residential Low Flow Faucet Aerators (Retrofit)
- Residential Pipe Wrap (Retrofit)
- Residential Programmable Thermostat (Retrofit)
- Residential Tankless Water Heater (New Construction/Time of Natural Replacement)
- Residential Heat Reflector Panels
- Commercial Air Curtains (New Construction/Retrofit)
- Commercial Air Curtains with Vestibule (New Construction/Retrofit)
- Commercial Condensing Make Up Air Unit (New Construction/Time of Natural Replacement)
- Commercial Condensing Storage Gas Water Heater (New Construction/Time of Natural Replacement)
- Commercial Condensing Unit Heater (New Construction/Time of Natural Replacement)
- Commercial Demand Control Ventilation New Construction/Time of Natural Replacement)
- Commercial Demand Control Ventilation (Retrofit)
- Commercial Destratification Fans (New Construction/Retrofit)
- Commercial Energy Recovery Ventilator (55% effectiveness baseline)
- Commercial Energy Recovery Ventilator (No ERV baseline)
- Commercial ENERGY STAR Convection Oven (New Construction/Time of Natural Replacement)
- Commercial ENERGY STAR Dishwasher (New Construction/Time of Natural Replacement)
- Commercial ENERGY STAR Fryer (New Construction/Time of Natural Replacement)
- Commercial ENERGY STAR Steam Cooker (New Construction/Time of Natural Replacement)
- Commercial Heat Recovery Ventilator (55% effectiveness baseline)
- Commercial Heat Recovery Ventilator (No HRV baseline)
- Commercial High Efficiency Condensing Furnace (New Construction/ Time of Natural Replacement)
- Commercial High Efficiency Under-Fired Broiler (New Construction/Time of Natural Replacement)
- Commercial Infrared Heater (New Construction)
- Commercial Infrared Heater (Retrofit)
- Commercial Multi-Residential Showerhead
- Commercial Ozone Laundry (New Construction/Retrofit)

- Commercial Pre-rinse Spray Nozzle (New Construction/Time of Natural Replacement/Retrofit)
- Commercial Condensing Tankless Gas Water Heater (New Construction/ Time of Natural Replacement)
- Commercial Kitchen Demand Controlled Ventilation (New Construction/Time of Natural Replacement)
- Commercial Kitchen Demand Controlled Ventilation (Retrofit)

RESIDENTIAL – ADAPTIVE THERMOSTATS – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential → Space Heating → Adaptive Thermostats → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definition	
Measure Category	Retrofit (R) New Construction (NC)	
Baseline Technology	Non-Programmable (NPT) or Programmable Thermostat (PT)	
Efficient Technology	Adaptive Thermostat	
Market Type	Residential	
Annual Natural Gas Savings (m ³)	Retrofit - Retail Purchase	185 m ³
	Retrofit (Direct Install) - Replacing Non-Programmable Thermostat	217 m ³
	Retrofit (Direct Install) - Replacing Programmable Thermostat	173 m ³
	New Construction - Replacing Programmable Thermostat	105 m ³
Annual Electrical Cooling Savings (kWh)	Retrofit – Retail Purchase	176 kWh
	Retrofit (Direct Install)	235 kWh
	New Construction	206 kWh
Measure Life	15 years	
Incremental Cost (\$ CAD)	Retrofit	\$300
	New Construction	\$200
Restrictions	This measure requires that one adaptive thermostat would replace a conventional programmable or non-	

Parameter	Definition
	programmable thermostat serving one single zone heating appliance.

OVERVIEW

Adaptive thermostats employ advanced features beyond conventional programmable thermostats. These more sophisticated, yet easier to use devices, address key usability and programming issues of traditional units. Functions may include remote access for additional flexibility and control, an important feature when the user’s plans for the day have changed.

Leading manufacturers have developed competitive solutions in this area with unit prices ranging from \$200 to \$300.

APPLICATION

Residential customers that use a forced air heating and air conditioning system or hydronic space heating system would qualify under this program. Customers that have either a programmable or non-programmable thermostat would qualify for this measure.

BASELINE TECHNOLOGY

In the 2010 Lawrence Berkeley Labs study, “How People Actually Use Thermostats,” [1] research comprised of qualitative interviews, online surveys, and interaction experiments identified key barriers/issues with older style programmable thermostats. These included:

- Poor usability
- Time consuming & difficult to set up
- Menus too technical
- Confusing abbreviations
- Small and hard to read fonts
- Unpredictable at home & away times make programming useless
- Lack of feedback on programming

Adaptive or self-learning thermostats are different than traditional programmable thermostats and they resolve many of the challenges of programmable thermostats.

EFFICIENT TECHNOLOGY

Adaptive or self-learning thermostats typically have the following key features and benefits:

- Ease of creating schedules
- Intuitive set up, typically using narrative & lifestyle related questions

- Pro-active or forced automatic energy savings adjustment features
- Greater control with remote web or app based control over home’s settings if schedule changes
- Maintenance alerts
- Ongoing “Learning” of lifestyle schedules and preferences taking into account motion, humidity levels, occupancy and temperature preferences

While not inherently necessary for adaptive learning, most such thermostats also have wi-fi capabilities.

For an efficient technology to be eligible as a measure, the following four key automated features are required:

1. Proper setback scheduling
2. Occupancy based setbacks
3. System performance optimization
4. Encouragement of conservation behavior.

The features are subsequently described in additional detail.

Proper Setback Scheduling

Adaptive thermostats use different levels of sophistication to reduce the difficulties inherent in older thermostats when it comes to setting up a schedule. They typically use simpler dialogue-based set up menus where the user is prompted with lifestyle occupancy related questions. [2]

Occupancy-Based Setbacks

For households that do not maintain a regular schedule, this feature has an automated way of determining when a household is unoccupied. Geofencing and temperature/occupancy sensors are features that sense occupant location at any given time and will adjust schedules accordingly.

System Performance Optimization

System performance optimization capabilities use analytics to more efficiently run a household’s HVAC equipment. This is typically based on data collected from the system’s performance, coupled with feedback on external conditions such as temperature and humidity. While there is no direct communication between adaptive thermostats and the HVAC equipment, the data on system performance (HVAC equipment and building envelope) is 'learned' based on how the building temperatures respond to the thermostats control signals. This is largely an optimization of start-up and stop sequences, but also factors in feedback such as weather forecasts and humidity measurements. [2]

Encouraging Conservation Behavior

Encouraging conservation behavior leverages the on-going relationship that an adaptive thermostat builds to offer the occupants different forms of suggestions to conserve energy and

save money. This can range from suggestions to lower the temperature, accept a new optimized setback schedule, or to change the furnace filter. [2]

ENERGY IMPACTS

These devices typically have sensors that monitor light, humidity levels, motion and occupancy, temperature. Most adaptive thermostats build schedules by asking users simple questions during setup to understand the residents' typical schedules and comfort preferences. Algorithm-based software establishes heating and cooling schedules accordingly resulting in natural gas savings and electric cooling savings, in some cases even modifying the schedules for additional moderate savings.

NATURAL GAS AND ELECTRIC SAVINGS ALGORITHMS

In 2012, an independent impact and process evaluation study was conducted by the Cadmus Group on behalf of National Grid. [3] The Wi-Fi thermostat used in the pilot was an adaptive thermostat. This study reflects the climatic conditions for the Ontario Gas utilities.

A total of 86 households participated in the program accounting for 123 thermostats. Sixty-nine households were located in Massachusetts and 17 households were located in Rhode Island. The analysis was based on pre- and post-installation home energy use.

The gas savings attributed to the adaptive thermostat over a non-programmable thermostat replacement was 10% for the household. Comparatively, the gas savings attributed to the adaptive thermostat over a programmable thermostat was 8%. [3] As expected, when the Adaptive Thermostats are replacing programmable thermostats, the percent savings are lower than for non-programmable Thermostats. A smaller but similar study in New Hampshire found similar savings of 8%. [3] Manufacturer estimates of savings tend to be higher. NEST estimates 20% [4], ecobee estimates 23% [5], and Honeywell estimates about 20% for their Lyric.¹ [6]

Retrofit Natural Gas Savings

Savings from the Cadmus report were applied to end-use consumption by furnace type. First space heating energy use is calculated.

Enbridge load research data provides estimates of annual natural gas use of existing non-multifamily family homes with natural gas furnaces by furnace type (high, mid and conventional efficiency), as shown in Table 2.² [7] The market share of each furnace type is known from Enbridge's 2013 Residential Market Survey. [8] Unknown furnace types were

¹ Using their web calculator's default settings and assuming 2,077 m³ per year from below

² Natural gas forced air furnaces comprise approximately 90% of the residential space heating market in Enbridge Service territory. For the purposes of this substantiation document, it is assumed that furnace energy usage is representative of the 10% that use non-furnace gas heating systems.

distributed using known furnace type weighting. Based on this data the weighted average (column A * column C) Enbridge space heating single family natural gas use is 2,077 m³/yr.

Table 2. Enbridge Existing Single Family Home Space Heating Gas Use³ [8] [7]

Furnace Type, by Efficiency	Average Consumption for Furnace Type (m³) From 2012 Load Research Report (A)	% Furnace Type from 2008 Residential Survey (B)	% Furnace Type Adjusted to Exclude Unknown (C)
High	1,916	52%	61%
Mid	2,248	27%	32%
Conventional	2,698	6%	7%
Unknown		15%	
Weighted Average Consumption / Total %	2,077	100%	100%

Union Gas analysis of a sample of 50 homes found average natural gas use for space heating of 2,315 m³/yr. [9]

Based on a 60/40 share of customers for Enbridge and Union, respectively [10], the weighted average single family residential home energy use for space heating in Ontario is 2,172 m³/yr. This number is consistent with 2,158 m³ reported by Natural Resources Canada [11]. Applying the savings of 10% and 8% associated with replacement of non-programmable and programmable thermostats, respectively, the savings is 217 m³/yr for a non-programmable baseline and 174 m³/yr for a programmable baseline.

In the retail market the replaced thermostat type is unknown. Assuming 71% of the displaced thermostats are conventional programmable and 29% are nonprogrammable,⁴ the weighted average savings is 185 m³/yr for this scenario.

³ The “high” and “mid” annual energy use data comes from the Enbridge Gas Distribution Load Research-Strategy, Research and Planning group load research data as presented in Figure 1 of *Enbridge Load Research Newsletter* June 2012. The furnace type population distribution data comes from Residential Market Survey Data 2013, produced for Enbridge Gas Distribution by TNS, slide 41, weighted. Subsequent columns of data are calculated.

⁴ As of 2007, 39% of all Canadian dwellings had programmable thermostats, based on NRCAN data. [16] This estimate can be improved by considering additional factors. Ontario residents are 25% more likely than the average Canadian resident to have programmable thermostats, based on Statistics Canada data. [17] From the same source, homeowners, a group far more likely to buy adaptive thermostats than renters, were 15% more likely than average to have them and higher income households were 25% to 50% more likely than average households to have them. There are two other factors worth considering for which data were not available: The marketwide penetration has increased since 2007, and, the cohort of buyers willing to consider adaptive technology is more likely to have already invested in a programmable thermostat than the average buyer. Using a combined estimate of 33% more likely and then adding all of the adjustment factors together (additive is a conservative approach; the more logical multiplicative combining would lead to more than 100% programmable saturation), the estimated overall baseline replacement is 71% programmable.

Retrofit Electric Cooling Savings

Cooling load was derived from analysis provided by Toronto Hydro⁵ which establishes average annual electric energy use (kWh) related to air conditioning. The average annual electrical cooling consumption of 0.81 kWh/ft² was applied against the average house size of 1,812 ft² [8] as established in the Enbridge 2013 Residential Market Survey resulting in an estimated average cooling load for a typical customer of approximately 1,468 kWh/year. Applying the 16% savings as established in the Cadmus Report for electric cooling savings [3], results in an estimated electric cooling savings of 235 kWh/year.

$$\text{Retrofit Cooling Savings} = 0.81 \frac{\text{kWh}}{\text{ft}^2} \times 1,812 \text{ ft}^2 \times 16\% = 235 \frac{\text{kWh}}{\text{yr}}$$

For the retail purchase market it is not known if the adaptive thermostat also controls central air conditioning. In Ontario 58% of households had central air conditioning as of 2007 [12]. As with the programmable/nonprogrammable assessment, current adaptive thermostat buyers are more likely to have central air conditioning than the average household in 2007. Using an assumption of a 75% penetration, the retail purchase impact is 176 kWh/yr.

New Construction Natural Gas Savings

The estimated annual space heating natural gas use for new construction in Ontario is 1,315 m³.⁶ [13]. For new homes that otherwise would have a programmable thermostat,

$$\text{New Construction Natural Gas Savings} = 1,315 \text{ m}^3 \times 8\% = 105 \text{ m}^3$$

New Construction Electric Cooling Savings

Cooling load for the typical Ontario new construction archetype⁷ house is also derived from the Toronto Hydro data⁸ but is based on the electrical cooling consumption per square foot associated with the highest efficiency air conditioner rating. Applying this electrical cooling consumption of 0.59 kWh/ft² to the square footage of the new construction archetype (2,185 ft²), cooling load is estimated to be 1,282 kWh/year. Applying the 16% savings to this amount from

⁵ Peaksaver summary data provided by Toronto Hydro including 63,000 participants and based on a range of equipment efficiency and house sizes. Energy Efficiency ratings in the range of 9 to 13 BTU/w used by Toronto Hydro in their analysis was from the ASHRAE Fundamentals Handbook.

⁶ buildABILITY Final Report Table 5 Page 11 [12], The authors created a single building archetype in the modeling tool Hot2000 based on data from a sample of 100 recent new construction homes the Ontario Ministry of Municipal Affairs and Housing and from the Canada Mortgage and Housing Corporation Residential Building Activity Report. The energy use used in this document is that modeled for this archetype when located in Building Zone 1, the region with the most new construction activity in Ontario.

⁷ buildABILITY Final Report Table 10 Page 16, Heating Zone 1, Package [12]

⁸ Peaksaver data provided by Toronto Hydro including 63,000 participants and based on a range of equipment efficiency and house sizes. Energy Efficiency ratings in the range of 9 to 13 BTU/w used by Toronto Hydro in their analysis was from the ASHRAE Fundamentals Handbook.

the Cadmus Report [3] results in an estimated electric cooling savings of 205 kWh for new homes with central air conditioning.

$$\text{Retrofit Cooling Savings} = 0.59 \frac{\text{kWh}}{\text{ft}^2} \times 2,185 \text{ ft}^2 \times 16\% = 206 \frac{\text{kWh}}{\text{yr}}$$

ASSUMPTIONS

Table 3 provides a list of assumptions utilized in the measure savings algorithms to derive the savings values listed in Table 1 above.

Table 3. Assumptions

Definition	Inputs	Source/Comments
Average household size – existing homes	1,812 ft ²	[8]
Average household size – new construction	2,185 ft ²	[13]
Estimated annual gas consumption for new construction	1,315	[13]
Estimated average annual gas consumption for existing homes	2,172	From utilities surveys and billing analysis (blended value between utilities) as described in the Home Energy Use section above i
Annual savings fraction for residential new construction	8%	Calculated in algorithms section
Annual savings fraction for residential retrofit – non-programmable	10%	Calculated in algorithms section
Annual savings fraction for residential retrofit – programmable	8%	Calculated in algorithms section
Cooling savings fraction	16%	[3]
Annual electrical cooling consumption – new construction	0.59 kWh/ ft ²	Peaksaver data provided by Toronto Hydro
Annual electrical cooling consumption – existing homes	0.81 kWh/ft ²	Peaksaver data provided by Toronto Hydro

SAVINGS CALCULATION EXAMPLE

For savings derivations and results values, see the algorithms section.

USES AND EXCLUSIONS

This measure requires that one adaptive thermostat would replace a conventional programmable or non-programmable thermostat serving one single zone heating appliance.

MEASURE LIFE

Navigant Consulting estimates 15 years as the effective useful life base on the average lifetime of programmable thermostat from the ENERGY STAR website. [14]

INCREMENTAL COST

High-end adaptive thermostats such as the Nest and Honeywell Adaptive Thermostats retail at approximately \$250. [15] The cost of a programmable thermostat retails for \$50. Installation costs are similar for both types of thermostats. Hence the incremental cost to upgrade from a baseline code compliant programmable to adaptive thermostat at time of new construction is \$200, as shown in Table 4. For retrofits, the full adaptable thermostat material cost plus the labor associated with installation, nominally \$50 for a one half hour installation both apply and the total cost is \$300. This applies to both programmable and nonprogrammable baselines.

Table 4. Incremental Cost

Measure Category	Incremental Cost
Retrofit	\$300
New Construction	\$200

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RESIDENTIAL – HIGH EFFICIENCY CONDENSING FURNACE – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential → Space Heating → High Efficiency Condensing Furnace → New Construction/Time of Natural Replacement	

Table 1 below provides a summary of the key measure parameters and a savings coefficient.

Table 1. Measure Key Data

Parameter	Definitions
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)
Baseline Technology	90% AFUE
Efficient Technology	95% AFUE
Market Type	Residential
Annual Natural Gas Savings Rate (m ³ /kBtu/hr)	1.05 m ³ per kBtu/hr of input capacity
Measure Life	18 years
Incremental Cost (\$ CAD)	\$494
Restrictions	Installed equipment must have at least a 95% AFUE. This measure is restricted to central air furnaces in residential homes. In addition to residential type dwellings, this measure is also applicable to multi-residential dwellings where each home is served by a dedicated furnace(s) (either standalone or wall mounted)

OVERVIEW

The measure is for the installation of condensing furnaces with an AFUE of 95% or higher in residential homes. Condensing gas furnaces achieve savings through the

utilization of a sealed, super insulated combustion chamber, more efficient burners, and multiple heat exchangers that remove a significant portion of the waste heat from the flue gasses. As the heat exchangers remove waste heat from the flue gases, the gases condense and the resulting condensate must be drained.

APPLICATION

The measure is for the installation of condensing furnaces which have efficiencies that are higher than the code requirement for new homes. Residential furnaces (units with capacity of up to 225 kBtu/hr input) are performance rated by their annual fuel utilization efficiency or AFUE. This is a measure of the seasonal performance of the equipment and is more comprehensive than combustion or thermal efficiency measurements.

BASELINE TECHNOLOGY

Canada’s Energy Efficiency Regulations require that new residential furnaces have at least a 90% rated annual fuel utilization efficiency (AFUE) [1] [2]. For new construction installations, the baseline technology is considered to be the minimum efficiency required by the regulations established December 31, 2009.

Table 2. Baseline Technology

Type	AFUE
Gas Condensing Furnace	90%

EFFICIENT TECHNOLOGY

The efficient technology is a furnace with an AFUE rating equal to, or higher than 95%. This is the minimum efficiency for an ENERGY STAR furnace in Canada, effective February 1, 2013.

Table 3. Efficient Technology

Type	AFUE
Gas Condensing Furnace	95%

ENERGY IMPACTS

The primary energy impact associated with the installation of condensing furnaces is a reduction in natural gas usage resulting from improved efficiency.

The Ontario Building Code requires that all furnaces installed in new construction homes with permit pull dates after December 31, 2014 use brushless direct current motors (also known as electronically commutated motors, or ECMs). Such motors are significantly more efficient than traditional permanent split capacitor (PSC) type motors. With this code elevation, there is no electricity savings associated with the ECMs often installed with new condensing furnaces [3]. No water consumption impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

The annual gas savings factor is calculated in the formula below using an assumption for the equivalent full load hours (EFLH), derived by Caneta Research Inc, and the difference in assumed efficiencies for the equipment. The annual natural gas savings for a given size furnace can be calculated by multiplying the rated input of the furnace times the savings factor¹.

The natural gas savings factor attributed to this measure is calculated using the following formula:

$$NG \text{ savings factor} = \frac{EFLH}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{AFUE_{EE}}{AFUE_{base}} - 1 \right)$$

where,

<i>NG savings factor</i>	= Annual gas savings factor resulting from installing the new furnace (m ³ /yr)/(kBtu/hr)
<i>EFLH</i>	= Equivalent full load hours (hrs/yr)
$35.738 \frac{kBtu}{m^3}$	= Conversion of rated heating capacity from input kBtu/hr to m ³ /hr
<i>AFUE_{EE}</i>	= Efficient equipment AFUE (%)
<i>AFUE_{base}</i>	= Baseline equipment AFUE (%)

ASSUMPTIONS

The assumptions used to calculate the deemed savings coefficient are shown in Table 4.

¹ The Regulations are defined based on Btu/hr of gas input and residential boilers and most commercial heating equipment are also rated based on input capacity. Note that some residential furnace manufacturers rate the capacity based on Btu/hr output. For example, spot checks of manufacturer literature in August 2014 found that Trane, and Bryant publish furnace capacity based on output; Carrier and Rheem list input capacity. Increase the savings by 5% if output capacity is the basis.

Table 4. Assumptions

Variable	Definition	Inputs	Source
<i>EFLH</i>	Equivalent full load hours	675 hours ²	[4] based on the average London (Ontario) home

SAVINGS CALCULATION EXAMPLE

The example below shows how to calculate gas savings achieved from installing one condensing furnace with a rated input of 110 kBtu/hr. First the calculation of the savings factor is shown and then the calculation of the annual natural gas savings is shown from the savings factor.

$$NG \text{ savings factor} = \frac{675 \text{ hours}}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{95\%}{90\%} - 1 \right) = \frac{1.05 m^3}{\frac{kBtu}{hr}}$$

And,

$$Annual \text{ NG savings} = \frac{1.05 m^3}{\frac{kBtu}{hr}} \times 110 \frac{kBtu}{hr} = 115 m^3$$

USES AND EXCLUSIONS

To qualify for this measure the condensing furnaces must be gas-fired, have an AFUE of at least 95%, and be installed in a residential home. In addition to residential type dwellings, this measure is also applicable to multi-residential dwellings where each home is served by a dedicated furnace(s) (either standalone or wall mounted).

MEASURE LIFE

The measure life attributed to this measure is 18 years [5] [6]. Expert opinions and studies cited by NRCAN are 15, 18, and 20 years [7]. The ASHRAE handbook states that most heat exchangers have a design life of 15 years and the design life of commercial heating equipment is about 20 years. [8]

INCREMENTAL COST

The measure incremental cost is \$494³ based on the average difference in incremental cost between 90 AFUE and 95 AFUE residential furnaces. [9]

² Based on new construction homes only. See reference 3 for details.

³ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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RESIDENTIAL – HIGH EFFICIENCY GAS STORAGE WATER HEATERS – NEW CONSTRUCTION

Version Date and Revision History	
Version	1
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OEB Approval Date	
Residential → Water Heating → High Efficiency Gas Storage Water Heaters → New Construction	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definition	
Measure Category	New Construction (NC)	
Baseline Technology	ENERGY STAR power vented storage tank water heater	Energy factor of 0.67
Efficient Technology	High efficiency storage water heater	Energy factor of 0.80
Market Type	Residential	
Annual Natural Gas Savings (m ³)	68.3 m ³	
Measure Life	16 years	
Incremental Cost (\$ CAD)	\$545	
Restrictions	This measure is restricted to new construction installations in residential homes.	

OVERVIEW

This measure is for the installation of a new high efficiency gas storage water heater in the case of residential new construction.

There are two major categories of water heating equipment for domestic use: storage water heaters, which keep a supply of hot water in a tank, and those that do not store hot water and only heat water when it is needed.

Gas storage water heaters can further be differentiated by natural draft or power vented flue gas exhaust. A power vent is a fan that speeds the exhaust of combustion gases, which increases efficiency, which increases overall performance but requires additional capital cost. An ENERGY STAR power vent storage water heater is considered the baseline for this measure.

Storage water heaters have a lower capital cost than on-demand water heaters, but they also have standby heat losses associated with continuously maintaining water stored at high temperatures. Higher efficiency storage water heaters have tanks with generous amounts of insulation to reduce these losses and more efficient gas burners than standard efficiency storage water heaters.

APPLICATION

This measure focuses on high efficiency gas storage water heaters that have efficiencies above the basic code requirements (new construction projects or time of natural replacement) in a residential setting.

Gas storage water heaters are performance rated using an energy factor (EF). The EF is a measure of efficiency and it can be defined as the total energy delivered as hot water divided by the total energy consumed by the water heater over a 24-hour period in simulated use.

These ENERGY STAR units have an EF of 0.67 and the ability to produce at least 67 US gallons per hour of hot water after warm-up. This measure is intended to provide an incentive to install the highest efficiency power vented water heaters with an EF of 0.80 or greater. The energy consumption of high efficiency water heaters is calculated based on the daily and annual water consumption of a household (according to the number of people in the household) extrapolated from a hot water consumption research study undertaken by Natural Resources Canada (NRCAN) [1]. Tank volume capacity requirements are associated with the number of occupants and what is standard issue according to the manufacturers, e.g., a typical family of three to four people would warrant a 50-US gallon tank in order to meet the hot water demand for the household.

BASELINE TECHNOLOGY

For the new construction market, the ENERGY STAR rated power vented storage water heaters are considered baseline because experience indicates that this is a popular choice amongst homebuilders today in order to achieve an efficiency level that falls within the OBC SB-12 required compliance path as referenced in Table 2.1.1.2.A of that supplementary standard. [2] [3] A gas storage water heater with a minimum EF to qualify for ENERGY STAR is shown in Table 1.

Table 1. Baseline Technology

Type	Water Heater Input (Btu/hr)	EF
Gas storage water heater	<75,000	0.67

EFFICIENT TECHNOLOGY

A high efficiency gas storage heater with a minimum energy factor is shown in Table 2.

Table 2. Efficient Technology

Type	Water Heater Input (Btu/hr)	Minimum EF
Gas storage water heater	<75,000	0.80

ENERGY IMPACTS

Natural gas savings are achieved due to the difference in efficiencies between a high efficiency option and the baseline efficiency gas storage water heaters. The higher-efficiency equipment is typically able to both heat and store hot water more efficiently than the standard equipment.

There is a small amount of electrical savings for this measure, which have been shown to be negligible (<1 kWh annually) in the calculations.

NATURAL GAS SAVINGS ALGORITHMS

The following algorithms are referenced from the DOE Water Heater Analysis Model (WHAM) [4] and were used to calculate the stipulated gas impact in cubic meters per year and electric impact in kWh per year.

The total annual energy consumption for the water heater, Q_{in} , is calculated with the inlet water temperature specific to Ontario installations derived from the reference provided in Table 4 below. The total annual natural gas consumption of the water heater is the total annual energy consumption of the unit converted from British thermal units (Btus) to meters cubed.

The energy consumption of the high efficiency water heaters is calculated based on the daily and annual water consumption of a household (according to the number of people in the household) extrapolated from a hot water consumption research study undertaken by NRCan [5]. Tank volume capacity requirements are associated with the number of occupants and what is standard issue according to the manufacturers, e.g., a typical family of three to four people would warrant a 50-US gallon tank in order to meet the hot water demand for the household.

$$Q_{Out} = \rho \times V \times C_p \times (T_F - T_I)$$

where,

Q_{Out} = Energy required to heat tap water to tank temperature (Btu/day)

ρ = The density of water (lb/gal)

V = The daily drawn water (gal/day)

C_p = The specific heat of water (Btu/lb °F)

T_F = The water tank temperature (°F)

T_I = The inlet water temperature to the water heater (°F)

$$Q_{In} = 365 \times \left(\frac{Q_{Out}}{RE} + UA \cdot (T_{Tank} - T_{Amb}) \times \left(24 - \frac{Q_{Out}}{RE \cdot P_{On}} \right) \right)$$

where,

- Q_{In} = The total annual water-heater energy consumption (Btu/year)
- Q_{Out} = Energy required to heat tap water to tank temperature (Btu/day)
- RE = Recovery efficiency
- UA = Standby heat-loss coefficient
- T_{Tank} = Average tank temperature (°F)
- T_{Amb} = Ambient air temperature (°F)
- P_{On} = Water heater input rate (kBtu/hr)

$$\text{Annual NG consumption} = Q_{In}$$

Annual NG savings

$$= \text{Annual NG consumption (baseline)} - \text{Annual NG consumption (high efficiency)}$$

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithms to derive the stipulated savings values listed in Table 1 above. The algorithms are provided in the following section.

Table 4. Assumptions

Variable	Definition	Inputs		Source/Comments
		Base Efficiency	High Efficiency	
	Average single family residential household size	2.9		Common assumptions table
C_p	Specific heat capacity of water	1.00 Btu/lb °F		Common assumptions table
ρ	Density of Water	8.29 lb/gal		Common assumptions table
V	Daily drawn water	42 US gallons		[5]
RE	Recovery efficiency	0.78	0.90	[6]
UA	Standby heat-loss coefficient	5.78		[4]
T_{Amb}	Ambient air temperature	67.5°F (19.7°C)		[7]
T_{in}	Average city or inlet water temperature	48.9°F (9.39°C)		Common assumptions table
T_{Tank}	Domestic hot water factory set tank	120°F (48.9°C)		Common assumptions table

Variable	Definition	Inputs		Source/Comments
		Base Efficiency	High Efficiency	
	temperature			
P _{on}	Water heater input rate ()	44.89 kBtu/hr	40.00 kBtu/hr	[6]
	Tank size	50 US gallons		[5]
	Energy density of natural gas	35,738 m ³ /Btu		Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for a retrofit installation of a high efficiency storage tank hot water heater. For this example, it will be assumed that the equipment is sized for installation in a household size of three, which is the average household size in Ontario.

Q_{out} can be calculated with actual values for the daily drawn water volume and inlet temperature, but similarly to above. This value is the same for both the baseline and the high efficiency technology:

$$Q_{out} = 8.30 \times 30 \times 1.00 \times (120^{\circ}F - 48.9^{\circ}F) = 17,442 \text{ Btu}$$

Using Q_{out}, the total annual water heater energy consumption can be calculated as Q_{in} for both the baseline and the high efficiency equipment:

$$Q_{In\ base} = 365/1000 \times \left(\frac{17,442}{0.784} + 5.78 \times (120^{\circ}F - 67.5^{\circ}F) \times \left(24 - \frac{17,442}{0.784 \cdot 44,894} \right) \right) \\ = 14,145 \text{ kBtu}$$

Similarly,

$$Q_{In\ HE} = 11,724 \text{ kBtu}$$

Now the Q_{in} for the baseline and high efficiency technology can be subtracted and converted to meters cubed of natural gas savings.

$$\text{Annual NG savings} = 14,145 - 11,724 = 2,420 \text{ kBtu}$$

$$\text{Annual NG savings} = 2,420 \text{ kBtu} \times \frac{1,008}{35,738} = 68.3 \text{ m}^3$$

USES AND EXCLUSIONS

This measure requires that the gas storage water heaters be of a nominal input of 75 kBtu/hr or less and also be of the highest power vented efficiency or at least 0.80 EF.

MEASURE LIFE

The measure life is 16 years [8].

Residential high efficiency water heaters have a highly variable life expectancy because maintenance and water quality factors, such as hardness, can have a great effect on the equipment's lifetime [9] [10]. Most water heaters used in the Enbridge and Union areas are provided through water heater rental businesses and are therefore constructed of higher durability than standard units for purchase. This measure is also for the highest-efficiency units, which will have a more durable construction than standard units. Considering this, the lifetime referenced, though it's at the high end for typical residential units, is appropriate.

INCREMENTAL COST

The average approximate incremental cost, including installation, for a 40 to 50 US-gallon storage tank water heater is \$545^{1,2}

Note: At this point there is only one manufacturer of water heaters that meet the high efficiency criteria, but the units are sold under different trade names.

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¹Costs estimated and averaged for qualifying models using Home Depot, Menards, and Warners' Stellian websites, 2015.

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RESIDENTIAL – LOW-FLOW SHOWERHEADS – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential/Low-Income → Water Heating → Low-flow Showerheads → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings values based on the efficient technology.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	New Construction (NC) Retrofit (R)	
Baseline Technology	2.5 gpm	
Efficient Technology	1.5 gmp	
	1.25 gpm	
Market Type	Residential	
Annual Natural Gas Savings per Showerhead (m ³)	<i>Efficient Technology</i>	<i>Savings</i>
	1.25 gpm	28.2 m ³
	1.5 gpm	22.5 m ³
Annual Water Savings per Showerhead (liters)	1.25 gpm	13,885 liters
	1.5 gpm	9,546 liters
Measure Life	10 years	
Incremental Cost	Utility to use actual per showerhead cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.	
Restrictions	None.	

OVERVIEW

Hot water heating represents a large share of the energy consumption in homes. One of the simplest ways to reduce hot water heating costs is to reduce the amount of hot water use. Installing low-flow showerheads can have a noticeable impact on a residence's hot water consumption. The savings that can be achieved are attractive since this measure is relatively inexpensive and easy to implement.

Low-flow showerheads restrict the flow of the water while maintaining the water pressure.

APPLICATION

This measure pertains to the implementation of low-flow showerheads in single-family residential homes.

BASELINE TECHNOLOGY

The baseline technology is a showerhead with a flow of 2.5 gpm. [1]

EFFICIENT TECHNOLOGY

The efficient technology is a low-flow showerhead with a flow rate of 1.5 gpm or lower.

ENERGY IMPACTS

The primary energy impact associated with implementation of low-flow showerheads is a reduction in natural gas resulting from a reduction in the hot water consumption. There is reduction in water consumption associated with this measure.

NATURAL GAS SAVINGS ALGORITHM

This algorithm outlines a methodology to determine the energy consumption as a function of a showerhead's rated flow-rate. It is based on the methodology developed by Navigant Consulting using data from a SAS statistical billing analysis study with the specific purpose of determining the impact of low-flow showerheads in Ontario.

The SAS study [2] analyzed the gas consumption in Enbridge territory over the course of two years for 178 households which included a control group, a low-flow group, and a treatment group which had high-flow showerheads in the first year of the study. After a year into the study, showerheads in the treatment group were replaced with low-flow fixtures of 1.25 gpm.

The study resulted in two groups of savings: homes with showerheads that had pre-existing showerheads with full-on flow rates, or nominal/rated flow rates, between 2.0 gpm to 2.5 gpm and homes with showerheads with full-on flow rates greater than 2.5 gpm.

The full-on flow rate groups in the SAS sample and their associated savings levels are shown in Table 2:

Table 2. Savings from SAS Study [2] [3]

Rated Flow Rate	Average of Rated Flow Rates (gpm) ¹	Nominal Rated Flow of Low Flow Showerhead (gpm)	Nominal Flow Reduction (gpm)	Annual Savings (m ³) ²	Annual Savings Per Nominal gpm Flow Reduction (m ³ /gpm)
2.0 to 2.5 gpm	2.40	1.25	1.15	46.4	40.3
>2.5 gpm	3.09	1.25	1.84	87.8	47.7

The average reduction in annual natural gas use in each household was 44.0 m³ per gpm reduction in rated showerhead flow rate. Using this relationship, the gas savings can be calculated for any combination of baseline and high efficiency showerheads, if rated flow rate is known.

$$\text{Annual energy savings} \left(\frac{\text{m}^3}{\text{yr}} \right) = 44 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

Using this relationship, the gas savings can be calculated for any combination of baseline and high efficiency showerheads, if rated flow rate is known. The average number of showers in the SAS study was 2.06 per household. Using this factor, we can adjust the saving to a per showerhead basis.

$$\frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) = \frac{44 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})}{2.06 \frac{\text{showerheads}}{\text{household}}}$$

This results in a savings calculation of:

$$\frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) = 21.4 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

Because the population in the study had an average of 2.75 people per household as compared to 2.9 people per single family household based on census data, it is necessary to adjust the usage to reflect this.

$$\begin{aligned} \frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) \\ = 21.4 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm}) \times \frac{2.9 \text{ people}}{2.75 \text{ people}} \end{aligned}$$

$$\frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) = 22.5 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

¹ The average flow rate used here is from actual bag tested flow rate data provided by Enbridge Gas for the corresponding year of the SAS study (2007). [3]

² The savings presented here are from a SAS study, which analyzed consumption of households over two years, beginning in 2007. [2]

WATER SAVINGS ALGORITHM

The water savings were calculated using the following algorithm:

$$Savings = Ppl \times Sh \times 365 \frac{days}{year} \times T \times (Fl_{base} - Fl_{eff}) \times 3.785 \frac{L}{gal} \times PSA$$

Where,

<i>Savings</i>	= Annual savings in liters
<i>Ppl</i>	= Number of people per household
<i>Sh</i>	= Showers per capita per day
365	= Days per year
<i>T</i>	= Showering time (minutes)
<i>Fl_{base}</i>	= As-used flow rate with base equipment (gpm) – Calculated from equation from Summit Blue Study
<i>Fl_{eff}</i>	= As-used flow rate with efficient equipment (gpm) – Calculated from equation from Summit Blue Study
PSA	= Proportion of showerhead activity in residences affected by replacement (in order to adjust the water savings to account for residences with multiple showerheads)

Fl_{base} and *Fl_{eff}* are the “as-used” flow rate. The nominal flow-rate is the flow the showerhead will deliver at full flow at 80 psi. However, based on Enbridge flow rate bag test data, the flow for installed fixtures varies from the rated flow rate of the showerhead. [3] [4] [5].

The following regression based on a study in 443 California homes of+ weighted regression analysis of as-used flow compared to full-on flow rate:

$$As - Used Flow Rate^3 = 0.542 \times Nominal Flow Rate + 0.691 [4]$$

Where,

<i>As – Used Flow Rate</i>	= Actual flow of installed showerhead
<i>Nominal Flow Rate</i>	= Rated flow listed on the showerhead

ASSUMPTIONS

Table 7 provides a list of constants and assumption used in the derivation of the water savings values.

³ The lower limit of this equation is 1.25 gpm due to water pressure limitations. As the showerhead flow rate is reduced, the full-on flow will approach the as-used flow since as there is a limit to the acceptable flow-rate. [4] As such, the algorithm assumes that a showerhead with a full-on flow rate of 1.25 gpm also has an as-used flow of 1.25 gpm. Actual flow rates lower than 1.25 gpm can be assumed to result in longer showers, negating additional savings.

Table 7 Assumptions

Assumption	Value	Source
Average person per single detached house (2006)	2.9	Common assumptions table
Average number of people per single family residence in SAS study treatment group	2.75	[2]
Average number of showers per single family residence in SAS study treatment group	2.06	[2]
Showers per capita per day	0.75	[4]
Proportion of showerhead affected by replacement (PSA)	76%	[4]
Average showering time per day per showerhead (minutes)	7.6 minutes	[4]

SAVINGS CALCULATION EXAMPLE

The scenario for the gas savings is as follows. A showerhead will be replaced with a 1.5 gpm showerhead for a single family residence.

Natural Gas Savings

Using the equation above for the replacement of a baseline 2.5 gpm showerhead with a 1.5 gpm showerhead,

$$\text{Annual energy savings (m}^3/\text{yr)} = 22.5 \frac{\text{m}^3/\text{yr}}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

$$\text{Annual energy savings (m}^3/\text{yr)} = 22.5 \times (2.5 - 1.5)$$

$$\text{Annual energy savings} = 22.5 \frac{\text{m}^3}{\text{yr}}$$

Water Savings

$$\begin{aligned} \text{Savings} &= 2.9 \frac{\text{people}}{\text{residence}} \times 0.75 \frac{\text{showers}}{\text{person}} \times 7.6 \frac{\text{mins}}{\text{shower}} \times 365 \frac{\text{days}}{\text{year}} \\ &\times \left(2.05 \frac{\text{gallons}}{\text{min}} - 1.5 \frac{\text{gallons}}{\text{min}} \right) \times 3.785 \frac{\text{liters}}{\text{gal}} \\ &\times 76\% \text{ showerheads affected in each residence} = 9,546 \frac{\text{liters}}{\text{year}} \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure, low-flow showerheads must be implemented in residential homes.

MEASURE LIFE

The measure life attributed to this measure is 10 years. [4]

INCREMENTAL COST

The incremental cost for this measure could not be determined by looking at big-box retailer data. The driver for higher cost of fixtures is the available features of the showerheads. However, the previous substantiation sheet based the incremental cost on bulk purchases by the utility for program implementation. Since the incremental cost of the measure in the previous substantiation sheet is based on actual cost to the utility, it is the most accurate data. This method is consistent with other TRMs. Table 8 presents the measure incremental cost.

Table 8. Incremental Cost

Measure Category	Incremental Cost (\$)
All measure categories	Utility to use actual per showerhead cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.

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RESIDENTIAL – LOW FLOW FAUCET AERATORS –RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential → Water Heating → Low-Flow Bathroom and Kitchen Faucet Aerators → Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition		
Measure Category	Retrofit (R)		
Baseline Technology	Standard flow bathroom and kitchen aerators	2.2 gpm (8.35 lpm)	
Efficient Technology	Low flow bathroom and kitchen aerators.	1.0 gpm (3.8 lpm)	1.5 gpm (5.7 lpm)
Market Type	Residential, Multiresidential		
		1.0 gpm Aerator	1.5 gpm Aerator
Annual Natural Gas Savings (m ³)	Bathroom aerator	6.40 m ³	3.73 m ³
	Kitchen aerator	19.82 m ³	11.56 m ³
Annual Water Savings (liters)	Bathroom aerator	2,501 liters	1,459 liters
	Kitchen aerator	7,742 liters	4,516 liters
Measure Life	10 years		
Incremental Cost (\$ CAD)	\$1.14 – Kitchen \$0.60 - Bathroom		
Restrictions	Existing residential homes with natural gas fired water heaters		

OVERVIEW

The measure consists of installing either 1.0 or 1.5 gpm aerators on bathroom and kitchen faucets in residential dwellings. The aerators are provided to the dwelling occupants at no cost by the participating utility.

Reduction in water and natural gas consumption result from the measure. The magnitude of the site specific savings is heavily dependent upon human behavior and will vary significantly between sites. The savings algorithm and the resulting savings values are based on data and assumptions representing typical consumption patterns, inlet and outlet water temperatures, flow rates, and water heating equipment efficiencies. These factors are taken from studies that have been previously completed and are referenced in this document.

APPLICATION

This measure applies to the installation of 1.0 and 1.5 gpm bathroom faucet aerators in the residential settings. The measure is applicable to retrofit installation in existing facilities with natural gas fueled domestic water heating. The measure is also applicable to new construction with distribution through participating building contractors.

BASELINE TECHNOLOGY

The baseline technology is defined as an aerator with a flow rate of 2.2 gpm (8.3 lpm). This value is reflected in the Ontario Building Code and is consistent with the maximum allowable flow rate for all faucet aerators manufactured or sold in the United States after Jan 2014, as specified by US Energy Policy Act of 1992. [1]

Table 2. Baseline Technology

Type	Maximum Flow Rate
Code compliant faucet aerator	2.2 gpm (8.35 lpm)

EFFICIENT TECHNOLOGY

The high efficiency technology is a low flow aerator with a rated flow of 1.5 gpm (5.7 lpm) or less at a water pressure of 60 psi. [2]

Table 3. Efficient Technology

Type	Maximum Flow Rate
Low-flow faucet aerator	1.5 gpm (5.7 lpm)

ENERGY IMPACTS

This measure results in a reduction in water and natural gas consumption. The reduction in water consumption is a function of the baseline and efficient flow rates and typical per capita use patterns. Natural gas savings are dependent upon these factors, the % of the flow reduction

represented by heated water, typical entering and leaving hot water temperatures, and water heater efficiencies.

WATER AND NATURAL GAS SAVINGS ALGORITHMS

The measure savings are calculated using the following algorithms:

$$W_{savings} = Fu \times Ppl \times Dr\% \times Fa\% \times \left(\frac{Fl_{base} - Fl_{eff}}{Fl_{base}} \right) \times 3.78 \frac{\text{liters}}{\text{gallon}} \times 365 \frac{\text{days}}{\text{year}}$$

Where,

$W_{savings}$	=	Annual water savings (liters)
Fu	=	Faucet use per capita (gallons)
Ppl	=	Number of people per household
$Dr\%$	=	Percentage of flow that goes straight down the drain (%) This is the proportion of water use that depends on faucet on-time, such as when rinsing a toothbrush, as opposed to being dependent on the volume of water drawn, such as when filling a basin.
$Fa\%$	=	Single faucet use (bathroom or kitchen) as a % of total household faucet use (%)
Fl_{base}	=	Rated flow of baseline equipment (gpm)
Fl_{eff}	=	Rated flow of efficient equipment (gpm)

Once the reduction in water consumption is determined for each aerator, natural gas savings can be calculated using this water savings value and the following formula.

$$NG_{savings} = W_{savings} \times 8.33 \frac{BTU}{\text{gallon} - ^\circ F} \times \%_{hot} \times (T_{out} - T_{in}) \times \frac{\left(\frac{1}{RE} \right)}{35,738 \text{ BTU per } m^3}$$

Where,

$NG_{savings}$	=	Annual natural gas savings (m^3)
$W_{savings}$	=	Annual water savings from equation above (gallons/year)
$\%_{hot}$	=	% of aerator flow that is heated by water heater
T_{out}	=	Water temperature leaving the water heater ($^\circ F$)
T_{in}	=	Water temperature entering the water heater ($^\circ F$)
RE	=	Water heater recovery efficiency factor (%)

ASSUMPTIONS

The assumptions used to calculate the savings coefficients are shown in Table 4.

Table 4. Assumptions

Parameter	Description	Value	Source
F_u	Faucet use per capita	10.9 gallons / day (41.29 liters / day)	[3]
P_{pl}	Average people per household	2.9 people per household	Common assumptions table
$Dr \%$	Percentage of flow that goes directly down the drain ¹	70% - bathroom 50% - kitchen	[4]
$Fa \%$	The percentage to total faucet flow represented by each faucet	15% bathroom (per faucet) 65% kitchen faucet	[4]
T_{in}	Average city or inlet water temperature	9.39 °C (48.9 °F)	Common assumptions table
T_{hot}	Domestic hot water factory set tank temperature	48.9 °C (120 °F)	Common assumptions table
$\%_{hot}$	% of aerator flow that is heated	46%	[5] [6]
RE	Recovery Efficiency	78.68%	Common assumptions table

SAVINGS CALCULATION EXAMPLE

Inserting values from the list of assumptions provided in Table 4 into the water savings equation above leads to a water consumption reduction for a single 1.5 gpm bathroom aerator of:

$$10.9 \text{ gallon/day per person} \times 2.9 \text{ people} \times 70\% \times 15\% \times (2.2 - 1.5) / 2.2 \times 365 \text{ days/year} \times 3.785 \text{ liters/gallon} = \mathbf{1,459 \text{ liters/year}} \text{ (385.4 gallons per year)}$$

Inserting the water savings value, temperatures and water heater recovery efficiency into the natural gas savings equation leads to annual natural gas savings of:

¹ There is no research data on the percentage of water that flows straight down the drain. Assuming that it's probably not all straight down the drain nor is it all batch use for kitchen faucets, a range of 25% to 75% was assumed with 50% as the point estimate. For bathroom faucets, one would expect less batch use than in the kitchen, but not 0% so the range was set from 50% to 90% straight down the drain, with 70% as the point estimate.

$$385.4 \text{ gallons / year} \times 46\% \text{ heated water} \times 8.33 \text{ BTU / gallon} \cdot ^\circ\text{F} \times (120 - 48.9) ^\circ\text{F} / 78.68\% / 35,738 \text{ BTU/m}^3 = \underline{\underline{3.73 \text{ m}^3 \text{ natural gas}}}$$

USES AND EXCLUSIONS

To qualify for this measure aerators must meet the maximum flow requirement listed in Table 3, and be installed in new or existing residential dwellings equipped with natural gas fueled water heaters.

MEASURE LIFE

The measure life attributed to this measure is 10 years. [7]

INCREMENTAL COST

Table 5 presents the measure incremental cost.

Table 5. Incremental Cost [8]

Boiler Rated Input (Btu/h)	Incremental Cost (\$)
High Efficiency Aerator	\$1.14 – Kitchen \$0.60 - Bathroom

The cost is equipment cost associated with bulk purchases by the participating utility for direct distribution to residential end users.

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RESIDENTIAL – PIPE WRAP – RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential → Water Heating → Pipe Wrap → Retrofit	

Table 1 Table 1 provides a summary of the key measure parameters and savings.

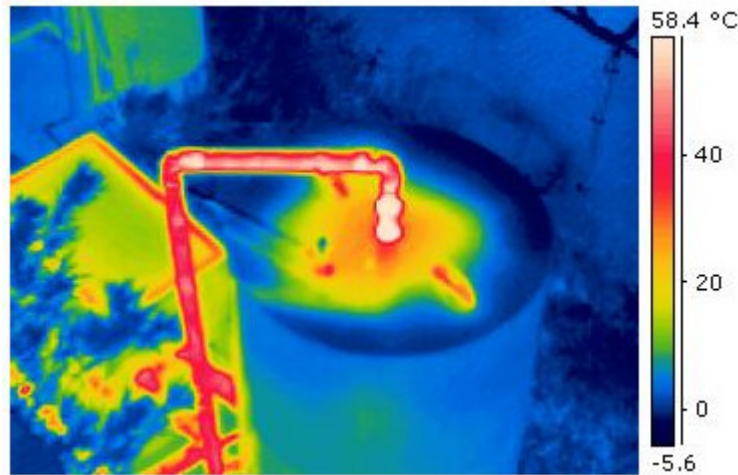
Table 1. Measure Key Data

Parameter	Definition
Measure Category	Retrofit
Baseline Technology	No existing pipe wrap
Efficient Technology	Pipe wrap
Market Type	Residential
Annual Natural Gas Savings Rate (m ³ /ft)	3.54 m ³ /ft.
Measure Life	15 years [1]
Incremental Cost (\$ CAD)	\$0.39 per foot
Restrictions	This measure is restricted to retrofit installations in residential homes. The savings are applicable for pipe wrap of up to two meters (6.56 ft) in length.

OVERVIEW

This measure provides the gas savings estimate and costs of insulating hot water pipes for conventional gas hot water storage tanks in a residential retrofit type of application. Figure 1 illustrates the heat loss phenomenon. Natural gas savings are calculated using an engineering algorithm and are reported in meters cubed per linear foot (m³/ft).

Figure 1: Temperature of Hot Water Pipe Exiting Water Heater¹



APPLICATION

This measure is for pipe-wrap for domestic hot water heating systems in residential homes.

BASELINE TECHNOLOGY

The baseline case is a hot water pipe without pipe wrap insulation. The R-value is shown in Table 2.

Table 2. Baseline Technology

Type	Value
No pipe wrap	R-0.435 [2]

This value is based on the heat transfer between water and air through copper with a heat transmission coefficient $U=2.3 \text{ Btu/ft}^2 \cdot \text{°F} \cdot \text{h}$.

EFFICIENT TECHNOLOGY

The energy efficient case is a hot water pipe with pipe wrap insulation. The R-value of the pipe wrap is shown in Table 3.

Table 3. Efficient Technology

Type	Value
Added pipe wrap insulation (R_{Post})	$R_{\text{Pre}} + R-4.35^2$ [3]

¹ Photograph by Dylan Pankow. Downloaded from <https://www.flickr.com/photos/cbcthermal/1475767378/in/photostream/> on 8/1/2014.

² Added insulation has an U-value of $0.230 \text{ BTU-in/hr-ft}^2 \cdot \text{°F}$

This value is based on a nominal ½-inch diameter copper pipe with ½-inch polyethylene insulation.³

ENERGY IMPACTS

Natural gas savings are achieved due to the difference in thermal resistance (R) between the energy efficient pipe wrap and the baseline condition of zero pipe wrap. The insulated pipe wrap reduces the rate of heat flow between the hot water in the pipe and the ambient air surrounding the pipe. This reduction of heat loss with insulated pipes can raise water supply temperature 1.1 °C-2.2 °C (2°F-4°F) [4] as compared with uninsulated pipes.

NATURAL GAS SAVINGS ALGORITHMS

The following algorithm is referenced from the Home Energy Services Impact Evaluation [5] and was used to calculate the stipulated gas impact. The total annual gas savings per linear foot, *S*, is calculated based on the difference in R values as shown in Table 4 below.

$$S = \frac{\left[\left(\frac{1}{R_{pre}} - \frac{1}{R_{post}} \right) \times C_{pipe} \times (T_{pipe} - T_{amb}) \times 8760 \times TRF \right]}{RE \times 35,738 \frac{Btu}{m^3}}$$

where,

S = Annual gas savings (m³/ft)

R_{pre} = R-value of baseline equipment (ft²·°F·h/Btu)

R_{post} = R-value of efficient equipment (ft²·°F·h/Btu)

C_{pipe} = Circumference of the outlet water pipe (ft)

T_{pipe} = Temperature of the outlet water pipe (°F)

T_{amb} = Ambient air temperature (°F)

TRF = Thermal regain factor, which discounts savings because reducing heat loss to conditioned space in the heating season is not beneficial⁴

$$TRF = \left[1 - \left(Regain \times \frac{Heating\ Hours\ per\ Year}{Total\ Hours\ per\ Year} \right) \right]$$

³ The cited reference is web available and includes the material conductivity. The equivalent R-value can be calculated from radial heat loss equation and was also provided in a separate company spec sheet of the same name and title as the cited spec sheet, but that is not available on line.

⁴ Regain is a function of both space type and insulation level. Adding insulation to pipes in fully conditioned space with thermostatically controlled heating systems saves no energy in the heating season because the water heater waste heat offsets heating system energy (Regain=100%). While most water heaters are located within insulated space in Ontario, no data was found on the proportions of them in spaces heated with thermostatically controlled systems versus those in unconditioned or semi-conditioned space. In lieu of this the average value calculated for Massachusetts in [5] was used. For simplification, the analysis does not consider interactive effects with semi-conditioned spaces warmed with electric resistance spot heaters.

RE = Water heater recovery efficiency

$$S = \frac{\left[\left(\frac{1}{0.435} - \frac{1}{4.785} \right) \times 0.164 \times (120 - 67.5) \times 8760 \times \left[1 - \left(0.58 \times \frac{5,567}{8,760} \right) \right] \right]}{0.7868 \times 35,738}$$

$$\text{Annual NG savings} = 3.54 \text{ m}^3/\text{ft}$$

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithm to derive the stipulated savings values listed in Table 1 above.

Table 4. Assumptions

Variable	Definition	Value	Source/Comments
R_{pre}	R-value of baseline equipment	0.435 ft ² ·°F·h/Btu	[2]
R_{post}	R-value of efficient equipment (baseline + additional insulation)	4.785 ft ² ·°F·h/Btu	Sum of baseline equipment R and pipe wrap R. [3]
C_{pipe}	Circumference of outlet water pipe	0.164 ft	Based on copper pipe with ½-inch nominal 5/8-inch actual outside diameter [3]
T_{pipe}	Domestic hot water factory set tank temperature	120°F (48.9°C)	Common assumptions table (no heat trap)
T_{amb}	Ambient air temperature	67.5°F (19.7°C)	[6]
<i>Regain</i>	Regain	0.58	[5]
<i>RE</i>	Recovery efficiency	78.68%	Common assumptions table
	Energy density of natural gas	35,738 Btu/m ³	Common assumptions table
	Total hours per year	8,760	
	Heating hours per year	5,567	Common assumptions table

The savings are applicable for pipe wrap of up to two meters (6.56 ft) in length.

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for a pipe wrap retrofit installation on a residential hot water heater for a two meter (6.56 ft) length of pipe. For this

example, it will be assumed that the equipment is sized for installation in a household size of 2.9, which is the average household size in Ontario.

$$\text{Annual NG savings} = 3.54 \frac{m^3}{ft} \times 6.56 ft = 23.2m^3$$

MEASURE LIFE

The measure life is 15 years [1].

INCREMENTAL COST

The average approximate incremental cost, assuming homeowner installation, of pipe wrap on a hot water outlet pipe is approximately \$0.39 per foot [7].⁵

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⁵ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

RESIDENTIAL – PROGRAMMABLE THERMOSTATS – RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential → Space Heating → Programmable Thermostats → Retrofit	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definition
Measure Category	Retrofit (R)
Baseline Technology	Nonprogrammable thermostat
Efficient Technology	Programmable thermostat with at least two programming modes (weekday and weekend)
Market Type	Residential
Annual Natural Gas Savings (m ³)	46 m ³
Measure Life	15 years
Incremental Cost	\$97
Restrictions	Limited to replacement in situations where existing thermostat is identified as non-programmable

OVERVIEW

Residential home heating and cooling system thermostats maintain temperature in the spaces by either turning equipment on and off as necessary or modulating the systems to address the heating and cooling loads. Setting the temperatures back when residences are unoccupied or the residents are sleeping presents a significant potential for savings, as it reduces heat loss and allows the heating and cooling systems to operate for shorter periods of time.

APPLICATION

This measure is for the installation of a programmable thermostat in the residential homes in place of nonprogrammable thermostats. Because the 2012 Ontario Building Code requires

programmable thermostats in new construction homes this measure is applicable for retrofits only.

BASELINE TECHNOLOGY

The baseline for this measure is a manual thermostat.

EFFICIENT TECHNOLOGY

The efficient technology is a programmable thermostat with at least two programming modes for weekdays and weekends. The thermostat should already have pre-programmed modes from the manufacturer.

ENERGY IMPACTS

Natural gas savings are achieved due to the heating system having to heat at a lower temperature during the evening and unoccupied hours.

There is a small amount of electrical savings for this measure for homes with AC systems. Based on RECS data for the Northeast United States and the TMY3 data for London, Ontario, the cooling hours are very limited for this measure, especially during setback periods.

NATURAL GAS SAVINGS ALGORITHMS

The approach used to calculate savings is to:

- (1) Estimate the annual average natural gas heating energy used in Ontario homes.
- (2) Calculate the theoretical technical savings potential based on a switch from a fixed setpoint to a programmed night setback, expressed as a percentage of annual heating energy use;
- (3) Develop one behavioral factor to discount savings due to the fact that some manual thermostat owners manually reduce their setpoint at night or during unoccupied daytime periods;
- (4) Develop a second behavior factor to discount savings due to the fact that some programmable thermostat owners do not program their thermostats as aggressively as the technical savings potential assumes; and
- (5) Combine the factors to estimate annual natural gas savings.

Home Energy Use

Enbridge load research data provides estimates of annual natural gas use of existing non-multifamily family homes with natural gas furnaces by furnace type (high, mid and conventional efficiency).¹ [1] The market share of each furnace type is known from Enbridge’s 2013 Residential Market Survey. [2] Unknown furnace types were distributed using known furnace type weighting. Based on this data the weighted average (column A * column C) Enbridge space heating single family natural gas use is 2,077 m³/yr.

Table 2. Enbridge Existing Single Family Home Space Heating Gas Use² [2] [1]

Furnace Type, by Efficiency	Average Consumption for Furnace Type (m ³) From 2012 Load Research Report (A)	% Furnace Type from 2008 Residential Survey (B)	% Furnace Type Adjusted to Exclude Unknown (C)
High	1,916	52%	61%
Mid	2,248	27%	32%
Conventional	2,698	6%	7%
Unknown		15%	
Weighted Average Consumption / Total %	2,077	100%	100%

Union Gas analysis of a sample of 50 homes found average natural gas use for space heating of 2,315 m³/yr. [3]

Based on a 60/40 share of customers for Enbridge and Union, respectively [4], the weighted average single family residential home energy use for space heating in Ontario is 2,172 m³/yr.

Theoretical Technical Savings Potential

A common rule of thumb for thermostat setback savings is 1.8% of annual heating energy use per degree C (1% per degree F) for an 8 hour per night setback adjustment.³ [5] [6]. The most common presumption for technical savings potential is 8°F setback. Therefore the technical savings potential is 8%.

¹ Natural gas forced air furnaces comprise approximately 90% of the residential space heating market in Enbridge Service territory. For the purposes of this substantiation document, it is assumed that furnace energy usage is representative of the 10% that use non-furnace gas heating systems.

² The “high” and “mid” annual energy use data comes from the Enbridge Gas Distribution Load Research-Strategy, Research and Planning group load research data as presented in Figure 1 of *Enbridge Load Research Newsletter* June 2012. The furnace type population distribution data comes from Residential Market Survey Data 2013, produced for Enbridge Gas Distribution by TNS, slide 41, weighted. Subsequent columns of data are calculated.

³ This savings fraction can be supported through simple analysis of hourly weather data. Many articles on program thermostat savings potential directly or indirectly cite a 1978 study *Energy Savings through Thermostat Setbacks*, Nelson, Lorne W. and J. Ward MacArthur (1978), ASHRAE Transactions, Volume 83, AL-78-1 (1): 319-333. The article itself was not readily accessible, but the referenced University of Alberta document summarizes it well. The archived but accessible ENERGY STAR programmable thermostat calculator uses this same rule of thumb in citing “Industry data (2004)” and using a 3% savings per degree per 24 hours of reduction, the same as 1% per 8 hours.

https://www.energystar.gov/ia/partners/promotions/cool_change/downloads/CalculatorProgrammableThermostat.xls

Behavior Factor – Baseline

The theoretical technical savings potential is based on the thermostat being set to a constant temperature. Field studies and telephone surveys have found that some residents with manual thermostats set them back at night. This reduces the technical savings potential. Two studies focused on this particular factor and found 44% [7] and 66% [8] of users do this. A third study found that residents with manual thermostats actually set back their temperature 1.49 hours per week more often than those with programmable thermostats, leading to about a (3%) realization rate.⁴ [9] The authors speculate that the reason for this is due to factors such as being able to pre-heat the home before awaking with a programmable thermostat. Two of the studies do not quantify the number of degrees of setback. Data from the third study indicates a median of 4 to 5 degrees of night setback for those that manually do so. [7]

If the three values are averaged 71% of the theoretical technical potential is lost due to pre-retrofit behavior mimicking the desired post-retrofit behavior. We discounted this baseline penalty factor by 1/3 based on the professional judgment that the referenced studies did not all directly compare before and after setpoints. We expect that on average both the systematic benefits of programmability and the likelihood of additional degrees of setback when programmed result in some additional savings even for those that previously manually set back their thermostats.

$$\text{Pre-retrofit savings behavior discount factor} = \left(\frac{44\% + 66\% + 103\%}{3} \right) \times \frac{2}{3} = 47\%$$

where,

Pre-retrofit savings behavior discount factor = savings reduction due to manual energy efficient behavior such as manual setback in the pre-retrofit case

Behavior Factor – Post-Retrofit

A number of studies have found that programmable thermostat owners do not configure setpoints in such a way that they will achieve the nominal 8% savings presented in the technical potential section. Quantifications of this phenomenon are listed below for programmable thermostat owners and space heating controls:

- 53% set them in “hold mode”⁵ [10]
- 38% do not use them to reduce temperature at night⁶ [11]
- 60% on hold (low income-specific)⁷ [10]

⁴ 1.49 hr. /week / (8 hr. /day * 7 days/wk.) nominal presumed extra setback hours per week per technical potential basis = 3%.

⁵ Carrier study of 35,471 programmable thermostats in the territories of LIPA, Con Edison, SCE, and SDG&E as cited in [10].

⁶ Based on total US homes participating in RECS survey.

- Unquantified impact due to poor usability of conventional programmable thermostats.⁸ [10]

Preprogramming of thermostats helps and was an ENERGY STAR requirement when the label existed, [12] but the majority of owners reprogram or otherwise override the settings from their factory settings. Averaging these three values is a representation of the percentage of savings not realized because of programmable thermostats being used as fixed manual thermostats.

The average is 50%. *Post – retrofit savings behavior discount factor* = $\left(\frac{53\%+38\%+60\%}{3}\right) = 50\%$

where,

Pre-retrofit savings behavior discount factor = savings reduction due to inadequate use of the control features of a programmable thermostat

Savings Calculations

Using the behavior adjustment values estimated above and applying them to the theoretical savings, the total savings fraction is 2.1%:

$$\text{Annual savings fraction} = 8\% \times (100\% - 47\%) \times (100\% - 50\%) = 2.1\%$$

For comparison below are findings from prior studies regarding overall savings:

- 0% difference in setpoints on average⁹ [13]
- 0% effect on net unit energy consumption (UEC) ¹⁰ [14]
- (18%) savings¹¹
- 6.8% savings¹² [15]
- 3.6% savings¹³

⁷ Based on on-site inspections of low income residences finding 45% on hold, 30% programmed, and 25% off, not visible, or reported as nonprogrammable (small sample).

⁸ Six different studies are cited in Meier, 2010.

⁹ "Respondents with programmable thermostats report thermostat setpoints that are not substantially different from those of respondents with manual thermostats"

¹⁰ "Essentially zero," per *Three-Block Regression Analysis Regarding Effects of Programmable Thermostats on Setpoint Behavior and Electric Central Air/Gas Heat UECs*. Prepared for Southern California Edison by Athens Research. 2005, as cited in Dyson, 2005.

¹¹ It must be noted that this analysis did normalize for home physical characteristics and weather but did not adjust for any characteristic behavioral differences between those with and without programmable thermostat. *Programmable Thermostats Installed into Residential Buildings: Predicting Energy Saving Using Occupant Behavior & Simulation*, prepared for Southern California Edison by James J. Hirsch & Associates. 2004, as cited and described in Dyson, 2005.

¹² This report's recommended results are contrary to the others. It is oft-cited and is based on a relatively robust method: Pre- and post-retrofit billing analysis with participants and a nonparticipant control group, with subsequent adjustment and normalization for the presence of other measures, home size, and other factors. The authors used several methods before settling on the preferred one that resulted in the 6.8% savings. One reviewer observed that an alternate approach presented in the report that used a participation indicator (the reviewer's preference) and led to significantly lower savings of 1.7% to 1.8%. For this commentary see Cadmus et al, 2012. [18]

Once the annual average residential usage is determined, the annual energy savings due to programmable thermostats (NG Savings, in m³), are as follows:

$$NG\ Savings = ARSH \times Annual\ savings\ fraction$$

ASSUMPTIONS

Table 3 provides a list of assumptions utilized in the measure savings algorithms to derive the stipulated savings values listed in Table 1 above. The algorithms are provided in the following section.

Table 3. Assumptions

Definition	Inputs	Source/Comments
Annual average residential household space heating natural gas use	2,172 m ³	From utilities surveys and billing analysis (blended value between utilities) as described in the Home Energy Use section above
Annual savings fraction	2.1%	Calculated above

SAVINGS CALCULATION EXAMPLE

The savings for this measure is calculated as follows:

$$NG\ Savings = ARSH \times Annual\ savings\ fraction$$

$$NG\ Savings = 2,172\ m^3/year \times 2.1\% = 46\ m^3/year$$

USES AND EXCLUSIONS

This measure requires that the thermostat have two programming modes for weekday and weekend.

MEASURE LIFE

The measure life for this measure is 15 years. [16]

INCREMENTAL COST

The cost of a programmable thermostat is \$97.¹⁴ [16]

¹³ *Programmable Thermostats Report to KeySpan Energy Delivery on Energy Savings and Cost Effectiveness* GDS Associates. , 2002, as cited in Cadmus (2012). Not found on line. This value also recommended by Cadmus for MA.

¹⁴ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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RESIDENTIAL –TANKLESS GAS WATER HEATERS – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
End date	N/A
Residential → Water Heating → Tankless Water Heater → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings values.

Table 1. Measure Key Data

Parameter	Definition
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)
Baseline Technology	Storage Water Heater, EF = 0.67
Efficient Technology	High Efficiency Non-Condensing Tankless Water Heater, EF = 0.82
	Condensing Tankless Water Heater, EF = 0.91
Market Type	Residential
Annual Natural Gas Savings (m ³)	High Efficiency Non-Condensing Tankless: 88.8 m ³
	Condensing Tankless: 128.0 m ³
Measure Life	20 years
Incremental Cost (\$ CAD)	High Efficiency Non-Condensing Tankless = \$1,667
	Condensing Tankless = \$2,066
Restrictions	This measure applies to the installation of natural gas tankless water heaters in residential buildings.

OVERVIEW

The measure consists of the installation of natural gas tankless water heaters for domestic hot water production in residential buildings. Natural gas tankless water heaters are available in both condensing and non-condensing models.

Tankless, also called instantaneous or on-demand, water heaters provide hot water without using a storage tank. There is nominal “storage”, ranging from 2-10 gallons within the heat exchanger, but this represents 5% or less of the storage tank capacity associated with equivalent storage water heaters. The reduced storage capacity results in the need for higher capacity burners to generate the flow of hot water necessary to serve equivalent peak loads. This translates to higher equipment and installation costs for these units.

The algorithm and the associated variables are presented in the section “Natural Gas Savings Algorithm”.

APPLICATION

This measure provides incentives for installing tankless natural gas water heaters in residential buildings for the new construction and TNR measure categories.

Tankless water heaters are performance rated differently depending on their size. Those above 250 kBtu/hr are rated for their thermal efficiency and those below 250 kBtu/hr are rated for their energy factor (EF). The EF is an average daily efficiency that includes all standby or storage losses, while thermal efficiency is a short term measure of the equipment’s performance that includes flue losses but no other losses. Residential water heaters are typically smaller than 250 kBtu/hr.

BASELINE TECHNOLOGY

The residential water heater minimum efficiency requirement varies as a function of the prescriptive compliance path chosen from those offered in the Ontario Building Code Supplemental Standard SB-12, Table 2.1.1.2.A. [1] ENERGY STAR rated power vented storage water heaters are considered baseline because experience indicates that prescriptive paths that use this energy factor specification is a popular choice amongst Ontario new homebuilders today in order to comply with code. [2] [3] [4]. A gas storage water heater with a minimum EF to qualify for ENERGY STAR is shown in Table 2 and is assumed to be the baseline in New Construction and TNR installations.

Table 1. Baseline Technology

Type	Minimum Energy Factor (EF)
Gas storage water heaters	0.67

EFFICIENT TECHNOLOGY

The high efficiency technology is a natural gas fueled tankless water heater with minimum rated EFs in Table 3. 0.82 is the minimum EF allowable for ENERGY STAR eligibility, which also is the minimum required for Union and Enbridge program incentive eligibility as of October 2014 [4]. 0.91 is the minimum rated EF of a condensing tankless water heater from the Natural Resources Canada (NRCAN) list of available products [5]. Both non-condensing and condensing units are eligible for this measure.

Table 2. Efficient Technology

Type	Minimum EF
Tankless gas water heater	0.82
Condensing Tankless gas water heater	0.91

ENERGY IMPACTS

Natural gas savings are achieved as a result of the higher overall average efficiencies of the tankless units and elimination of storage or standby losses.

There is no water consumption impact associated with this measure and the electric impacts are negligible. Condensing units typically require electricity for powered venting. The baseline in Ontario also is power vented so there is no associated electric energy impact with venting. Some condensing units require small condensate pumps that run for a few minutes a day but this electricity use is not significant.

NATURAL GAS SAVINGS ALGORITHMS

The natural gas savings are calculated using the algorithms below, which are based on EFs and the average annual DHW heating load. The average annual DHW heating load is derived from a study of hot water use conducted by NRCAN, Union Gas, and Caneta Research Inc. who metered a sample of residential hot water heaters in Ontario [6].

$$\text{Annual NG Savings} = \frac{\text{DHWload}}{35.738 \frac{\text{kBtu}}{\text{m}^3}} \times \left(\frac{1}{\text{EF}_{\text{baseline}}} - \frac{1}{\text{EF}_{\text{EE}}} \right)$$

and,

$$\text{DHWload} = \text{dailyDHW} \times 365 \frac{\text{days}}{\text{yr}} \times \rho \times C_p \times (T_s - T_c) / 1,000$$

where,

$$\text{Annual NG Savings} = \text{Annual natural gas saving (m}^3\text{), see Table 1}$$

$DHWload$	= Annual domestic hot water heating load (kBtu), calculated
$EF_{baseline}$	= The assumed baseline storage water heater EF
EF_{EE}	= The assumed tankless water heater EF
$dailyDHW$	= The average daily Canadian DHW consumption (US Gallons)
$365 \frac{days}{yr}$	= Days in a year
ρ	= Density of water (lb/US gallon)
C_p	= Specific heat of water (Btu/lb/°F)
T_s	= Average temperature of DHW (°F)
T_c	= Average temperature of city supply water (°F)

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithms to derive the savings values listed in Table 1 above.

Table 4. Assumptions

Variable	Definition	Inputs	Source/Comments
$dailyDHW$	The average daily DHW consumption	54 US Gallons	NRCan, Union Gas, and Caneta Research Inc. [6]
ρ	Density of water	8.29 lb/US Gal	Common assumptions table
C_p	Specific heat of water	1 Btu/lb/°F	Common assumptions table
T_s	Temperature of DHW water	48.9°C (120 °F)	Common assumptions table
T_c	Temperature of city supply water	9.3°C (48.9 °F)	Common assumptions table
	Energy density of natural gas	35,738 Btu/m ³	Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings were calculated. The annual domestic hot water heating load can be calculated using the average daily household DHW consumption in Canada.

$$\begin{aligned}DHWload &= 54 \frac{US\ Gal}{day} \times 365 \frac{days}{yr} \times 1 \frac{Btu}{lb^{\circ}F} \times 8.29 \frac{lb}{US\ gal} \times (120^{\circ}F - 48.9^{\circ}F)/1000 \\ &= 11,608\ kBtu/yr\end{aligned}$$

The natural gas savings for a non-condensing tankless water heater can then be calculated from the difference in equipment efficiencies as:

$$Natural\ Gas\ Savings = \frac{11,617\ kBtu/yr}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{1}{0.67} - \frac{1}{0.82} \right) = 88.8\ m^3/yr$$

And the natural gas savings for a condensing tankless water heater can be calculated similarly as:

$$Natural\ Gas\ Savings = \frac{11,617\ kBtu/yr}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{1}{0.67} - \frac{1}{0.91} \right) = 128.0\ m^3/yr$$

USES AND EXCLUSIONS

Natural gas-fueled tankless water heaters installed in residential buildings qualify for this measure. The measure type must be new construction or TNR.

MEASURE LIFE

The measure life is 20 years [7].

INCREMENTAL COST

The incremental cost data is taken from an incremental cost study completed for six efficiency programs in the northeast US during 2011. [8]

Data reviewed from this and other studies did not show significant variation in incremental cost over the anticipated size range. The average values from the study are reported in Table 5.

Table 5. Incremental Cost¹

Type	Material	Installation	Total
Non-Condensing	\$767	\$900	\$1,667
Condensing	\$1,166	\$900	\$2,066

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¹ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

RESIDENTIAL/LOW INCOME – HEAT REFLECTOR PANELS – RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Residential/Low-Income → Space Heating → Heat Reflector Panels → Retrofit	

Table 1 provides a summary of the key measure parameters and savings values.

Table 1. Measure Key Data

Parameter	Definitions	
Measure category	Retrofit	
Baseline technology	No heat reflector panel installed behind radiator	
Efficient technology	Heat reflector panel installed behind radiator	
Market type	Residential/Low Income	
Annual natural gas savings per single family household (m ³)	<i>Efficient Technology</i>	<i>Savings</i>
	4.1% reduced gas consumption	143.2 m ³
Measure life	25 years	
Incremental cost	Utility to use actual per heat reflector panel cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.	
Restrictions	To qualify for this measure, heat reflector panels must be implemented in older single-family residential homes by direct install using certified contractors.	

OVERVIEW

Space heating represents a large share of the energy consumption in homes. For older hydronically (hot water) heated homes, one of the simplest ways to reduce space heating costs is to reduce the amount of heat being absorbed by surrounding walls. Installing heat reflector panels behind radiators can have a noticeable impact on a residence's space heating energy consumption. The savings that can be achieved are attractive since this measure is relatively inexpensive and easy to implement.

A heat reflector panel, attached to the wall behind radiators, reflects heat back into the room that would usually be absorbed by the wall. Also, the air trapped behind the radiator prevents conductive heat loss to the exterior.

APPLICATION

This measure pertains to the implementation of heat reflector panels in older (built before 1980) single-family residential homes that have hydronic heating through radiators served by boiler systems.

BASELINE TECHNOLOGY

The baseline technology is an older (built before 1980) single-family residential home with radiant heating and no heat reflector panels attached to the wall behind a radiator.

EFFICIENT TECHNOLOGY

The efficient technology is a saw tooth panel made of clear PVC with a reflective surface attached to the wall behind a radiator. [1]

ENERGY IMPACTS

The primary energy impact associated with implementation of heat reflector panels is a reduction in heat loss through the wall, thus resulting in a reduction in natural gas consumption. Table 1 in the “Overview” section provides annual savings values (m³ of natural gas) per single family home.

NATURAL GAS SAVINGS ALGORITHM

Results of Load Research Study

This algorithm outlines a methodology to determine the energy consumption as a function of the average boiler consumption of a single-family residence. It is based on a study conducted by Enbridge Gas Distribution Load Research Group in 2007 with the specific purpose of investigating the effects of heat reflector panels on residential heating consumption.

The study examined the gas consumption of boilers before and after the installation of heat reflector panels; the research details and study results were presented by Enbridge Gas Distribution in a 2008 report [2].

Automatic meter reading (AMR) equipment was installed at 31 randomly selected sample sites and boiler consumption was monitored for several weeks. Heat reflector panels were then installed by a panel manufacturer and monitoring of consumption continued. The daily consumption data collected was then separated into two groups: consumption before the installation of the heat reflector panel and consumption after the installation of the heat reflector panel.

Using the daily consumption data, the direction and magnitude of the impact of heat reflector panels was calculated by comparing the pre-installation period use-per-degree-day with the post-installation period use-per-degree-day for each site.

The study concluded that heat reflector panels, on average, reduced gas consumption by 4.1% within the sample. A 90% confidence interval was also computed for the average estimate (yielding a low value of 2.8% and a high value of 5.4%). The study provided 90% confidence that the true average would fall between the provided ranges when inferring from the sample to the population. The study results are summarized in Table 2:

Table 2. Summary of Results from EGD Load Research Group (2007) Study [2]

Number of Sites	31
Study Start Date	November 23, 2007
Study End Date	March 31, 2007
Average Change in Consumption	-4.1%
Standard Deviation of the Change	4.4%
90% Confidence Interval (High)	-5.4%
90% Confidence Interval (Low)	-2.8%

A previous Enbridge Gas Distribution Load Research study conducted in 2006 showed the average annual boiler consumption (with a 90% confidence interval) for a single-family residence to be 3,493 m³ [2]. Applying the average change in consumption resulting from the Heat Reflector Panel study to an average boiler consumption of 3,493 m³ resulted in an annual gas consumption savings value of 143.2 m³.

$$\begin{aligned}
 \text{Annual energy savings} & \left(\frac{\text{m}^3}{\text{year}} \right) \\
 & = \text{Average annual consumption} \left(\frac{\text{m}^3}{\text{year}} \right) \\
 & \times (\% \text{ average change in consumption due to heat reflector panels})
 \end{aligned}$$

ASSUMPTIONS

Table 3 provides a list of constants and assumption used in the derivation of the gas consumption savings values.

Table 3. Constants and Assumptions

Assumption	Value	Source
Average annual boiler consumption for an older single family residence (m ³)	3,493	[2]
Minimum space between radiator and the wall (inches)	0.25	[1]

SAVINGS CALCULATION EXAMPLE

The scenario for the gas savings is as follows. A heat reflector panel will be installed by certified contractors in a single-family residence which previously did not have any heat reflector panels.

Natural Gas Savings

Using the equation above for the installation of heat reflector panels compared to a residence not previously having any heat reflector panels,

$$\begin{aligned}
 \text{Annual energy savings} & \left(\frac{m^3}{\text{year}} \right) \\
 & = \text{Average annual consumption } m \left(\frac{m^3}{\text{year}} \right) \\
 & \times (\% \text{ average change in consumption due to heat reflector panels}) \\
 \text{Annual energy savings (} m^3/\text{yr)} & = 3,493 \times (4.1\%) \\
 \text{Annual energy savings} & = 143.2 \frac{m^3}{\text{yr}}
 \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure, heat reflector panels must be implemented in older single-family residential homes by direct install using certified contractors.

MEASURE LIFE

The measure life attributed to this measure is 25 years [3]

INCREMENTAL COST

The incremental cost for this measure could not be determined by looking at big-box retailer data. However, the previous substantiation sheet based the incremental cost on bulk purchases by the utility for program implementation. Since the incremental cost of the measure in the previous substantiation sheet is based on actual cost to the utility, it is the most accurate data. This method is consistent with other TRMs.

Table 4 presents the measure incremental cost.

Table 4. Measure Incremental Cost

Measure Category	Incremental Cost (\$)
All measure categories	Utility to use actual per heat reflector panel cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.

REFERENCES

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COMMERCIAL – AIR CURTAINS – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Air Curtains → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings.

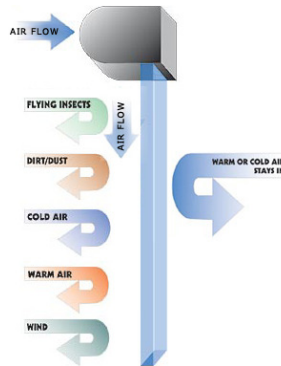
Table 1. Measure Key Data

Parameter	Definition								
Measure Category	New Construction (NC) Retrofit (R)								
Baseline Technology	No Air Curtain or Vestibule								
Efficient Technology	Air curtain that meets the minimum standards of the Air Movement and Control Association International, Inc. (AMCA)								
Market Type	Commercial								
Annual Natural Gas Savings (m ³)	Single Door			Double Door			Shipping and Receiving		
	7'x3'	7'x6'	8'x6'	2x7'x3'	2x7'x6'	2x8'x6'	8'x8'	8'x10'	10'x10'
	671	1,343	1,622	1,343	2,686	3,243	12,108	15,135	20,796
Annual Electric Penalty (kWh)	152	110	95	305	219	1,89	1,453	2,906	2,906
Measure Life	15 years								
Incremental Cost (\$ CAD)	Air Curtain Type			Approximate Cost					
	Single door	7' x 3'		\$1,429					
		7' x 6'		\$2,000					
		8' x 6'		\$2,143					
	Double door	2' x 7' x 3'		\$2,857					
		2' x 7' x 6'		\$4,000					
		2' x 8' x 6'		\$4,286					
	Shipping and receiving	8' x 8'		\$5,000					
		8' x 10'		\$5,000					
10' x 10'		\$6,429							
Restrictions	This measure is restricted to exterior doors without vestibules in buildings with natural gas heating								

OVERVIEW

Air Curtains are typically mounted above doorways and separate indoor and outdoor environments with a stream of air strategically engineered to strike the floor with a particular velocity and position. This air flow prevents outdoor air infiltration (heat, moisture, dust, fumes, insects), while also permitting an unobstructed entryway for pedestrians or goods. Figure 1 illustrates the schematic design for a typical air curtain installation.

Figure 1: Air Curtain Installation¹



The anticipated savings from this measure will be calculated for three types of door configurations: single door, double door, and shipping and receiving doors. Natural gas savings are calculated using an engineering algorithm and are reported in meters cubed (m³). Electric savings are calculated using an engineering algorithm and are reported in kilowatt hours (kWh).

APPLICATION

This measure provides incentives for installing air curtains in commercial facilities. The units serve to reduce the infiltration of outdoor air at the entrance points and reduce the heating and cooling requirements.

BASELINE TECHNOLOGY

There are no code standards that require air curtains in Ontario. This may change in the future² but the current baseline is a doorway without an air curtain, as shown in Table 2.

¹ Illustration downloaded from http://www.mitzvahengg.com/Non_Re_Circulating_Air_Curtains.htm on 10/14/2014.

² A code change proposal, CE192-13, toward the 2015 International Energy Conservation Code (IECC) was approved at the ICC (Group B) Committee Action Hearings in Dallas on April 27, 2013 and approved at the Final Action Hearings in Atlantic City in October 2013. [10] This standard provides an exception to the requirement for a vestibule if, "Doors that have an air curtain with a minimum velocity of 2 m/s at the floor, have been tested in accordance with ANSI/AMCA 220 and installed in accordance with manufacturer's instructions. Manual or automatic controls shall be provided that will operate the air curtain with the opening and closing of the door. Air curtains and their controls shall comply with Section C408.2.3." [1]

Table 2. Baseline Technology

Scenario	Requirement
All	Exterior doorway without vestibule or air curtain

EFFICIENT TECHNOLOGY

Air curtains that meet the requirements as shown in Table 3:

Table 3. Efficient Technology

Scenario	Requirement
All	Air Curtain that has been tested in accordance with ANSI/AMCA 220 [1]

ENERGY IMPACTS

The primary energy impact associated with the installation of air curtains is a reduction in natural gas usage or electricity resulting from reduced infiltration of cold air or hot air that needs to be heated or cooled when it enters a building. Table 1 provides annual savings coefficients, differentiated by door type.

There is an electric penalty associated with the addition of an air curtain due to the air curtain's fan. In air conditioned spaces, the overall electric penalty is reduced due to a reduced air-conditioning load. No water consumption impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Natural gas energy savings are achieved by determining the difference between heat lost at a doorway before and after the addition of an air curtain during the heating season.

$$\text{Annual NG Savings} = \frac{(q_{bc} - q_{ac})}{35.74 \text{ kBtu/m}^3} \times \text{HR} \times \frac{\text{day}_{hs}}{\text{Eff}}$$

where,

q_{bc} = Rate of transfer of sensible heat through open doorway (kBtu/hr)

q_{ac} = Rate of transfer of sensible heat through air curtain (kBtu/hr)

HR = Hour per day that door is open, see Table 4

day_{hs} = Heating days per year, see Table 4

Eff = Heating system efficiency, see Table 4

Heat Transfer at Doorway without Air Curtain for Heating Season:

$$q_{bc} = \frac{1.08 \text{ Btu}/(\text{hr} \cdot \text{F} \cdot \text{CFM}) \times Q_A \times (t_{ih} - t_{oh})}{1,000}$$

where,

1.08 = 60 min/hr × 0.239 Btu/ lb_m-F specific heat of air × 0.074 lbm/ft³ density of dry air (Btu/hr-F-CFM)

Q_A = Total air flow entering doorway (cfm)

t_{ih} = Inside temperature during heating season (°R), see Table 4

t_{oh} = Outside temperature during heating season (°R), see Table 4

Total air entering doorway is the combination of that caused by wind and thermal forces [2]:

$$Q_A = \sqrt{Q_w^2 + Q_t^2}$$

To determine the air entering doorway due to wind forces, the following equation is used [2]:

$$Q_w = V_h \times H \times W \times C_v \times 88 \text{ fpm}/\text{mph}$$

where,

Q_w = Air flow entering doorway due to wind forces (cfm)

V_h = Wind velocity during heating season (mph), see Table 4

H = Height of doorway (ft), see Table 4

W = Width of doorway (ft), see Table 4

C_v = Effectiveness of openings, see Table 4

Air entering doorway due to thermal forces can be calculated as [2]:

$$Q_t = 60 \text{ sec}/\text{min} \times H \times W \times C_{dh} \times \sqrt{2 \times g \times H/2 \times \left((t_{ih} - t_{oh})/t_{ih} \right)}$$

where,

Q_t = Air flow entering doorway due to thermal forces (cfm)

C_{dh} = Discharge coefficient for opening during heating season (C_{dh} is assumed to be 0.65 for unidirectional flow)

$$C_{dh} = 0.4 + 0.0025 \times (t_{ih} - t_{oh})$$

$$C_{dh} = 0.4 + 0.0025 \times (531.67 - 492.97) = 0.5$$

g = Constant acceleration due to gravity (ft/sec²), see Table 4

Heat Transfer at Doorway with Air Curtain for Heating Season:

Air curtain effectiveness [3]:

$$q_{ac} = q_{bc} \times (1 - E)$$

where,

E = Air curtain effectiveness (%), see Table 4

ELECTRIC SAVINGS ALGORITHMS

Electricity savings is achieved by determining the reduced air conditioning load during the summer season less the increased electricity use by the air curtain's fan.

$$\text{Electricity Savings } \left(\frac{kWh}{hr} \right) = \left(\frac{(q_{tbc} - q_{tac})}{SEER} - (HP \times 0.7457) \right) \times HR \times day_{cs}$$

where,

q_{tbc} = Rate of transfer of total heat through open doorway (kBtu/hr)

q_{tac} = Rate of transfer of total heat through air curtain (kBtu/hr)

SEER = Seasonal Energy efficiency ratio of cooling unit (kBtu/kWh), see Table 4

HP = Air curtain fan electric input power (hp), see Table 4

0.7457 = Unit conversion factor, brake horsepower to electric power (kW/hp)

HR = Hour per day that door is open, see Table 4

day_{cs} = Cooling days per year, see Table 4

Heat Transfer at Doorway without Air Curtain for Cooling Season:

Calculating air flow through the doorway during the cooling season is similar to calculating it for the heating season, but the formula is enthalpy-based instead of dry bulb temperature-based to account for humidity-related load.

Total heat transfer without air curtain:

$$q_{tbc} = \frac{4.5 \times Q_A \times (h_{oc} - h_{ic})}{1,000}$$

where,

4.5 = 60 min/hr \times 0.075 lb_m/ft³ density of dry air (lb-min/ft³-hr)

Q_A = Same formula as for heating

h_{oc} = Average enthalpy of outside air (Btu/lb)

h_{ic} = Average enthalpy of inside air (Btu/lb)

The values for average wind velocity and the inside and outside air temperatures to calculate Q_A differ as noted in Table 4. Also, C_d for cooling is derived per the following equation:

C_{dc} = Discharge coefficient for opening during cooling season

$$C_{dc} = 0.4 + 0.0025 \times (t_{ic} - t_{oc})$$

$$C_{dc} = 0.4 + 0.0025 \times (536.87 - 531.67) = 0.41$$

t_{ic} = Inside temperature during cooling season (°R), see Table 4

t_{oc} = Outside temperature during cooling season (°R), see Table 4

Heat transfer with the air curtain is as with heating:

$$q_{tac} = q_{tbc} \times (1 - E)$$

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithm to derive the stipulated savings values listed in Table 1 above.

Table 4. Assumptions

Variable	Definition	Scenario			Source/Comments		
		Single Door	Double Doors	Shipping and Receiving			
t_{ih}	Space temperature setpoint	72°F (22.2°C) (531.67°R)			Common assumptions table		
t_{oh}	OA temperature heating system enabled	33.3°F (0.7°C) (492.97°R)			Common assumptions table		
t_{ic}	Space temperature setpoint	72°F (22.2°C) (531.67°R)			Common assumptions table, room setpoint		
t_{oc}	OA temperature cooling system enabled	77.2°F (25.1°C) (536.87°R)			Common assumptions table		
h_{ic}	Inside enthalpy for cooling season	22.7 Btu/lb			Common assumptions table		
h_{oc}	Outside enthalpy for cooling season	27.4 Btu/lb			Common assumptions table		
HR	Hour per day door is open	1	5.6		[4] [5] ^{3,4}		
HP	Air curtain horsepower	1	2	8x8	8x10	10x10	[6] ⁵
				1.5	3	3	

³ Based on an average of warehouse, retail, and grocery store door opening 35% of the way estimated at 5 seconds per opening and approximately 2,000 openings per day. Baseline data approximated from cited reference.

⁴ Based on an average of grocery and retail space openings at 5.6 deliveries per day at 60 minutes per delivery. Baseline data approximated from cited reference.

⁵ Assumes motor efficiency and load factor are the same, so that nameplate rated output brake horsepower and running input electric power are the same.

Variable	Definition	Scenario			Source/Comments
		Single Door	Double Doors	Shipping and Receiving	
V_h	Average wind velocity for heating season	2.2 mph (3.5 kph)			[7] - Calculated using the wind profile law for the center of the doorway reduced by 25% due to diagonal wind
V_c	Average wind velocity for cooling season	1.8 mph (2.9 kph)			[7] – Calculated using the wind profile law for the center of the doorway reduced by 25% due to diagonal wind
C_{dh}	Discharge coefficient for opening during heating season	0.5			[2]
C_{dc}	Discharge coefficient for opening during cooling season	0.41			[2]
C_v	Effectiveness of openings	0.3			[2] - Assume diagonal wind ⁶
E	Effectiveness of air curtain	70% (Range between 60% - 80%)			[3]
Eff	Commercial heating system efficiency	80%			Common assumptions table
SEER	Commercial Seasonal cooling system efficiency	13 kBtu/kWh			Common assumptions table
g	Acceleration due to gravity	32.2 ft/sec ² (9.8 mps)			Common assumptions table
	Conversion from mph to fpm	88 fpm/mph			Common assumptions table
	Energy density of natural gas	35,738 Btu/m ³			Common assumptions table
	Conversion from HP to kWh	0.7457 kW/HP			Common assumptions table
day_{hs}	Heating days per year	232			Common assumptions table
day_{cs}	Cooling days per year	30		0	Common assumptions table

The analysis assumes that the air curtain fan is only on during the heating season for uncooled spaces.

⁶ The flow through the inlet will depend on orientation of the doorway; the flow is maximized when the inlet is directly facing the prevailing wind. Wind blowing perpendicularly, directly into a door will result in a C_v of 0.5 to 0.6. Wind blowing diagonally into it will result in a C_v of 0.25 to 0.35. Wind blowing across a doorway will result in lesser C_v due to entrainment, as will the negative pressure on a doorway on the leeward side of a building.

SAVINGS CALCULATION EXAMPLE

The example below illustrates the annual natural gas savings value for a retail space with a single door (6'x8') entrance.

Air flow rate Q_A from wind and thermal forces before air curtain

$$= \sqrt{(V_h \times H \times W \times C_v \times 88)^2 + (60 \times H \times W \times C_{dh} \times \sqrt{2 \times g \times H/2} \times ((t_{ih} - t_{oh})/t_{ih}))^2}$$

$$= \sqrt{(2.2 \times 8 \times 6 \times 0.3 \times 88)^2 + \left(60 \times 8 \times 6 \times 0.5 \times \sqrt{2 \times 32.2 \times (8/2)} \times \left(\frac{531.67 - 492.97}{531.67}\right)\right)^2}$$

$$Q_A = 6,830 \text{ cfm}$$

$$\text{Heat loss before air curtain} = q_{bc} = \frac{1.08 \times Q_A \times (t_{ih} - t_{oh})}{1,000}$$

$$= \frac{1.08 \times 6,830 \times (72 - 33.3)}{1,000} = 285 \text{ kBtu/hr}$$

$$q_{ac} = q_{bc} \times (1 - E) = 285 \times (1 - 0.7) = 86 \text{ kBtu/hr}$$

$$\text{Annual NG Savings} = \frac{(q_{bc} - q_{ac})}{35.74} \times \text{HR} \times \frac{\text{day}_{hs}}{\text{Eff}} = \frac{(285 - 86)}{35.74} \times 1 \times \frac{232}{0.80} = 1,622 \text{ m}^3$$

It will also have a negative electric savings due to fan operation:

$$\text{Annual Electric Impact, Heating Season} = -HP \times 0.7457 \times \text{HR} \times \text{day}_{hs}$$

$$= 1 \times 0.7457 \times 1 \times 232 = -173 \text{ kWh}$$

During the cooling season the air curtain will reduce the load on the retail space's HVAC system, saving electricity, which will be partially offset by the air curtain fan operation at the same time.

$$Q_A$$

$$= \sqrt{(1.8 \times 8 \times 6 \times 0.3 \times 88)^2 + \left(60 \times 8 \times 6 \times 0.41 \times \sqrt{2 \times 32.2 \times (8/2)} \times \left(\frac{536.87 - 531.67}{536.87}\right)\right)^2}$$

$$Q_A = 2,946 \text{ cfm}$$

$$q_{tbc} = \frac{4.5 \times Q_A \times (h_{oc} - h_{ic})}{1,000} = \frac{4.5 \times 2,918 \times (27.4 - 22.7)}{1,000} = 62.3 \text{ kBtu/hr}$$

$$q_{tac} = 62.3 \times (1 - 0.7)$$

$$q_{tac} = 18.7 \text{ kBtu/hr}$$

Annual Electric Impact, Cooling Season

$$= \left(\frac{(q_{tbc} - q_{tac})}{EER} - (HP \times 0.7457) \right) \times HR \times day_{cs}$$

$$= \left(\frac{(62.3 - 18.7)}{13} - (1 \times 0.7457) \right) \times 1 \times 30 = 78 \text{ kWh}$$

The net annual electricity loss is -95 kWh/yr.

USES AND EXCLUSIONS

This measure is restricted to exterior doors without vestibules in buildings with natural gas heating.

MEASURE LIFE

The measure life is 15 years [8].

INCREMENTAL COST

The purchase and installation cost for air curtains is summarized in the table below. [9]

Table 5. Incremental Cost ⁷

Air Curtain Type		Approximate Cost
Single door	3' x 7'	\$1,429
	6' x 7'	\$2,000
	6' x 8'	\$2,143
Double door	2 x 7' x 3'	\$2,857
	2 x 7' x 6'	\$4,000
	2 x 6' x 8'	\$4,286
Shipping and receiving	8' x 8'	\$5,000
	8' x 10'	\$5,000
	10' x 10'	\$6,429

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⁷ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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COMMERCIAL – PEDESTRIAN AIR CURTAINS WITH VESTIBULE – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	December 22, 2017
OEB Approval Date	
Commercial → Space Heating → Air Curtains → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definition					
Measure Category	New Construction (NC) Retrofit (R)					
Baseline Technology	No Air Curtain					
Efficient Technology	Ambient or heated air curtain that meets the minimum standards such the Air Movement and Control Association International, Inc. (AMCA), ISO 27327, or any similar standard.					
Market Type	Commercial					
Application	Pedestrian Single Door With Vestibule			Pedestrian Double Door With Vestibule		
Size	7'x3'	7'x6'	8'x6'	2x 7'x3'	2x 7'x6'	2x 8'x6'
Annual Natural Gas Savings (m ³) – heating season	454	909	1,097	909	1,817	2,194
Annual Electrical Penalty due to the operation of Air Curtain Fan (kWh)- heating season	173	173	173	346	346	346
Annual Electric Penalty due to Heated Air Curtain (kWh)- heating season	2,320	4,408	4,408	4,408	8,816	8,816
Net Annual Electric Savings (kWh) – cooling season	6.4	35	45	13	70	90
Measure Life	15 years					
Incremental Cost (ambient air curtain) (\$ CAD)	\$1,351	\$1,892	\$2,027	\$2,703	\$3,784	\$4,054

Parameter	Definition					
Incremental Cost (heated air curtain) (\$ CAD)	\$2,027	\$2,297	\$2,432	\$4,054	\$4,594	\$4,864
Restrictions	This measure is restricted to air door applications on exterior doors that are installed in buildings that are comfort heated to an air temperature of 72 F with Natural Gas fueled pressure balanced HVAC (heated mechanical ventilation) systems capable of maintaining indoor air temperature during normal operation of exterior doors.					

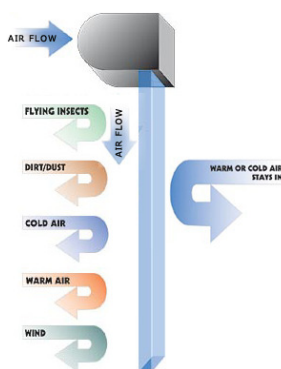
OVERVIEW

Air curtains are typically mounted above doorways and separate indoor and outdoor environments with a stream of air strategically engineered to strike the floor with a particular velocity and position. This air flow prevents outdoor air infiltration (heat, moisture, dust, fumes, insects), while also permitting an unobstructed entryway for pedestrians or goods.

In addition, air curtains may be sold with integrated electrical heaters which warm the cold air as it flows through the unit. For these air curtains, there is a pre-wired heater control box with a wall mounted thermostat to maintain a warm air stream.

Figure 1 illustrates the schematic design for a typical air curtain installation.

Figure 1: Air Curtain Installation¹



The anticipated savings from this measure will be calculated for two types of door configurations: single pedestrian door with vestibule and double pedestrian door with vestibule. In addition, an electric penalty for the addition of a heated air curtain will be calculated for each of the pedestrian door scenarios. For the purposes of this document, a vestibule is assumed to be a pre-existing enclosed space on the interior of an exterior door that is not designed to be heated, or temperature controlled by the remainder of the building heating system. This can include a space enclosed by two sets of doors, or a designated area with no heating or its own separate heating system that might include localized radiant heating.

¹ Illustration downloaded from http://www.mitzvahengg.com/Non_Re_Circulating_Air_Curtains.htm on 10/14/2014.

Natural gas savings are calculated using an engineering algorithm and are reported in meters cubed (m³). Electric savings are calculated using an engineering algorithm and are reported in kilowatt hours (kWh).

APPLICATION

This measure provides incentives for installing air curtains in commercial facilities. The units serve to reduce the infiltration of outdoor air at the entrance points and reduce the heating and cooling requirements.

BASELINE TECHNOLOGY

There are no code standards that currently require air curtains in Ontario². The current baseline is a doorway without an air curtain, as shown in Table 2.

Table 2. Baseline Technology

Scenario	Requirement
All	Exterior doorway without air curtain

EFFICIENT TECHNOLOGY

Air curtains that meet the requirements as shown in Table 3:

Table 3. Efficient Technology

Scenario	Requirement
All	Air Curtain that has been tested in accordance with ANSI/AMCA 220 [1], ISO 27327, or any similar standard.

ENERGY IMPACTS

The primary energy impact associated with the installation of air curtains is a reduction in natural gas usage or electricity resulting from reduced infiltration of cold air or hot air that needs to be heated or cooled when it enters a building.

² A code change proposal, CE192-13, toward the 2015 International Energy Conservation Code (IECC) was approved at the ICC (Group B) Committee Action Hearings in Dallas on April 27, 2013 and approved at the Final Action Hearings in Atlantic City in October 2013. [13] This standard provides an exception to the requirement for a vestibule if, "Doors that have an air curtain with a minimum velocity of 2 m/s at the floor, have been tested in accordance with ANSI/AMCA 220 and installed in accordance with manufacturer's instructions. Manual or automatic controls shall be provided that will operate the air curtain with the opening and closing of the door. Air curtains and their controls shall comply with Section C408.2.3." [1]

In doorways with existing vestibules, the infiltration of cold or hot air has already been reduced. The resulting savings from the addition of an air curtain is in turn reduced when compared with doors without existing vestibules. Table 1 provides annual savings coefficients, differentiated by door type.

There is an electric penalty associated with the addition of an air curtain due to the air curtain’s fan. In air conditioned spaces, the overall electric penalty is reduced due to a reduced air-conditioning load. In addition, there is an electric penalty associated with the addition of a heated air curtain. No water consumption impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Natural gas energy savings are achieved by determining the difference between the heat lost at a doorway before and after the addition of an air curtain during the heating season.

Heat Transfer at Doorway without Air Curtain or Vestibule for Heating Season:

$$q_{bc} = \frac{1.08 \frac{Btu}{hr \cdot ^\circ F \cdot CFM} \times Q_{A,heating} \times (t_{ih} - t_{oh})}{1,000}$$

where,

q_{bc} = Heat transfer through a doorway without air curtain or vestibule during the heating season, (kBtu/hr)

1.08 = 60 min/hr x 0.240 Btu/ lb_m- °F specific heat of air x 0.075 lb_m/ft³ density of dry air (Btu/hr-°F-CFM)

$Q_{A,heating}$ = Total air flow entering doorway (cfm), during the heating season

t_{ih} = Inside temperature during heating season (°F), see Table 4

t_{oh} = Outside temperature during heating season (°F), see Table 4

Total air entering doorway is the combination of that caused by wind and thermal forces [2]:

$$Q_{A,heating} = \sqrt{Q_{wh}^2 + Q_{th}^2}$$

To determine the air entering doorway due to wind forces, the following equation is used [2]:

$$Q_{wh} = V_h \times H \times W \times C_v \times 88 \text{ fpm}/\text{mph}$$

where,

Q_{wh} = Air flow entering doorway due to wind forces during heating season (cfm)

V_h = Wind velocity during heating season (mph), see Table 4

H = Height of doorway (ft), see Table 4

W = Width of doorway (ft), see Table 4

C_v = Effectiveness of openings, see Table 4

88 *fpm/mph*= conversion factor

Air entering doorway due to thermal forces can be calculated as [2]:

$$Q_{th} = 60 \text{ sec/min} \times H \times W \times C_{dh} \times \sqrt{2 \times g \times H/2 \times \left(\frac{t_{ih} - t_{oh}}{t_{ih}} \right)}$$

where,

Q_{th} = Air flow entering doorway due to thermal forces during the heating season (cfm)

C_{dh} = Discharge coefficient for opening during heating season

$$C_{dh} = 0.4 + 0.0025 \times (t_{ih} - t_{oh})$$

$$C_{dh} = 0.4 + 0.0025 \times (531.67 - 492.7) = 0.5$$

g = Constant acceleration due to gravity (ft/sec²), see Table 4

t_{ih} = Inside temperature during heating season (°R), see Table 4

t_{oh} = Outside temperature during heating season (°R), see Table 4

For a doorway with a vestibule

For a doorway with a vestibule, the baseline heat loss through the entryway must be discounted to account for the vestibule's effectiveness.

$$\text{Annual NG Savings} = \frac{(q_{bcv} - q_{acv})}{35.74 \text{ kBtu/m}^3} \times \text{HR} \times \frac{\text{day}_{hs}}{\frac{\text{Eff}}{100\%}}$$

where,

Annual NG Savings = Natural gas savings from air curtain (m³)

q_{bcv} = Rate of transfer of sensible heat through doorway with vestibule (kBtu/hr)

q_{acv} = Rate of transfer of sensible heat through doorway with added air curtain (kBtu/hr)

HR = Hour per day that door is open, see Table 4 (hr/day)

day_{hs} = Heating days per year, see Table 4 (day/year)

Eff = Heating system efficiency, see Table 4 (%)

Accounting for vestibule effectiveness [3] [4]:

$$q_{bcv} = q_{bc} \times \left(1 - \frac{VE}{100\%} \right)$$

where,

VE = Vestibule effectiveness (%), see Table 4

Accounting for the addition of the air curtain [5]:

$$q_{acv} = q_{bcv} \times \left(1 - \frac{E}{100\%}\right)$$

where,

E = Air curtain effectiveness (%), see Table 4

Electric Impact for Heating Season:

There will be an electric penalty during the heating season due to operation of the fan on the air curtain.

$$\text{Annual Electric Impact, Heating Season (kWh/yr)} = -HP \times 0.7457 \times HR \times day_{hs}$$

where,

HP = Air curtain fan electric input power (hp), see Table 4

0.7457 = Unit conversion factor, brake horsepower to electric power (kW/hp)

HR = Hours per day that door is open, see Table 4 (hr/day)

day_{hs} = Heating days per year, see Table 4 (day/year)

Electric Impact for Heating Season with Heated Air Curtain:

In the case where an electrically heated air curtain is installed, there will be an electric penalty during the heating season due to operation of the heater on the air curtain.

$$\text{Annual Electric Heater Impact, Heating Season (kWh/yr)} = -kW \times HR \times day_{hs}$$

where,

kW = Electric heating power

ELECTRIC SAVINGS ALGORITHMS

Electricity savings is achieved by determining the reduced air conditioning load during the cooling season less the increased electricity use by the air curtain's fan during the cooling season.

Heat Transfer at Doorway without Air Curtain or Vestibule for Cooling Season:

Calculating air flow through the doorway during the cooling season is similar to calculating it for the heating season, but the formula is enthalpy-based instead of dry bulb temperature-based to account for humidity-related load.

$$q_{tbc} = \frac{4.5 \times Q_{A,cooling} \times (h_{oc} - h_{ic})}{1,000}$$

where,

q_{tbc} = Heat transfer through doorway without air curtain or vestibule during cooling season, (kBtu/hr)

4.5 = 60 min/hr × 0.075 lb_m/ft³ density of dry air (lb-min/ft³-hr)

$Q_{A,cooling}$ = Total air flow entering doorway during cooling season (cfm)

h_{oc} = Average enthalpy of outside air (Btu/lb), see Table 4

h_{ic} = Average enthalpy of inside air (Btu/lb), see Table 4

Total air entering doorway is the combination of that caused by wind and thermal forces:

$$Q_{A,cooling} = \sqrt{Q_{wc}^2 + Q_{tc}^2}$$

To determine the air entering doorway due to wind forces, the following equation is used:

$$Q_{wc} = V_c \times H \times W \times C_v \times 88 \text{ fpm/mph}$$

where,

Q_{wc} = Air flow entering doorway due to wind forces during cooling season (cfm)

V_c = Wind velocity during cooling season (mph), see Table 4

H = Height of doorway (ft), see Table 4

W = Width of doorway (ft), see Table 4

C_v = Effectiveness of openings, see Table 4

88 fpm/mph = conversion factor

Air entering doorway due to thermal forces can be calculated as:

$$Q_{tc} = 60 \text{ sec/min} \times H \times W \times C_{dc} \times \sqrt{2 \times g \times H/2 \times \left(\frac{t_{oc} - t_{ic}}{t_{oc}} \right)}$$

where,

Q_{tc} = Air flow entering doorway due to thermal forces during cooling season (cfm)

C_{dc} = Discharge coefficient for opening during cooling season

$$C_{dc} = 0.4 + 0.0025 \times (t_{oc} - t_{ic})$$

$$C_{dc} = 0.4 + 0.0025 \times (536.87 - 531.67) = 0.41$$

- g = Constant acceleration due to gravity (ft/sec²), see Table 4
 t_{ic} = Inside temperature during cooling season (°R), see Table 4
 t_{oc} = Outside temperature during cooling season (°R), see Table 4

For a doorway with a vestibule

For a doorway with a vestibule, the baseline heat loss through the entryway must be discounted to account for the vestibule’s effectiveness.

$$Electricity\ Savings = \left(\frac{(q_{tbcv} - q_{tacv})}{EER} - (HP \times 0.7457) \right) \times HR \times day_{cs}$$

where,

- $Electricity\ Savings$ = Electric savings from air curtain (kWh/yr)
 q_{tbcv} = Rate of transfer of total heat through doorway with vestibule (kBtu/hr)
 q_{tacv} = Rate of transfer of total heat through doorway with added air curtain (kBtu/hr)
 EER = Energy efficiency ratio of cooling unit (kBtu/kWh), see Table 4
 HP = Air curtain fan electric input power (hp), see Table 4
 0.7457 = Unit conversion factor, brake horsepower to electric power (kW/hp)
 HR = Hour per day that door is open, see Table 4 (hr/day)
 day_{cs} = Cooling days per year, see Table 4 (day/yr)

Accounting for vestibule effectiveness [3] [4]:

$$q_{tbcv} = q_{tbc} \times \left(1 - \frac{VE}{100\%} \right)$$

where,

- VE = Vestibule effectiveness (%), see Table 4

Accounting for the addition of the air curtain [5]:

$$q_{tacv} = q_{tbcv} \times \left(1 - \frac{E}{100\%} \right)$$

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithm to derive the stipulated savings values listed in Table 1 above.

Table 4. Assumptions

Variable	Definition	Scenario				Source/Comments
		Single Door		Double Doors		
t_{ih}	Space temperature setpoint	72°F (22.2°C) (531.67°R)				Common assumptions table
t_{oh}	OA temperature heating system enabled	33.03°F (0.6°C) (492.7°R)				Common assumptions table
t_{ic}	Space temperature setpoint	72°F (22.2°C) (531.67°R)				Common assumptions table, room setpoint
t_{oc}	OA temperature cooling system enabled	77.2°F (25.1°C) (536.87°R)				Common assumptions table
h_{ic}	Inside enthalpy for cooling season	22.7 Btu/lb				Common assumptions table
h_{oc}	Outside enthalpy for cooling season	27.4 Btu/lb				Common assumptions table
HR	Hour per day door is open	1				[4] [6] ^{3,4}
HP	Air curtain horsepower	1		2		[7] ⁵
kW	Electric heating power	3'	6'	6'	12'	[8] [9]
		10	19	19	38	
V_h	Average wind velocity for heating season	2.2 mph (3.5 kph)				[10] - Calculated using the wind profile law for the center of the doorway reduced by 25% due to diagonal wind
V_c	Average wind velocity for cooling season	1.8 mph (2.9 kph)				[10] – Calculated using the wind profile law for the center of the doorway reduced by 25% due to diagonal wind
C_{dh}	Discharge coefficient for opening during heating season	0.5				[2]
C_{dc}	Discharge coefficient for opening during cooling season	0.41				[2]

³ Based on an average of warehouse, retail, and grocery store door opening 35% of the way estimated at 5 seconds per opening and approximately 2,000 openings per day. Baseline data approximated from cited reference.

⁴ Based on an average of grocery and retail space openings at 5.6 deliveries per day at 60 minutes per delivery. Baseline data approximated from cited reference.

⁵ Assumes motor efficiency and load factor are the same, so that nameplate rated output brake horsepower and running input electric power are the same.

Variable	Definition	Scenario						Source/Comments
		Single Door			Double Doors			
C_v	Effectiveness of openings	0.3						[2] - Assume diagonal wind ⁶
E	Effectiveness of air curtain without vestibule	70% (Range between 60% - 80%)						[5]
VE	Effectiveness of vestibule	33%						[4] [3]
Eff	Commercial heating system efficiency	80%						Common assumptions table
EER	Commercial cooling system efficiency	13 kBtu/kWh						Common assumptions table
g	Acceleration due to gravity	32.2 ft/sec ² (9.8 mps)						Common assumptions table
	Conversion from mph to fpm	88 fpm/mph						Conversion factor
	Energy density of natural gas	35,738 Btu/m ³						Common assumptions table
	Conversion from HP to kWh	0.7457 kW/HP						Common assumptions table
day_{hs}	Heating days per year	232						Common assumptions table
day_{cs}	Cooling days per year	30						Analysis of TMY3 data for London, ON
	Door Type	Single Pedestrian			Double Door Pedestrian			
H	Height of doorway (ft)	7	7	8	7	7	8	
W	Width of doorway (ft)	3	6	6	6	12	12	

It is assumed that the air curtain will be turned off during the cooling season if the air curtain is installed in a space which lacks air conditioning. For these cases, there will be no electric impact during the cooling season.

⁶ The flow through the inlet will depend on orientation of the doorway; the flow is maximized when the inlet is directly facing the prevailing wind. Wind blowing perpendicularly, directly into a door will result in a C_v of 0.5 to 0.6. Wind blowing diagonally into it will result in a C_v of 0.25 to 0.35. Wind blowing across a doorway will result in lesser C_v due to entrainment, as will the negative pressure on a doorway on the leeward side of a building.

SAVINGS CALCULATION EXAMPLE

The example below illustrates the annual natural gas savings and electric savings for a retail space with a double door (2 x 8'x6') entrance with a vestibule which has installed a heated air curtain.

Heating Season:

Air flow rate $Q_{A,heating}$ from wind and thermal forces before air curtain

$$\begin{aligned}
 &= \sqrt{(V_h \times H \times W \times C_v \times 88)^2 + (60 \times H \times W \times C_{dh} \times \sqrt{2 \times g \times H/2} \times ((t_{ih} - t_{oh})/t_{ih}))^2} \\
 &= \sqrt{(2.2 \times 2 \times 8 \times 6 \times 0.3 \times 88)^2 + \left(60 \times 2 \times 8 \times 6 \times 0.5 \times \sqrt{2 \times 32.2 \times (8/2)} \times \left(\frac{531.67 - 492.7}{531.67}\right)\right)^2} \\
 & \qquad \qquad \qquad Q_{A,heating} = 13,700 \text{ cfm}
 \end{aligned}$$

Heat loss, q_{bc} , before air curtain or vestibule

$$\begin{aligned}
 &= \frac{1.08 \times Q_{A,heating} \times (t_{ih} - t_{oh})}{1,000} \\
 &= \frac{1.08 \times 13,700 \times (72 - 33.03)}{1,000} \\
 & \qquad \qquad \qquad q_{bc} = 576.6 \text{ kBtu/hr}
 \end{aligned}$$

Accounting for the vestibule effectiveness:

$$q_{bcv} = q_{bc} \times (1 - VE) = 576.6 \times (1 - 0.33) = 386.3 \text{ kBtu/hr}$$

Accounting for the addition of the air curtain:

$$q_{acv} = q_{bcv} \times (1 - E) = 386.3 \times (1 - 0.7) = 115.9 \text{ kBtu/hr}$$

Calculation of annual natural gas savings:

$$\begin{aligned}
 \text{Annual NG Savings} &= \frac{(q_{bcv} - q_{acv})}{35.74} \times \text{HR} \times \frac{\text{day}_{hs}}{\text{Eff}} = \frac{(386.3 - 115.9)}{35.74} \times 1 \times \frac{232}{0.80} \\
 &= 2,194 \text{ m}^3
 \end{aligned}$$

There will also be an electric penalty due to fan operation:

$$\text{Annual Electric Impact, Heating Season} = \text{HP} \times 0.7457 \times \text{HR} \times \text{day}_{hs}$$

$$= 2 \times 0.7457 \times 1 \times 232 = 346 \text{ kWh}$$

There will also be an electric penalty associated with the heater on the air curtain:

$$\begin{aligned} \text{Annual Electric Heater Impact, Heating Season} &= \text{kW} \times \text{HR} \times \text{day}_{hs} \\ &= 38 \times 1 \frac{\text{hr}}{\text{day}} \times \frac{232 \text{ days}}{\text{year}} = 8,816 \text{ kWh} \end{aligned}$$

Cooling Season:

During the cooling season the air curtain will reduce the load on the retail space's HVAC system, saving electricity, which will be partially offset by the air curtain fan operation at the same time.

$$\begin{aligned} Q_{A,cooling} &= \sqrt{(1.8 \times 2 \times 8 \times 6 \times 0.3 \times 88)^2 + \left(60 \times 2 \times 8 \times 6 \times 0.41 \times \sqrt{2 \times 32.2 \times (8/2) \times \left(\frac{536.87 - 531.67}{536.87}\right)}\right)^2} \\ Q_A &= 5,893 \text{ cfm} \end{aligned}$$

Heat loss, q_{tbc} , before air curtain or vestibule

$$q_{tbc} = \frac{4.5 \times Q_A \times (h_{oc} - h_{ic})}{1,000} = \frac{4.5 \times 5,893 \times (27.4 - 22.7)}{1,000} = 125 \text{ kBtu/hr}$$

Accounting for the vestibule effectiveness:

$$q_{tbcv} = q_{tbc} \times (1 - VE) = 125 \times (1 - 0.33) = 84 \text{ kBtu/hr}$$

Accounting for the addition of the air curtain:

$$q_{tacv} = q_{tbcv} \times (1 - E) = 84 \times (1 - 0.7) = 25 \text{ kBtu/hr}$$

Calculation of electric savings:

$$\begin{aligned} \text{Electricity Savings, Cooling Season} &= \left(\frac{(q_{tbcv} - q_{tacv})}{EER} - (HP \times 0.7457) \right) \times \text{HR} \times \text{day}_{cs} \\ &= \left(\frac{(84 - 25)}{13} - (2 \times 0.7457) \right) \times 1 \times 30 = 90 \text{ kWh} \end{aligned}$$

Therefore,

$$\text{Annual NG Savings} = 2,194 \text{ m}^3$$

$$\text{Annual Electric Savings} = -(346 + 8,816) + 90 = -9,072 \text{ kWh}$$

USES AND EXCLUSIONS

This measure is restricted to exterior pedestrian doors with a vestibule in buildings with natural gas heating.

MEASURE LIFE

The measure life is 15 years [11].

AIR CURTAIN COST

The purchase and installation cost for air curtains is summarized in the table below⁷. [12]

Table 5. Incremental Cost ⁸

Air Curtain Type		Approximate Cost Ambient Air Curtain	Approximate Cost Heated Air Curtain
Single door	7' x 3'	\$1,351	\$2,027
	7' x 6'	\$1,892	\$2,297
	8' x 6'	\$2,027	\$2,432
Double door	2 x 7' x 3'	\$2,703	\$4,054
	2 x 7' x 6'	\$3,784	\$4,594
	2 x 8' x 6'	\$4,054	\$4,864

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⁷ Costs include the full purchase and installation of an air curtain where none previously existed.

⁸ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 11/26/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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COMMERCIAL – CONDENSING MAKE-UP AIR UNIT – NEW CONSTRUCTION/ TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Condensing Make-Up Air Unit (MUA) → New Construction/Time of Natural Replacement	

Table 1 below provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definitions		
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)		
Baseline Technology	80% Thermal Efficiency Conventional Make-Up Air Unit		
Efficient Technology	≥ 90% Thermal Efficiency, Condensing Make-Up Air Unit		
Market Type	Commercial		
Annual Natural Gas Savings Rate (m ³ /CFM)	Condensing MUA Type	Commercial	Multi-Residential and Long Term Care
	Constant Speed	0.407	0.919
	2 Speed	1.22	2.45
	VFD	2.03	3.00
Annual Electric Savings Rate (kWh/CFM)	Constant Speed	0	0
	2 Speed	1.24	1.61
	VFD	2.04	2.30
Measure Life	20 Years		
Incremental Cost (\$ CAD)	Constant Speed	2 Speed	VFD
	\$870+\$0.66/CFM	\$870+\$1.01/CFM	\$870+\$1.02/CFM

Parameter	Definitions
Restrictions	Only condensing make-up air units installed in commercial, multi residential or long term care facilities are eligible for the incentive. Applies to air flows from 1,500 CFM up to 14,000 CFM. Systems with Demand Control Ventilation will not qualify. Retail is not eligible for this measure. Savings factors are based on base case unit delivering the total fresh air flow from the MUA unit during operation. Air Handling Units (AHU) with return, reheat and cooling are not eligible.

OVERVIEW

The measure is for the installation of natural gas condensing make-up air (MUA) units with a thermal efficiency of 90% or higher in commercial buildings. Similar to condensing furnaces, high efficiency make-up air units achieve savings through the utilization of a sealed, super insulated combustion chamber, more efficient burners, and multiple heat exchangers that remove a significant portion of the waste heat from the flue gasses. Because multiple heat exchangers are used to remove waste heat from the escaping flue gas, most of the vapor in the flue gas condenses and must be drained.

The measure also covers 2 speed and variable speed equipped models. MUAs with the ability to modulate incoming outside air during periods of reduced occupation reduce fuel consumption by reducing load on the equipment.

APPLICATION

The measure is for the installation of condensing make-up air units which have efficiencies that are higher than code requires. Commercial make-up air units are performance rated by their thermal efficiency (TE). This is a measure of the operating efficiency of the make-up air unit and is defined as the energy out, or the energy transferred to the hot air, divided by the energy in, or the energy contained within the fuel.

BASELINE TECHNOLOGY

Canada’s Energy Efficiency Regulations require that new commercial ($\geq 225,000$ Btu/hr) hot air heating equipment have a rated thermal efficiency (TE) of at least an 80% [1]. For NC/TNR installations, the baseline technology is considered to be the minimum efficiency required by the regulations effective January 1, 2014.

Table 2. Baseline Technology

Type	Thermal Efficiency
Gas Make-Up Air Unit	80%

EFFICIENT TECHNOLOGY

The efficient technology is a condensing make-up air unit with a thermal efficiency rating equal to, or higher than 90%. This is typically the minimum efficiency available for a condensing make-up air unit [2] [3].

Table 3. Efficient Technology

Type	Thermal Efficiency
Gas Condensing Make-Up Air Unit	≥ 90%

ENERGY IMPACTS

The primary energy impact associated with the installation of condensing make-up air unit in this service territory is a reduction in natural gas usage resulting from the unit’s improved efficiency.

There are electrical savings impacts associated with the measure when the unit installed is equipment with two speed or variable speed capability. These options also lead to additional savings from reducing the outside air during heating and cooling seasons.

No water consumption impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

The measure natural gas savings are calculated using an assumed load profile for each type of equipment, typical meteorological year 2 (TMY) data for London, Ontario [4], and the difference in assumed efficiencies for the equipment. The assumed load profiles were developed by Agviro Inc. [5] and are shown in Table 5 in the “Assumptions” section. The binned weather data is shown in Table 6.

The natural gas savings factor attributed to this measure is calculated using the following formulas:

$$Heat\ Load\ Rate = \sum_{5^{\circ}}^{T_o} 1.08 \frac{Btu}{hr\ ^{\circ}F\ CFM} \times bin \times (T_s - T_o)$$

And,

$$NG \text{ Savings Factor} = \frac{\text{Heat Load Rate}}{35,738 \frac{\text{Btu}}{\text{m}^3}} \times \left(\frac{V_{Base}}{TE_{base}} - \frac{V_{EE}}{TE_{EE}} \right)$$

where,

<i>Heat Load Rate</i>	= Annual heating load per CFM of MUA rated air flow capacity assuming no modulation (Btu/yr/CFM)
1.08	= 60 min/hr × 0.239 Btu/ lb _m -F specific heat of air × 0.074 lb _m /ft ³ density of dry air (Btu/hr-F-CFM)
<i>bin</i>	= Annual hours in each five degree temperature bin ¹ (hr/yr), see Table 6 (use appropriate column for appropriate building type)
<i>T_s</i>	= Supply air temperature set point (°F)
<i>T_o</i>	= Outside air temperatures (°F)
<i>NG Savings Factor</i>	= Annual gas savings factor resulting from installing the new condensing MUA (m ³ /yr)/CFM
<i>V_{Base}</i>	= Baseline fan motor speed (%)
<i>V_{EE}</i>	= Energy efficient fan motor speed (%)
$35,738 \frac{\text{Btu}}{\text{m}^3}$	= Conversion of rated heating capacity from Btu/hr to m ³ /hr, common assumptions table
<i>TE_{base}</i>	= Baseline equipment thermal efficiency (%)
<i>TE_{EE}</i>	= Efficient equipment thermal efficiency (%)

ELECTRIC SAVINGS ALGORITHM

Electric energy savings are achieved if the MUA are equipped with 2 stage or VFD fan motor controls. The savings factors in Table 1 are averaged across all fan sizes from Table 7.

The electric savings from reducing the speed of a motor is derived using affinity laws. Affinity laws describe the relationship between motor power and speed, which say that the power output of a motor theoretically has a cubic relationship with motor speed. In actuality there are losses and the exponent defining the relationship is typically somewhere between 2.0 and 3.0 [6]. For this review, a value of 2.5 was used.

In addition there are losses inherent to the VFD that must be accounted for. These are typically larger at lower motor sizes and lower speeds, but are typically less than 10%. For this review a penalty of 5% was taken for all VFD applications [7].

¹ Tabulated from TMY2 weather data for London, Ontario from: https://energyplus.net/weather-location/north_and_central_america_wmo_region_4/CAN/ON/CAN_ON_London.716230_CWEC

The savings are calculated from the daily load profiles in Table 5 by assuming the profile is valid for the entire year. This utilizes the following equation which is summed over the hours of the day. The methodology of this equation is to calculate motor power consumption at each hour of the day, assuming constant speed for the hour and multiply by 365 for a full year of operation. This assumes that the daily load profile in Table 5 is accurate for all days of the year [8].

$$Motor\ kWh\ Rate = \sum_{h=1}^{24\ hrs} (V_h - V_h^x) \times 365 \frac{days}{yr} \times \frac{hp}{(\eta - VFD_p)} \times 0.746 \frac{kW}{hp} \div CFM$$

Where,

<i>Motor kWh Rate</i>	= Annual electric savings rate due to the motor modulation (kWh/CFM)
V_h	= Speed of the motor for each hour of the day (%)
x	= Affinity law exponent
$365 \frac{days}{yr}$	= Number of days in the year
hp	= Power input of the fan motor (hp)
η	= Fan motor efficiency (%)
VFD_p	= Penalty for the VFD (%)
$0.746 \frac{kW}{hp}$	= Conversion from hp to kW
<i>CFM</i>	= CFM of MUA (ft ³ /min), see Table 7

Added to this, are the cooling energy savings that are derived from reduced ventilation loads using 2-speed and VFD options. These are calculated similarly to the natural gas savings by summing the cooling load in British Thermal Units and applying a cooling system efficiency using the following formula.

$$Cooling\ Load\ Rate = \left(\sum_{5^\circ}^{T_o} 1.08 \frac{Btu}{hr\ ^\circ F\ CFM} \times bin \times (T_o - T_s) \right)$$

And,

$$Cool\ kWh\ Rate = Cooling\ Load\ Rate \times (V_{Base} - V_{EE}) \div 12,000 \frac{Btu}{ton} \times 0.924 \frac{kW}{ton}$$

Where,

<i>Cool kWh Rate</i>	= The annual cooling load per CFM of MUA rated air flow capacity assuming no modulation (Btu/yr/CFM)
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bin	= Annual hours in each five degree temperature bin ² (hr/yr), see Table 5
T_s	= Supply air temperature set point (°F)
T_o	= Outside air temperatures (°F)
<i>Cool kWh Rate</i>	= The electrical cooling savings rate per CFM of MUA rated air flow capacity assuming no modulation (kWh/yr/CFM)
V_{Base}	= Baseline fan motor speed (%)
V_{EE}	= Energy efficient fan motor speed (%)
$12,000 \frac{Btu}{ton}$	= Conversion of Btus to tons of cooling
$0.924 \frac{kW}{ton}$	= Assumption for efficiency of MUA cooling across all equipment types (kW/ton)

The total electric savings rate is then calculated by adding the electric savings rate from the motor and from the reduced cooling load.

$$kWh \text{ Savings Rate} = Motor \text{ kWh Rate} + Cool \text{ kWh Rate}$$

Where,

<i>kWh Savings Rate</i>	= Total electrical savings rate per CFM (kWh/yr/CFM)
<i>Motor kWh Rate</i>	= Annual electric savings rate due to the motor modulation (kWh/CFM)
<i>Cool kWh Rate</i>	= The electrical cooling savings rate per CFM of MUA rated air flow capacity assuming no modulation (kWh/CFM)

ASSUMPTIONS

The assumptions used to calculate the savings coefficient are shown in Tables 4.

Table 4. Assumptions

Variable	Definition	Inputs	Source
T_s	Supply air temperature set point	72 °F	Common assumptions table
x	Affinity law exponent	2.5	[9]
VFD_p	Percent penalty for VFD losses	5%	[7]

² Tabulated from TMY2 weather data for London, Ontario from: https://energyplus.net/weather-location/north_and_central_america_wmo_region_4/CAN/ON/CAN_ON_London.716230_CWEC

Variable	Definition	Inputs	Source
η	Fan motor efficiency	90%	[10]
	Assumption for efficiency of MUA cooling across all equipment types	0.924 kW/ton	[11]

The load profiles used for the natural gas and electric savings calculations are shown in Table 5.

Table 5. Load Profiles for Multi-Residential/Long Term Care and Commercial Facilities [5]

Hour of the Day	Load Profiles					
	Healthcare and Hotels			Commercial		
	Base	2 stage	VFD	Base	2 stage	VFD
1	100%	50%	50%	0%	0%	0%
2	100%	50%	50%	0%	0%	0%
3	100%	50%	50%	0%	0%	0%
4	100%	50%	50%	0%	0%	0%
5	100%	50%	50%	0%	0%	0%
6	100%	50%	50%	0%	0%	0%
7	100%	100%	100%	0%	0%	0%
8	100%	100%	100%	0%	0%	0%
9	100%	100%	70%	100%	75%	50%
10	100%	100%	70%	100%	75%	50%
11	100%	100%	70%	100%	75%	50%
12	100%	100%	100%	100%	75%	50%
13	100%	100%	100%	100%	75%	50%
14	100%	100%	70%	100%	75%	50%
15	100%	100%	70%	100%	75%	50%
16	100%	100%	70%	100%	75%	50%
17	100%	100%	100%	100%	75%	50%
18	100%	100%	100%	100%	75%	50%
19	100%	100%	100%	100%	75%	50%
20	100%	100%	100%	100%	75%	50%
21	100%	50%	50%	0%	0%	0%
22	100%	50%	50%	0%	0%	0%
23	100%	50%	50%	0%	0%	0%
24	100%	50%	50%	0%	0%	0%
Average Air Flow³	100.0%	79.2%	71.7%	100%	75%	50%

Table 6 shows the binned weather data.

³ Only during hours that ventilation is being provided.

Table 6. Binned Weather Data for London Ontario [4]

Midpoint Temperature (°F) of 5°F bin (+2.5°F, -2.5°F)	Hours In Each Bin (all hours of the year) ⁴ (hours) – Multi-Residential and Long-Term Care	Hours In Each Bin (8am to 8 pm) ⁵ (hours) – Commercial
97.5 (36.4°C)	0	0
92.5 (33.6°C)	8	8
87.5 (30.8°C)	59	59
82.5 (28.1°C)	225	216
77.5 (25.3°C)	407	378
72.5 (22.5°C)	593	385
67.5 (19.7°C)	772	401
62.5 (16.9°C)	717	293
57.5 (14.2°C)	758	317
52.5 (11.4°C)	649	298
47.5 (8.6°C)	625	269
42.5 (5.8°C)	643	268
37.5 (3.1°C)	697	294
32.5 (0.3°C)	672	307
27.5 (-2.5°C)	649	304
22.5 (-5.3°C)	501	259
17.5 (-8.1°C)	352	159
12.5 (-10.8°C)	237	107
7.5 (-13.6°C)	122	47
2.5 (-16.4°C)	61	9
-2.5 (-19.2°C)	13	2
-7.5 (-21.9°C)	0	0
Heating Degree Hours ₇₂	218,846 hr °F	96,948 hr °F
Cooling Degree Hours ₇₂	5,976 hr °F	5,618 hr °F

The assumed fan horsepower for each fan size is shown in Table 7.

Table 7. Fan Size and Associated Fan Power [5]

Fan Flow (CFM)	Fan power (hp)
1,700	1
3,300	2
6,000	3
9,000	5
14,000	8.5

⁴ Hours of operation based on multi-residential and long-term care load profile.

⁵ Hours of operation based on commercial load profile.

SAVINGS CALCULATION EXAMPLE

The example below shows how to calculate gas savings achieved from installing one 1,700 CFM condensing MUA equipped with a VFD in a commercial building.

The heat load rate is calculated first and the sum of the bin hours times the temperature difference is shown.

$$\text{Heat Load Rate} = 1.08 \frac{\text{Btu}}{\text{hr } ^\circ\text{F CFM}} \times 96,948 \text{ hr } ^\circ\text{F} = 104,704 \frac{\text{Btu}}{\text{CFM}}$$

And the calculation for the natural gas savings factor then becomes,

$$\text{NG Savings Factor} = \frac{104,704 \text{ Btu/CFM}}{35,738 \frac{\text{Btu}}{\text{m}^3}} \times \left(\frac{100\%}{80\%} - \frac{50\%}{90\%} \right) = 2.03 \frac{\text{m}^3}{\text{CFM}}$$

Therefore, annual natural gas savings are:

$$\text{Annual NG Savings} = 1,700 \text{ CFM} \times 2.03 \frac{\text{m}^3}{\text{CFM}} = 3,451 \text{ m}^3$$

The annual motor electric savings are calculated also from a summation, which is not easily shown explicitly, but is shown in equation form here,

$$\begin{aligned} \text{Motor kWh Rate} &= \sum_{h=1}^{24 \text{ hrs}} (V_h - V_h^{2.5}) \times 365 \frac{\text{days}}{\text{yr}} \times \frac{1 \text{ hp}}{90\% - 5\%} \times 0.746 \frac{\text{kWh}}{\text{hp}} \div 1700 \text{ CFM} \\ &= 1.86 \frac{\text{kWh}}{\text{CFM}} \end{aligned}$$

The electric savings from the reduced cooling load are calculated similarly to those for the natural gas savings, but using cooling system efficiencies instead of heating system efficiencies.

$$\text{Cooling Load Rate} = \left(1.08 \frac{\text{Btu}}{\text{hr } ^\circ\text{F CFM}} \times 5,618 \text{ hr } ^\circ\text{F} \right) = 6,067 \frac{\text{Btu}}{\text{CFM}}$$

And,

$$\text{Cool kWh Rate} = 6,067 \frac{\text{Btu}}{\text{CFM}} \times (100\% - 50\%) \div 12,000 \frac{\text{Btu}}{\text{ton}} \times 0.924 \frac{\text{kWh}}{\text{ton}} = 0.23 \frac{\text{kWh}}{\text{CFM}}$$

The total electrical savings rate is then:

$$\text{kWh Savings Rate}^6 = 1.86 \frac{\text{kWh}}{\text{CFM}} + 0.23 \frac{\text{kWh}}{\text{CFM}} = 2.10 \frac{\text{kWh}}{\text{CFM}}$$

There for the annual electric savings are:

$$\text{Annual kWh Savings} = 1,700 \text{ CFM} \times 2.10 \frac{\text{kWh}}{\text{CFM}} = 3,562 \text{ kWh}$$

⁶ Note, this value was calculated for the entire range of assumed horsepower sizes and averaged to get 1.60kWh/CFM. Individual sizes vary from the average slightly.

USES AND EXCLUSIONS

To qualify for this measure the condensing MUA must be gas-fired, have a thermal efficiency of at least 90% and be installed in a new commercial facility or replace failed equipment. The unit airflow shall be between 1,500 CFM up to 14,000 CFM. Systems with Demand Control Ventilation will not qualify. Retail is not eligible for this measure.

MEASURE LIFE

The ASHRAE handbook states that the typical design life of commercial heating equipment is 20 years [12].

INCREMENTAL COST

The incremental costs were developed in a study by Agviro Inc. for use by Enbridge Gas Distribution and Union Gas on a per CFM basis.

Table 8. Incremental Cost [5]

Condensing MUA	Condensing MUA and 2 Speed Motor	Condensing MUA and VFD Motor
\$870+\$0.66/CFM	\$870+\$1.01/CFM	\$870+\$1.02/CFM

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COMMERCIAL – CONDENSING STORAGE GAS WATER HEATERS – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Water Heating → Condensing Storage Water Heater → New Construction/Time of Natural Replacement	

Table 1 provides a –summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition		
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)		
Baseline Technology	Non-condensing storage water heater Greater than 75 kBtu/hr. of input Estimated overall efficiency of units shipped = 80.1%		
Efficient Technology	Condensing storage water heater Greater than 75 kBtu/hr. of input Estimated overall efficiency of units shipped = 94.5%		
Market Type	Commercial		
Annual Natural Gas Savings Rate (m ³ per kBtu/hr of rated input)	Low Utilization Application*	Medium Utilization Application*	High Utilization Application*
	1.36 m ³ per kBtu/hr. input	2.22 m ³ per kBtu/hr. input	3.09 m ³ per kBtu/hr. input
	*See Table 3 for utilization categories by facility type		
Measure Life	15 years		
Incremental Cost (\$ CAD)	250 KBtu/hr input rating and below	\$2,591	
	Above 250 KBtu/hr input rating	\$4,464	
Restrictions	This measure applies to the installation of condensing natural gas storage water heaters in commercial facilities.		

OVERVIEW

The measure consists of the installation of natural gas fueled condensing storage water heaters for hot water production in commercial facilities. Non-condensing storage water heaters are not eligible under this measure.

Natural gas fueled non-condensing commercial storage water heaters typically consist of an insulated storage tank and a vented burner. The burner is typically located at the bottom of the tank with a flue running straight up and exiting at the top of the tank. This allows for some cooling of the exhaust gas and associated transfer of energy to the hot water.

A primary difference in the design of condensing storage water heaters is the inclusion of a secondary heat exchanger. The exhaust is routed through this secondary heat exchanger before exiting the tank. This further cools the exhaust to the point where water vapor contained in the exhaust gas condenses, transferring the heat of vaporization to the water in the tank, and significantly improving efficiency.

The condensate removed from the flue gases is corrosive, so the heat exchanger and condensate drain system must be constructed of non-corrosive material adding, to the cost of the unit.

The savings values reported in Table 1 result from the differential in the shipment weighted average thermal efficiency values derived by Caneta Research Inc. as part of a 2009 study. [1] The values were calculated using manufacturers published thermal efficiency data for both condensing and non-condensing storage units and market share information provided by the Consortium for Energy Efficiency.

There is continuous heat loss from the tanks of the storage water heater to the surrounding space. The magnitude of this storage or stand-by loss is largely dependent upon the size of the storage tank and the level of tank insulation, and does not differ between condensing and non-condensing models.

The natural gas savings algorithm and the associated variables are presented in the Natural Gas Savings Algorithm section.

APPLICATION

This measure provides incentives for installing natural gas condensing storage water heaters in commercial facilities for either the new construction or time of natural replacement measure category. The units provide service hot water for entire commercial facilities, or in some cases for selected loads within the facility.

BASELINE TECHNOLOGY

The baseline technology for this measure is a natural gas fueled non-condensing, power-vented, storage water heater or greater, with an input rating of 75 kBtu/hr or greater [2], providing the service hot water needs for all or portions of commercial facilities.

Table 1 provides the shipment weighted average thermal efficiency for non-condensing storage water heaters meeting these criteria.

EFFICIENT TECHNOLOGY

The high efficiency technology is a natural gas fueled condensing storage water heater. Condensing storage water heaters with input rating of 200 kBtu/hr or greater are considered commercial units, but smaller units are frequently installed in commercial facilities to serve all of the service water needs or selected end uses. Units with an input rating of 75 kBtu/hr or greater are eligible for this measure [2]. Units must be certified to the appropriate CSA standard such as: CSA 4.3/ANSI Z21.10.3, or CSA P3-04, DOE 10 CFR Part 430.

Table 1 provides the shipment weighted average thermal efficiency of condensing storage water heaters from the Caneta report referenced earlier.

ENERGY IMPACTS

Natural gas savings are achieved as a result of the higher overall average thermal efficiency of the condensing storage units.

The natural gas algorithms and the associated variables are presented in the Natural Gas Savings Algorithm section.

There are no electric or water consumption impacts associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Shipment-weighted overall average efficiency values for non-condensing and condensing storage water heaters are as shown in Table 2. The values are based on manufacturers published efficiency ratings and market share data obtained in a 2009 study completed for Union Gas. [1]

Table 2. Shipment-Weighted Average Commercial Storage Water Heater Thermal Efficiencies

Type	Average Efficiency
Non-Condensing	80.1%
Condensing	94.5%

The 2011 ASHRAE HVAC Applications Handbook provides typical peak hourly demand and average daily hot water consumption data for several building types. [3] A 2012 Enbridge Gas funded study [4] indicates that water heaters are generally sized based on peak 15-minute demands with an oversizing factor applied. The same study includes data indicating the peak

15-minute demand can be estimated as 140% of the peak hourly demand. These values were used to derive Equivalent Full Load Hours (EFLH) values using the following algorithm.

$$EFLH = Demand_{avg. daily} \times \frac{1}{Demand_{peak 15 minute} \times OS_{factor}} \times Days per year$$

Where,

- $EFLH$ = The annual EFLH (hours/year)
- $Demand_{avg. daily}$ = The reported average daily service hot water demand for a specific building type (US gallon/occupant-day) [3]
- $Demand_{peak 15 minute}$ = The peak 15-minute service hot water demand for a specific building type (US gallon/occupant-hour) [3] [4]
- OS_{factor} = Typical storages water heater oversizing factor relative to 15-minute peak demand (130%) [4]
- $Days per year$ = The number of days per year when the facility is operational

Table 3 provides the EFLH values derived from this data and a description of typical building types and end uses for each utilization category.

Table 3. Utilization Categories and EFLH Values

Category	EFLH	Typical End Uses	Facility Types
Low Utilization	271	Lavatories (hand washing), kitchenette, custodial uses	Elementary schools, office, retail, churches
Medium Utilization	442	Low to moderate use showers, fast food kitchen	Secondary schools, fast food restaurant, dormitories, other
High Utilization	614	High use showers, full commercial kitchen, laundry	Fitness center, full service restaurant, hotels, in patient health care, multi-residential

These average thermal efficiencies and EFLH values are used to derive savings values representing the annual natural gas savings (m³ per kBtu/hr. input rating) associated with the increase in the thermal efficiency values for each utilization category based on the following algorithm.

$$Natural Gas Savings = EFLH \times \left(\frac{\eta_{proposed}}{\eta_{baseline}} - 1 \right) / NG_{ec}$$

Where,

<i>Natural Gas Savings Factor</i>	=Annual natural gas savings factor expressed as m ³ per kBtu/hr. input rating of condensing storage water heater
<i>EFLH</i>	=Annual Equivalent Full Load Hours for the utilization category (hours)
η_{proposed}	=The weighted shipment average thermal efficiency for condensing storage water heaters
η_{baseline}	=The weighted shipment average thermal efficiency for non-condensing storage water heaters
<i>NG_{ec}</i>	= Natural gas energy content

The resulting savings factors are provided in Table 4 below:

Table 4. Natural Gas Savings Resulting from Condensing Storage Water Heaters

Category	Savings
Low Utilization	1.36 m ³ per kBtu/hr. input
Medium Utilization	2.22 m ³ per kBtu/hr. input
High Utilization	3.09 m ³ per kBtu/hr. input

ASSUMPTIONS

Table 5 provides a list of assumptions utilized in the measure savings algorithms to derive the savings factors listed in Tables 1 and 4 above.

Table 5. Assumptions

Variable	Definition	Inputs	Source/Comments
EFLH	Annual equivalent full load hours of operation	Typical peak and hourly average hot water consumption values	Based on data from the ASHRAE HVAC Application Handbook [3] as shown in EFLH formula in the Natural Gas Savings Algorithm section.
η_{proposed} & η_{baseline}	Shipment weighted average thermal efficiency of proposed and baseline units	Results of baseline study	Caneta Research Inc. [5]
NG _{ec}	Energy density of natural gas	35,738 Btu/m ³	Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how savings would be calculated for a condensing storage water heater with rated input capacity of 400 kBtu/hr. in a full service restaurant.

Table 3 above indicates that installation in a full service restaurant is in the high utilization category, with a savings value from Table 1 of 3.09 m³ per kBtu/hr. rated input capacity.

Annual natural gas savings attributed to this high utilization category installation is calculated as:

$$3.09 \frac{m^3}{kBtu/hr} \times 400 \frac{kBtu}{hr} = 1,236 m^3$$

USES AND EXCLUSIONS

Natural gas-fueled condensing storage water heaters installed in commercial facilities and serving all or part of the service water heating load qualify for this measure. The measure type must be new construction or time of natural replacement installation where the preexisting unit was a natural gas non-condensing power-vented storage unit.

MEASURE LIFE

The measure life is 15 years. [6]

INCREMENTAL COST

There are several sources of information reflecting incremental cost associated with residential condensing water heaters but no previous studies reflecting commercial installations were located.

The incremental cost of equipment reported in Table 6 below resulted from an internet search of manufacturers and retailers websites. Retail pricing data for forty condensing and non-condensing units of various size showed relative consistent incremental equipment cost delta ranging between \$1,600 and \$2,000 for units under 250 kBtu/hr input capacity, with a significant increase to around \$3,000 for units with input capacity in excess of 250 kBtu/hr. Table 6 reflects the average incremental equipment cost for units in each of these size categories. The incremental installation cost is taken from an incremental cost study completed for six efficiency programs in the northeast US during 2011 [7], and is consistent with data from other studies.

Table 6. Incremental Cost¹

Input Rating	Incremental Cost of Equipment	Incremental Cost of Installation²	Total Incremental
250 KBtu/hr and below	CAD \$2,432 [8] [9] [10]	\$159 [7]	\$2,591
Above 250 KBtu/hr	CAD \$4,306 [8] [9] [10]	\$159 [7]	\$4,464

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COMMERCIAL – CONDENSING UNIT HEATER – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Condensing Unit Heater → New Construction/Time of Natural Replacement	

Table 1 below provides a summary of the key measure parameters and savings based on the rated input of the unit.

Table 1. Measure Key Data

Parameter		Definitions			
Measure Category		New Construction (NC) Time of Natural Replacement (TNR)			
Baseline Technology		80% Thermal Efficiency, 78% Annual Efficiency			
Efficient Technology		90% Thermal Efficiency, 89% Annual Efficiency			
Market Type		Commercial, Multiresidential			
Annual Natural Gas Savings Rate (m ³ /kBtu/hr)		New Construction	5.92 m ³ per kBtu/hr input rating		
		Time of Natural Replacement	7.89 m ³ per kBtu/hr input rating		
Annual Electric Penalty (kWh/year)		30 – 100 kBtu/hr	125 – 200 kBtu/hr	225 – 300 kBtu/hr	
		NC	222 kWh	398 kWh	410 kWh
		TNR	296 kWh	530 kWh	546 kWh
Measure Life		18 years			
Incremental Cost (\$ CAD)		\$12.90 per kBtu/hr input rating			
Restrictions		Must be a new commercial installation of a condensing unit heater			

OVERVIEW

The measure is for the installation of a condensing unit heater in commercial facilities. A condensing unit heater is a power-vented unit with a primary, non-condensing heat exchanger, followed by a secondary heat exchanger in which waste heat from the flue gases is recovered. As heat is extracted from the flue gases, condensation of some of the water vapor present in the flue gases occurs. To avoid damage to the unit heater from

the corrosive condensate, the heat exchanger is made of a corrosion-resistant material (e.g., stainless steel) and has a condensate drain connection. [1]

The anticipated savings from this measure are calculated utilizing an algorithm. The algorithm and the associated variables are presented in the sections “Natural Gas Savings and Electric Energy Savings Algorithms”.

APPLICATION

The measure covers the installation of condensing unit heaters in commercial settings. Condensing unit heaters are rated by their thermal efficiency, which is a measure of the operating efficiency of the unit. Thermal efficiency is defined as the energy out, or the energy contained in the hot air, divided by the energy in, or the energy contained within the fuel.

BASELINE TECHNOLOGY

Canadian building code requires unit heaters to be manufactured with at least 80% thermal efficiency, which is assumed to be the baseline for the measure shown in Table 2 [2]. The annual efficiency was estimated from the thermal efficiency using the ASHRAE 103 AFUE estimation software [1].

Table 2. Baseline for Condensing Unit Heaters

Type	Efficiency
Non-Condensing Unit Heater	80% Thermal Efficiency [2]
	78% Annual Efficiency [1]

EFFICIENT TECHNOLOGY

The efficient technology is considered to be a condensing unit heater with a thermal efficiency of 90% shown in Table 3. The annual efficiency was estimated from the thermal efficiency using the ASHRAE 103 AFUE estimation software [1].

Table 3. Efficient Technology for Condensing Unit Heater

Type	Efficiency
Condensing Unit Heater	90% Thermal Efficiency
	89% Annual Efficiency [1]

ENERGY IMPACTS

The primary energy impact associated with the installation of condensing boilers in this service territory is a reduction in natural gas usage resulting from the furnace’s improved efficiency. There is an electric energy usage increase resulting from using a higher capacity vent motor on the condensing unit heaters compared with standard unit heaters. No water consumption impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

The measure gas savings are calculated using an assumption for the equivalent full load hours (EFLH) and the difference in assumed efficiencies for the equipment. The EFLH assumption was derived utilizing bin data for the London, Ontario location with an oversizing factor of 25%. The savings factor calculated in this section and presented in Table 1 needs to be multiplied by the input capacity of the condensing unit heater to get annual savings for the measure.

The natural gas savings factor attributed to this measure is calculated using the following formula:

$$NG\ Savings\ Factor = \frac{EFLH}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{AE_{EE}}{AE_{base}} - 1 \right)$$

where,

<i>NG Savings Factor</i>	= Annual gas savings (m ³ /yr per kBtu/hr of new unit heater input capacity)
<i>EFLH</i>	= Equivalent full load hours (hr/yr)
$35.738 \frac{kBtu}{m^3}$	= Conversion of rated heating capacity from kBtu to m ³
<i>AE_{base}</i>	= Baseline equipment annual efficiency (%)
<i>AE_{EE}</i>	= Efficient equipment annual efficiency (%)

ELECTRIC PENALTY ALGORITHMS

Condensing unit heaters use more electricity than comparably sized non-condensing units. The measure electric energy penalty is calculated using the same assumption for EFLH as used in the natural gas savings and shown in Table 4. The electric consumption assumptions are shown in Table 5.

The electric energy penalty value attributed to this measure is calculated using the following formula:

$$\text{Annual kWh Penalty} = EFLH \times (\text{Elect}_{base} - \text{Elect}_{EE})$$

where,

Annual kWh Penalty = annual electric energy penalty resulted from installing the new unit heater (kWh/yr)

EFLH = Equivalent full load hours (hr/yr)

Elect_{base} = Power consumption of the baseline unit (kW)

Elect_{EE} = Power consumption of the condensing unit heater (kW)

LIST OF ASSUMPTIONS

The assumptions used to calculate the savings coefficient are shown in Table 4.

Table 4. Assumptions List

Variable	Definition	Inputs	Source
<i>EFLH_{NC}</i>	Equivalent full load hours for a unit heater – new construction	1,500 hrs	Common assumptions table
<i>EFLH_{TNR}</i>	Equivalent full load hours for a unit heater – time of natural replacement	2,000 hrs	Common assumptions table

The average electrical consumption values in Table 5 are researched from power ratings for a variety of units.

Table 5. Average Electrical Consumption [1]

Size Range	Baseline (kW)	Efficient (kW)
30 – 100 kBtu/hr	0.155	0.303
125 – 200 kBtu/hr	0.392	0.657
225 – 300 kBtu/hr	0.747	0.1020

SAVINGS CALCULATION EXAMPLE

The example below shows how to calculate gas savings achieved from installing one condensing unit heater with a rated input of 162.5 kBtu/hr in a new building.

$$NG \text{ savings factor} = \frac{1,500 \frac{hr}{yr}}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{89\%}{78\%} - 1 \right) = 5.92 \text{ per kBtu/hr input}$$

$$Annual \text{ NG savings} = 5.92 \frac{\frac{m^3}{yr}}{\frac{kBtu}{hr}} \times 162.5 \frac{kBtu}{hr} = 962 \frac{m^3}{yr}$$

The annual electric penalty is:

$$Annual \text{ kWh Penalty} = 1,500 \text{ hrs} \times (0.392 - 0.657) \text{ kW} = 398 \text{ kWh}$$

USES AND EXCLUSIONS

To qualify for this measure the condensing unit heater must be gas-fired, be installed in commercial facilities, and meet or exceed the minimum efficiency as shown in section "Efficient Technology" above.

MEASURE LIFE

The measure life attributed to this measure is 18 years [3] [4].

INCREMENTAL COST

The incremental cost of buying a condensing instead of non-condensing unit heater is \$12.90 per kBtu/hr. [1]

REFERENCES

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COMMERCIAL – DEMAND CONTROLLED VENTILATION – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
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Commercial → Space Heating → Demand Control Ventilation → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings coefficients differentiated by facility type:

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)	
Baseline Technology	New single-zone, constant volume ventilation system with natural gas fueled heating	Designed and operating in a manner that provides the minimum outdoor air requirement as specified in Table 6.2.2.1 of ASHRAE Standard 62.1-2013 [1]
Efficient Technology		Ventilation rate during the occupied periods of the building schedule is modulated in response to actual CO ₂ concentrations, as measured with an appropriately located CO ₂ sensor
Market Type	Commercial	
Annual Natural Gas Savings Rate (m ³ /ft ²)	Space Type	Savings
	Office	0.112 m ³ /ft ²
	Retail	0.392 m ³ /ft ²
Measure Life (\$ CAD)	10 years May be extended to 15 years with documented maintenance plan (see Measure Life section)	
Incremental Cost	\$1,050 per zone	
Restrictions	Multi-zone systems, variable air volume (VAV) systems, or systems equipped with heat recovery capabilities are not eligible for this prescriptive measure. Applications with free cooling economizers are eligible for this prescriptive measure.	

OVERVIEW

Adequate ventilation of buildings is necessary to remove “pollutants” resulting from activities occurring within the space and maintain acceptable levels of indoor air quality. This ventilation is typically accomplished by introducing a quantity of outside air sufficient to dilute the pollutants, while the same quantity of “contaminated” air is removed from the building through either passive or active means of building exhaust.

The minimum required ventilation rate is typically established during the design process, based on applicable building codes and anticipated occupancy patterns. Consideration is also given to any special building functions expected to generate excessive levels of pollutants (various manufacturing processes, sustained high levels of human activity, etc.).

Heating, cooling, and maintaining acceptable humidity levels for the ventilation air introduced to the space represent a very significant component of the overall building energy consumption. This energy is typically much greater than the sum of all “skin losses” or surface heat transfer from the building. Excessive ventilation can be extremely costly, with little if any associated benefit.

DCV is a control strategy that automatically modulates outside air dampers to control the quantity of outside air introduced to a space based on the “demand” or level of contaminants being produced within the space. In most spaces the optimum ventilation rate fluctuates in direct proportion to occupancy and the level of activity within the space.

There can be many different types of indoor air pollutants specific to the particular building activities. One common pollutant found in all occupied spaces is CO₂, which is produced by humans through respiration. CO₂ levels expressed in parts per million (ppm) have been found to provide a good representation of overall indoor air quality, and except for cases where specific process-related pollutants overshadow their impact, have become the universally accepted controlled variable for DCV systems.

APPLICATION

This measure pertains to the implementation of DCV, based on CO₂ concentrations within the space, for single-zone, constant volume ventilation systems.

Implementation includes the installation of a CO₂ sensor in an appropriate location within the space or in the return air duct. The sensor outputs are provided to an automated control system with a programmed sequence of operation that modulates the outside air damper position, controlling the ventilation rate in response to CO₂ concentrations. The controller can be part of the facility’s building automation system or an independent control device, integrated within a packaged rooftop unit (RTU), air handling unit (AHU), or make-up air unit (MUA).

Installations covered under this TRM section are incorporated into new RTUs or MUAs with natural gas heating as part of new construction or overall equipment replacement projects at the time of natural replacement.

DCV can also be implemented for complex ventilation systems including multi-zone and variable air volume (VAV) systems. However, the Enermodal market research study [3] conducted prior to development of this measure correctly concluded that the relative complexity of the installations and the wide variations in achievable savings make these installations better candidates for custom incentive applications.

BASELINE TECHNOLOGY

The baseline technology is represented by an existing single-zone, constant volume ventilation system, with natural gas-fueled heating, designed and operating in a manner that provides the minimum outdoor air requirement as specified by the data provided in Table 6.2.2.1 of ASHRAE Standard 62.1-2013. [1]

These minimum design outdoor air ventilation rates are intended to meet ventilation requirements when the space is at the anticipated peak occupancy level. ASHRAE Standard 62.1, Table 6.2.2.1 provides default occupancy density values for various space types along with values representing the minimum ventilation per person and per unit of area served by the system.

The baseline system provides this minimum outdoor air requirement on a continuous basis throughout the occupied periods of the building schedule and does not provide ventilation during the unoccupied periods of the building schedule¹. Table 2 presents the baseline requirements.

Table 2. Baseline Technology

Type	Requirement
New single-zone, constant volume ventilation system with natural gas fueled heating	Designed and operating in a manner that provides the minimum outdoor air requirement as specified in Table 6.2.2.1 of ASHRAE Standard 62.1-2013 [1], on a continuous basis during the occupied periods

EFFICIENT TECHNOLOGY

The efficient technology is represented by the baseline ventilation system with an appropriately located CO₂ sensor, a controller, and a control algorithm established to limit the maximum outdoor air ventilation rate to that based on the ASHRAE 62.1, Table 6.2.2.1 prescribed values, equivalent to the continuous occupied period ventilation provided by the baseline system.

The CO₂ sensor measures CO₂ concentrations and provides an output signal to a stand-alone control device specific to the ventilation system. The controller will accept the input from the sensor and generate a corresponding output signal to the outside air damper actuator, adjusting the damper position as described below.

¹ Some systems may have a fixed minimum outside air damper position, (typically 5% OA), to allow for a minimum level of ventilation even during unoccupied hours. As long as this minimum is present in both the baseline and efficient scenarios (with DCV implemented), it has no impact on the resulting measure savings.

Appendix H of the Enermodal market research study [3] presents the results of a survey of RTU installers representing 1,000 DCV installations. The study confirmed that control algorithms are typically established based on an assumed differential of 700 ppm in CO₂ concentrations of ambient outside air and design condition interior air. Typical ambient air CO₂ concentrations are around 400 ppm, meaning that most systems are calibrated to allow for steady state CO₂ concentrations of up to 1,100 ppm when the space is fully occupied with the outside air dampers at the position intended to allow for the ASHRAE 62.1 prescribed design flow rate. As occupancy declines, the CO₂ concentration drops and the controller reduces the damper opening. With no occupants in the space the CO₂ concentration eventually reaches the outdoor ambient level, at which point the outside air damper is closed (or in some cases set to a minimum position as described in footnote 1 on the previous page). Table 3 presents the efficient system requirements.

Table 3. Efficient Technology

Type	Requirement
New single-zone, constant volume ventilation system with natural gas fueled heating	Ventilation rate during the occupied periods of the building schedule is modulated in response to actual CO ₂ concentrations, as measured with an appropriately located CO ₂ sensor

ENERGY IMPACTS

The primary energy impact associated with implementation of DCV in this service territory is lower heating fuel consumption resulting from a reduction in the quantity of outside air introduced to the space during the heating season. Table 1 in the “Overview” section provides annual savings values (m³ natural gas / ft² area served), differentiated by space type. The savings are based on climate data for London, Ontario, which was selected as a proxy city for Ontario based on a weighted average analysis of Ontario’s 10 largest cities, provided by Enbridge Gas. The spreadsheet analysis used population and degree data obtained from online sources and was validated as part of the review for this measure. [4] [5] [6]

Extensive analysis completed by Enermodal Engineering as part of a market research study [3] led to the conclusion that in Ontario the cooling season energy impact (electric energy savings) occurs only during a limited number of hours when the space requires cooling and outside air temperature is warmer than the space temperature. The Excel-based tool developed by Enermodal Engineering and used to derive the savings values provided in Table 1 predicted cooling season electric savings equivalent to less than 1% of the projected heating natural gas savings. The predicted electric energy savings by the model is small enough to be within the level of precision that could reasonably be attained by the savings algorithm leading to the prediction.²

There is no water consumption impact associated with this measure.

² A reduction of the system peak electrical demand could result if space occupancy during the peak period is lower than the peak occupancy levels defined by ASHRAE 62.1 table 6.2.2.1.

NATURAL GAS SAVINGS ALGORITHM

As part of the Enermodal market research study [3], a spreadsheet tool was developed to predict annual natural gas savings for spaces of various types and sizes in selected locations throughout the Enbridge-Union Gas service territories. The tool is based on the algorithm described below.

The spreadsheet tool's multi-step algorithm is used to predict annual energy savings for spaces with varying end uses and sizes in five different climate zones. The results were calibrated against eQUEST-DOE-2 [7] building simulation model results for seventy-five combinations of building types, sizes, and climate zones.

The specific steps in the spreadsheet algorithm are as follows:

1. Determine the maximum anticipated occupancy and the associated design minimum outside air flow rate in CFM that is required by code [1]. This represents the baseline condition whenever the space is occupied.

$$Flow_{Design} = Occ_{Design} \times \frac{SF}{1000} \times Rp + SF \times Ra$$

where,

$Flow_{Design}$ = The design ventilation rate in expressed (CFM)

Occ_{Design} = The design occupants per 1000 square feet (from ASHRAE 62.1, Table 6.2.2.1)

SF = The area of zone served (ft²)

Rp = The occupant ventilation rate, CFM per person (from ASHRAE 62.1, Table 6.2.2.1)

Ra = The area ventilation rate, CFM per square foot (from ASHRAE 62.1, Table 6.2.2.1)

2. Apply the appropriate occupancy schedule [8] and determine space occupancy and the associated outside air flow rate (CFM) on an hourly basis for the efficient case condition during occupied periods with DCV implemented.

$$Flow_{efficient\ case} = Occ_{Design} \times \% Occ \times \frac{SF}{1000} \times Rp + SF \times Ra$$

where,

$Flow_{efficient\ case}$ = The hourly efficient case ventilation rate in expressed (CFM)

$\% Occ$ = The value taken from US DOE commercial reference building typical occupancy schedule for the specified space type.

When the space is unoccupied the outside air flow is assumed to be zero for both the baseline and efficient case scenario.

- Use typical hourly weather data [9] (dry-bulb temperature, humidity ratio, and outdoor air pressure) to calculate the density of air (lb/ft³) on an hourly basis and determine the resulting mass flow rate (lb/min).

$$M = Density_{Air} \times Flow_{Hourly} \times 60 \text{ min/hour}$$

where,

M_{hourly} = The hourly mass flow rate of air (lbs/hour)

$Density_{Air}$ = The density calculated from typical weather data representing each hour in the specific climate zone (lb/ft³)

$Flow_{Hourly}$ = The flow rate calculated in the above equations for each hour of the year (CFM)

- Subtract the hourly outdoor air temperature from the desired supply air temperature to determine the need for heating and the temperature rise (°F) required for each hour and calculate thermal energy requirement.

$$Q = M \times Cp_{Air} \times \Delta T$$

where,

Q = The thermal energy requirement (Btu/hour)

Cp_{Air} = The specific heat of air (Btu/lb-°F)

ΔT = The difference between average hourly outdoor temperature and supply air temperature (°F)

- Divide the hourly thermal energy requirement by the typical heating system efficiency to calculate the hourly average input energy (m³) for the baseline and efficient case conditions.

$$NG_{Hourly} = Q / \text{Heating system efficiency}$$

where,

NG_{Hourly} = The hourly natural gas consumption (m³)

$\text{Heating system efficiency}$ = The average heating system efficiency

- Sum the hour results to determine the annual energy input (kWh) of the baseline and efficient case conditions and deduct the annual efficient case energy input from the baseline value to determine the predicted annual savings in m³ of natural gas.

$$\text{Annual savings} = \sum_0^{8760} NG_{\text{efficient case}} - \sum_0^{8760} NG_{\text{Baseline}}$$

where,

Annual savings = The annual natural gas savings (m³/year)

$\sum_0^{8760} NG_{efficient\ case}$ = The summation of the efficient case hourly natural gas consumption

$\sum_0^{8760} NG_{Baseline}$ = The summation of the baseline hourly natural gas consumption

The results were normalized to derive the annual savings per square foot of area served for the typical climate zone represented by London, Ontario, presented in Table 1.

The savings values (m³/ft²) derived from the spreadsheet tool and reflected in Table 1 are then used to calculate and report project specific savings as follows:

$$Savings_{NG} = Savings \times Zone\ area$$

where,

$Savings_{NG}$ = The annual natural gas savings (m³)

$Savings$ = The savings value for the space type and climate zone from Table 1 (m³/ft²)

$Zone\ area$ = The area of the zone served by the RTU, AHU, or MUA (ft²)

ASSUMPTIONS

Table 4 provides a list of constants and assumption used in the derivation of the savings values.. Because duct runs for single-zone RTUs are generally short and/or within the conditioned space, this value also represents a reasonable estimate of system efficiency.

Table 4. Assumptions

Parameter	Value	Units	Reference
Space temperature setpoint	72	°F	Common assumptions table
OA temperature heating system is enabled	55	°F	Common assumptions table
Commercial heating system efficiency	80%	%	Common assumptions table
Energy density of natural gas	35,738	Btu/m ³	Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for a demand controlled ventilation installation for a 10,000 ft² office single-zone area.

$$\begin{aligned}
 Savings_{NG} &= Savings \times Zone\ area \\
 &= 0.112\ m^3/ft^2 \times 10,000\ ft^2 \\
 &= 1,120\ m^3\ per\ year
 \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure, DCV must be implemented for a single-zone, constant volume ventilation system with natural gas-fueled heating that previously operated to provide constant ventilation meeting the minimum outdoor air requirements specified by ASHRAE 62.1, Table 6.2.2.1.

Multi zone systems, VAV systems, or systems equipped with heat recovery capabilities are not eligible for this prescriptive measure.

MEASURE LIFE

The standard measure life attributed to this measure is 10 years. [2] This measure life is based on the predicted sustained savings associated with properly calibrated sensors and a well maintained control system.

Although physical components of the ventilation system can be expected to last longer, energy savings persist only as long as sensors and other components of the DCV system remain in calibration and functioning as intended.

Self-calibrating sensors are now available. The calibration warranty period for these sensors is typically between 3 and 5 years, depending upon the manufacturer.

In specific circumstances where a documented maintenance plan is in place, measure life is extended to 15 years. The maintenance plan must provide for inspection and calibration of all control system components, including but not limited to sensors, actuators, and transducers on a regular interval of not more than 5 years.

INCREMENTAL COST

Table 5 presents the measure incremental cost.

Table 5. Incremental Cost [3]

Measure Category	Cost Component	Incremental Cost (\$)
New construction / time of natural replacement	Equipment	\$750
	Maintenance (Year 5)	\$300
	Total (10 year life)	\$1,050
	Maintenance (Year 10)	\$300
	Total (15 year life)	\$1,350

Because the sustained savings over the measure life are dependent upon the periodic calibration of the sensors, costs associated with this effort over the anticipated 10-year measure life are included. The cost reflected above includes calibration at year 5 and in the case of a 15-year measure life at year 10, with an estimated cost of \$300.

REFERENCES

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COMMERCIAL – DEMAND CONTROLLED VENTILATION – RETROFIT

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Version	1
OEB Filing Date	Dec 21, 2016
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Commercial → Space Heating → Demand Controlled Ventilation → Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients differentiated by facility type.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	Retrofit (R)	
Base Technology	Existing single zone, constant volume ventilation system with natural gas-fueled heating	Designed and operating in a manner that provides the minimum outdoor air requirement as specified in Table 6.2.2.1 of ASHRAE Standard 62.1-2013 [1]
Efficient Technology		Ventilation rate during the occupied periods of the building schedule is modulated in response to actual CO ₂ concentrations, as measured with an appropriately located CO ₂ sensor.
Market Type	Commercial	
Annual Natural Gas Savings Rate (m ³ /ft ²)	Space Type	Savings
	Office	0.112 m ³ /ft ²
	Retail	0.392 m ³ /ft ²
Measure Life	10 years May be extended to 15 years with documented maintenance plan (see Measure Life section)	
Incremental Cost (\$ CAD)	\$1,350 per zone	
Restrictions	Multi-zone systems, VAV systems, or systems equipped with heat recovery capabilities are not eligible for this prescriptive measure. Applications with free cooling economizers are eligible for this prescriptive measure.	

OVERVIEW

Adequate ventilation of buildings is necessary to remove “pollutants” resulting from activities occurring within the space and maintain acceptable levels of indoor air quality. This ventilation is typically accomplished by introducing a quantity of outside air sufficient to dilute the pollutants, while the same quantity of “contaminated” air is removed from the building through either passive or active means of building exhaust.

The minimum required ventilation rate is typically established during the design process, based on applicable building codes and anticipated occupancy patterns. Consideration is also given to any special building functions expected to generate excessive levels of pollutants (various manufacturing processes, sustained high levels of human activity, etc.).

Heating, cooling, and maintaining acceptable humidity levels for the ventilation air introduced to the space represent a very significant component of the overall building energy consumption. This energy is typically much greater than the sum of all “skin losses” or surface heat transfer from the building. Excessive ventilation can be extremely costly, with little if any associated benefit.

DCV is a control strategy that automatically modulates outside air dampers to control the quantity of outside air introduced to a space based on the “demand” or level of contaminants being produced within the space. In most spaces the optimum ventilation rate fluctuates in direct proportion to occupancy and the level of activity within the space.

There can be many different types of indoor air pollutants specific to the particular building activities. One common pollutant found in all occupied spaces is CO₂, which is produced by humans through respiration. CO₂ levels expressed in parts per million (ppm) have been found to provide a good representation of overall indoor air quality, and except for cases where specific process-related pollutants overshadow their impact, have become the universally accepted controlled variable for DCV systems.

APPLICATION

This measure pertains to the implementation of DCV, based on CO₂ concentrations within the space, for single-zone, constant volume ventilation systems.

Implementation includes the installation of a CO₂ sensor in an appropriate location within the space or in the return air duct. The sensor outputs are provided to an automated control system with a programmed sequence of operation that modulates the outside air damper position, controlling the ventilation rate in response to CO₂ concentrations. The controller can be part of the facility’s building automation system or an independent control device, integrated within a packaged roof top unit (RTU), air handling unit (AHU), or make-up air unit (MUA).

Installations covered under this TRM section are incorporated as part of a retrofit into existing functional ventilation systems.

DCV can also be implemented for complex ventilation systems, including multi-zone and variable air volume (VAV) systems. However, the Enermodal market research study [2] conducted prior to development of this measure correctly concluded that the relative complexity of the installations and the wide variations in achievable savings make these installations better candidates for custom incentive applications.

BASELINE TECHNOLOGY

The baseline technology is represented by an existing single-zone, constant volume ventilation system, with natural gas-fueled heating, designed and operating in a manner that provides the minimum outdoor air requirement as specified by the data provided in Table 6.2.2.1 of ASHRAE Standard 62.1-2013. [1]

These minimum-design outdoor air ventilation rates are intended to meet ventilation requirements when the space is at the anticipated peak occupancy level. ASHRAE Standard 62.1, Table 6.2.2.1 provides default occupancy density values for various space types along with values representing the minimum ventilation per person and per unit of area served by the system.

The baseline system provides this minimum outdoor air requirement on a continuous basis throughout the occupied periods of the building schedule, and it does not provide ventilation during the unoccupied periods of the building schedule¹. Table 2 presents the baseline requirements.

Table 2. Baseline Technology

Type	Requirement
Existing single-zone, constant volume ventilation system with natural gas-fueled heating	Designed and operating in a manner that provides the minimum outdoor air requirement as specified in Table 6.2.2.1 of ASHRAE Standard 62.1-2013 [1], on a continuous basis during the occupied periods

EFFICIENT TECHNOLOGY

The efficient technology is represented by the baseline ventilation system with an appropriately located CO₂ sensor, a controller, and a control algorithm established to limit the maximum outdoor air ventilation rate to that based on the ASHRAE 62.1, Table 6.2.2.1 prescribed values, equivalent to the continuous occupied period ventilation provided by the baseline system.

The CO₂ sensor measures CO₂ concentrations and provides an output signal to a stand-alone control device specific to the ventilation system. The controller will accept the input from the sensor and generate a corresponding output signal to the outside air damper actuator, adjusting the damper position as described below.

¹Some systems may have a fixed minimum outside air damper position, (typically 5% OA), to allow for a minimum level of ventilation even during unoccupied hours. As long as this minimum is present in both the baseline and efficient scenarios (with DCV implemented), it has no impact on the resulting measure savings.

Appendix H of the Enermodal market research study [2] presents the results of a survey of RTU installers representing 1,000 DCV installations. The study confirmed that control algorithms are typically established based on an assumed differential of 700 ppm in CO₂ concentrations of ambient outside air and design condition interior air. Typical ambient air CO₂ concentrations are around 400 ppm, meaning that most systems are calibrated to allow for steady state CO₂ concentrations of up to 1,100 ppm when the space is fully occupied with the outside air dampers at the position intended to allow for the ASHRAE 62.1 prescribed design flow rate. As occupancy declines, the CO₂ concentration drops and the controller reduces the damper opening. With no occupants in the space the CO₂ concentration eventually reaches the outdoor ambient level, at which point the outside air damper is closed, (or in some cases set to a minimum position as described in footnote 1 on the previous page). Table 3 presents the efficient system requirements.

Table 3. Efficient Technology

Type	Requirement
Existing single-zone, constant volume ventilation system with natural gas-fueled heating	Ventilation rate during the occupied periods of the building schedule is modulated in response to actual CO ₂ concentrations, as measured with an appropriately located CO ₂ sensor

ENERGY IMPACTS

The primary energy impact associated with implementation of DCV in this service territory is lower heating fuel consumption resulting from a reduction in the quantity of outside air introduced to the space during the heating season. Table 1 in the “Overview” section provides annual savings values (m³ natural gas / ft² area served), differentiated by space type. The savings are based on climate data for London, Ontario, which was selected as a proxy city for Ontario based on a weighted average analysis of Ontario’s 10 largest cities, provided by Enbridge Gas. The spreadsheet analysis used population and degree data obtained from online sources and was validated as part of the review for this measure. [3] [4] [5]

Extensive analysis completed by Enermodal Engineering as part of a market research study [2] led to the conclusion that in Ontario the cooling season energy impact (electric energy savings) occurs only during a limited number of hours when the space requires cooling and outdoor air temperature is warmer than the space temperature. The Excel-based tool developed by Enermodal Engineering and used to derive the savings values provided in Table 1 predicted cooling season electric savings equivalent to less than 1% of the projected heating natural gas savings. The predicted electric energy savings by the model is small enough to be within the level of precision that could reasonably be attained by the savings algorithm leading to the prediction.²

There is no water consumption impact associated with this measure.

² A reduction of the system peak electrical demand could result if space occupancy during the peak period is lower than the peak occupancy levels defined by ASHRAE 62.1 table 6.2.2.1.

NATURAL GAS SAVINGS ALGORITHM

As part of the Enermodal market research study [2], a spreadsheet tool was developed to predict annual natural gas savings for spaces of various types and sizes in selected locations throughout the Enbridge-Union Gas service territories. The tool is based on the algorithm described below.

The spreadsheet tool's multi-step algorithm is used to predict annual energy savings for spaces with varying end uses and sizes in five different climate zones. The results were calibrated against eQUEST-DOE-2 [6] building simulation model results for seventy-five combinations of building types, sizes, and climate zones.

The specific steps in the spreadsheet algorithm are as follows:

1. Determine the maximum anticipated occupancy and the associated design minimum outside air flow rate in CFM that is required by code [1]. This represents the baseline condition whenever the space is occupied.

$$Flow_{Design} = Occ_{Design} \times \frac{SF}{1000} \times Rp + SF \times Ra$$

where,

$Flow_{Design}$	= The design ventilation rate in expressed (CFM)
Occ_{Design}	= The design occupants per 1000 square feet (from ASHRAE 62.1, Table 6.2.2.1)
SF	= The area of zone served (ft ²)
Rp	= The occupant ventilation rate, CFM per person (from ASHRAE 62.1, Table 6.2.2.1)
Ra	= The area ventilation rate, CFM per square foot (from ASHRAE 62.1, Table 6.2.2.1)

2. Apply the appropriate occupancy schedule [7] and determine space occupancy and the associated outside air flow rate (CFM) on an hourly basis for the efficient case condition during occupied periods with DCV implemented.

$$Flow_{efficient\ case} = Occ_{Design} \times \% Occ \times \frac{SF}{1000} \times Rp + SF \times Ra$$

where,

$Flow_{efficient\ case}$	= The hourly efficient case ventilation rate in expressed (CFM)
$\% Occ$	= The value taken from US DOE commercial reference building typical occupancy schedule for the specified space type

When the space is unoccupied the outside air flow is assumed to be zero for both the baseline and efficient case scenario.

- Use typical hourly weather data [8] (dry-bulb temperature, humidity ratio, and outdoor air pressure) to calculate the density of air (lb/ft³) on an hourly basis and determine the resulting mass flow rate (lb/min).

$$M = Density_{Air} \times Flow_{Hourly} \times 60 \text{ min/hour}$$

where,

M_{Hourly} = The hourly mass flow rate of air (lbs/hour)

$Density_{Air}$ = The density calculated from typical weather data representing each hour in the specific climate zone (lb/ft³)

$Flow_{Hourly}$ = The flow rate calculated in the above equations for each hour of the year (CFM)

- Subtract the hourly outdoor air temperature from the desired supply air temperature to determine the need for heating and the temperature rise (°F) required for each hour and calculate the thermal energy requirement.

$$Q = M \times Cp_{Air} \times \Delta T$$

where,

Q = The thermal energy requirement (Btu/hour)

Cp_{Air} = The specific heat of air (Btu/lb-°F)

ΔT = The difference between average hourly outdoor temperature and supply air temperature (°F)

- Divide the hourly thermal energy requirement by the typical heating system efficiency to calculate the hourly average input energy (m³) for the baseline and efficient case conditions.

$$NG_{Hourly} = Q / \text{Heating system efficiency}$$

where,

NG_{Hourly} = The hourly natural gas consumption (m³)

$\text{Heating system efficiency}$ = The average heating system efficiency

- Sum the hour results to determine the annual energy input (kWh) of the baseline and efficient case conditions and deduct the annual efficient case energy input from the baseline value to determine the predicted annual savings in m³ of natural gas.

$$\text{Annual savings} = \sum_0^{8760} NG_{\text{efficient case}} - \sum_0^{8760} NG_{\text{Baseline}}$$

where,

Annual savings = The annual natural gas savings (m³/year)

$\sum_0^{8760} NG_{efficient\ case}$ = The summation of the efficient case hourly natural gas consumption

$\sum_0^{8760} NG_{Baseline}$ = The summation of the baseline hourly natural gas consumption

The results were normalized to derive the annual savings per square foot of area served for the typical climate zone represented by London, Ontario presented in Table 1.

The savings values (m³ / ft²) derived from the spreadsheet tool and reflected in Table 1 are then used to calculate and report project specific savings as follows:

$$Savings_{NG} = Savings \times Zone\ area$$

where,

$Savings_{NG}$ = The annual natural gas savings (m³)

$Savings$ = The savings value for the space type and climate zone from Table 1 (m³ / ft²)

$Zone\ area$ = The area of the zone served by the RTU, AHU, or MUA (ft²)

ASSUMPTIONS

Table 4 provides a list of constants and assumption used in the derivation of the savings values. Because duct runs for single-zone RTUs are generally short and/or within the conditioned space, this value also represents a reasonable estimate of system efficiency.

Table 4. Assumptions

Parameter	Value	Units	Reference
Space temperature setpoint	72	°F	Common assumptions table
OA temperature heating system is enabled	55	°F	Common assumptions table
Commercial heating system efficiency	80%	%	Common assumptions table
Energy density of natural gas	35,738	Btu/m ³	Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for a DCV installation for a 10,000 ft² office single zone area.

$$\begin{aligned} Savings_{NG} &= Savings \times Zone\ area \\ &= 0.112\ m^3/ft^2 \times 10,000\ ft^2 \\ &= 1,120\ m^3\ per\ year \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure, DCV must be implemented for a single-zone, constant volume ventilation system, with natural gas fueled heating that previously operated to provide constant ventilation meeting the minimum outdoor air requirements specified by ASHRAE 62.1 Table 6.2.2.1.

Multi-zone systems, VAV systems, or systems equipped with energy or heat recovery capabilities are not eligible for this prescriptive measure.

MEASURE LIFE

The standard measure life attributed to this measure is 10 years. [9] This measure life is based on the predicted sustained savings associated with properly calibrated sensors and a well-maintained control system.

Although physical components of the ventilation system can be expected to last longer, energy savings persist only as long as sensors and other components of the DCV system remain in calibration and functioning as intended.

Self-calibrating sensors are now available. The calibration warranty period for these sensors is typically between 3 and 5 years, depending upon the manufacturer.

In specific circumstances where a documented maintenance plan is in place, the measure life is extended to 15 years. The maintenance plan must provide for inspection and calibration of all control system components, including but not limited to sensors, actuators, and transducers on a regular interval of not more than 5 years.

INCREMENTAL COST

Table 5 presents the measure incremental cost.

Table 5. Measure Incremental Cost [2]

Measure Category	Cost Component	Incremental Cost (\$)
Retrofit	Equipment	\$750
	Installation	\$300
	Maintenance (Year 5)	\$300
	Total (10 year life)	\$1,350
	Maintenance (Year 10)	\$300
	Total (15 year life)	\$1,650

Because the sustained savings over the measure life are dependent upon the periodic calibration of the sensors, costs associated with this effort over the anticipated 10-year measure life are included. The cost reflected above includes calibration at year 5 and in the case of a 15-year measure life at year 10, with an estimated cost of \$300.

REFERENCES

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COMMERCIAL – DESTRATIFICATION FANS– NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Destratification Fans → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients.

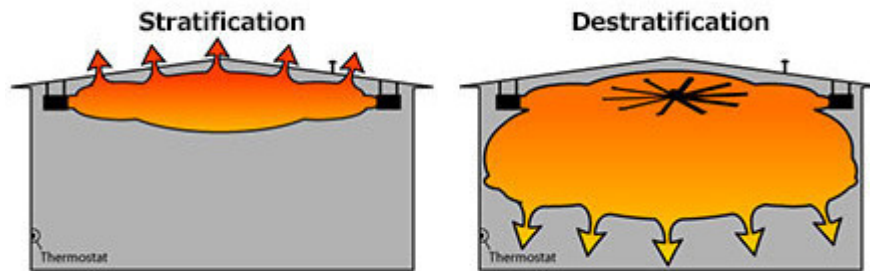
Table 1. Measure Key Data

Parameter	Definition	
Measure Category	New Construction (NC) Retrofit (R)	
Baseline Technology	No destratification fans	
Efficient Technology	Destratification fans	
Market Type	Commercial	
Annual Natural Gas Savings (m ³ / fan)	New Construction	Retrofit
	583 m ³ /fan	1,734 m ³ /fan
Measure Life	15 years	
Incremental Cost (\$ CAD)	\$8,714	
Restrictions	This measure is restricted to fans with a minimum diameter of 20 feet for use in warehousing, manufacturing, industrial or retail buildings with a minimum of 25 foot ceilings and forced air space heating, including unit heaters.	

OVERVIEW

This measure is for the installation of destratification fans in new and retrofit commercial types of applications. Figure 1 illustrates air mixing and resulting uniform air temperature distribution caused by the destratification fans. Natural gas savings are calculated using an engineering algorithm and are reported in meters cubed per square foot of roof area (m³/ft²).

Figure 1: Stratification vs. Destratification¹



APPLICATION

This measure provides incentives for installing destratification fans in commercial facilities. The units serve to reduce the stratification of air in a space with a high ceiling and therefore reduce space heating requirements.

BASELINE TECHNOLOGY

The baseline case is a space with neither destratification fans nor other mechanisms that combat destratification, such as radiant heaters and high velocity vertical throw unit heaters

EFFICIENT TECHNOLOGY

The energy efficient case is a space with destratification fans.

ENERGY IMPACTS

Stratification can result in ceiling temperatures as much as 10°C higher than temperatures at floor level [1]. As a result, thermostats are typically set higher to maintain temperatures which are comfortable for employees near the floor which in turn results in greater gas usage for heating. Destratification fans are designed to move large volumes of air at slow rates. This air churning moves the warmer air near the ceiling downward which equalizes the temperature within the space and also benefits the employees comfort levels on the floor. Depending on the size of the space, destratification fans can reduce ceiling temperatures by an average of 4°C and increase floor temperatures by an average of 1.5°C resulting in an overall temperature profile difference of less than 0.5°C [1]. Natural gas savings are achieved due to the difference in heat loss through the roof before and after destratification.

¹ Photograph downloaded from <http://www.allseasonshire.eu/blog/thermal-destratification-explained/> on 10/1/2014.

No water consumption impacts are associated with this measure. Any electrical costs associated with the operation of the destratification fans would be offset by the reduced use of auxiliary heating equipment such as blower motors on space heating equipment [1].

NATURAL GAS SAVINGS ALGORITHMS

The following algorithm was used to calculate the stipulated gas impact in cubic meters per fan. The total gas savings, *NG Savings*, is calculated based on the difference in heat loss through the roof before and after destratification. [2]

$$NG\ Savings = q_{bd} - q_{ad}$$

The heat loss per unit roof area through the roof before destratification is calculated in the following equation:

$$q_{bd} = U \times A \times (t_{ib} - t_o)$$

where,

- q_{bd} = Heat loss through the roof before destratification (Btu/h)
- U = Average heat transfer coefficient for the roof (Btu /ft²·°F·h)
- A = Area of roof influenced by destratification fans (ft²)
- t_{ib} = Temperature on underside of roof before destratification (°F)
- t_o = Outside air temperature (°F)

The heat loss per unit roof area through the roof after destratification is calculated in the following equation:

$$q_{ad} = U \times A \times (t_{ia} - t_o)$$

where,

- q_{ad} = Heat loss through the roof after destratification (Btu/ft²·h)
- U = Average heat transfer coefficient for the roof (Btu /ft²·°F·h)
- A = Area of roof influenced by destratification fans (ft²)
- t_{ia} = Average indoor air temperature after destratification (°F) [2]

$$t_{ia} = \frac{(t_{ib} \times H_{ah}) + (t_f \times H_{bh})}{(H_{ah} + H_{bh})} = \frac{(86.5 \times 8) + (72 \times 22)}{(22 + 8)} = 75.9^\circ F$$

where,

- t_{ib} = Temperature on underside of roof before destratification (°F)
- H_{ah} = Height above heaters to roof (ft)

- t_t = Thermostat temperature setting (°F)
- H_{bh} = Height below heaters to floor (ft)

Simplifying the equations to calculate the annual natural gas savings factor per unit area, the following equation is used:

$$NG\ Savings = \frac{hrs_{hs} \times U \times (t_{ib} - t_{ia}) \times 7,850 \frac{ft^2}{fan}\ Roof}{35,738 \frac{Btu}{m^3} \times \eta} + \frac{hrs_{hs} \times U_{wall} \times (t_{ib} - t_{ia}) \times Area\ of\ influence\ of\ fan\ in\ contact\ with\ exterior\ wall \frac{ft^2}{fan}\ Wall}{35,738 \frac{Btu}{m^3} \times \eta}$$

where,

- NG savings = Annual gas savings per unit area (m³/fan)
- hrs_{hs} = Heating season hours for this location (h)
- η = Efficiency of gas furnace

The calculated annual savings factor - Retrofit:

$$NG\ savings = \frac{5,567 \times 0.107 \times (86.5 - 75.9) \times 7,850}{35,738 \times 0.8} = 1,734 \frac{m^3}{fan}$$

The calculated annual savings factor – New Construction:

$$NG\ savings = \frac{5,567 \times 0.036 \times (86.5 - 75.9) \times 7,850}{35,738 \times 0.8} = 583 \frac{m^3}{fan}$$

ASSUMPTIONS

Table 4 provides a list of assumptions utilized in the measure savings algorithm to derive the stipulated savings values listed in Table 1 above.

Table 4. General Assumptions

Variable	Definition	Value		Source/Comments
hrs_{hs}	Heating hours per year	5,567		Based on TMY3 data for London, ON and on heating hours below 55°F (12.8 °C)
U	Average heat	Retrofit	New Construction	Codes and engineering judgment ²

² The substantiation document roof U-value should reflect the average of all buildings that receive this measure. No survey data on Ontario warehouse roof U-values was available. The current (IEC-2012) code minimum U-value for new construction is 0.032

Variable	Definition	Value		Source/Comments
	transfer coefficient for the roof	0.107 Btu/°F·h·ft ² (0.51 W/m ² ·K)	0.032 Btu/°F·h·ft ² (0.51 W/m ² ·K)	
t_{ib}	Temperature on underside roof deck before destratification	86.5°F (30.3°C)		Based on a temperature gradient of 0.426 °Cft calculated for 25 feet between the thermostat and the ceiling [1]
t_f	Space temperature setpoint	72°F (22.2°C)		Common assumptions table
H_{ah}	Height above heaters to roof	8 ft		Minimum requirements are 8 feet from floor or ceiling [3]
H_{bh}	Height below heaters to floor	22 ft		Minimum requirements are 8 feet from floor or ceiling [3]
	Effective area covered by fan	7,850 ft ²		[1]
η	Commercial heating system efficiency	80%		Common assumptions table
	Energy density of natural gas	35,738 Btu/m ³		Common assumptions table

The roof area upon which the savings is based may not exceed the manufacturer-rated maximum floor area covered by the destratification fans at their installed height.

SAVINGS CALCULATION EXAMPLE

The example below illustrates the savings value for six (6) twenty-four foot paddle destratification fans to be installed in a new commercial warehouse. The room has a 30 foot ceiling and a gas furnace set at 72°F (22.2 °C).

$$\text{Annual NG savings} = 583 \frac{\text{m}^3}{\text{fan}} \times 6 \text{ fans} = 3,498 \text{ m}^3$$

Btu/°F·h·ft² [6]. ASHRAE 90.1-1999 cites 0.036 Btu/°F·h·ft² for prescriptive use [7]. In the 1990's the ASHRAE-based code requirement was less stringent, 0.084 Btu/°F·h·ft² [8], and before this code was in effect average U-values likely were higher due to roof penetration. Insulation has been added to some older warehouses that have been re-roofed. Also, the savings calculated in this set of algorithms are based solely on reducing heat loss through the roof. There will be additional savings due to reduced heat loss through the upper part of the walls and possibly due to less stack effect-related infiltration. After consideration of all of these factors, engineering judgment was used estimate an average roof U-value (and effectively the overall UA) of 0.107 Btu/°F·h·ft².

USES AND EXCLUSIONS

This measure is restricted to fans with a minimum diameter of 20 feet for use in warehousing, manufacturing, industrial or retail buildings with a minimum of 30 foot ceilings and forced air space heating, including unit heaters. [4]

MEASURE LIFE

The measure life is 15 years [5].

INCREMENTAL COST

The purchase and installation cost for destratification fans will vary depending on the available electrical infrastructure and the need for specialty lifts for high ceilings. The approximate incremental cost (for equipment and installation) of a 24 foot destratification fan is \$8,714 [2].³

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³ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

COMMERCIAL – INCREMENTAL ENERGY RECOVERY VENTILATION (ERV) (55% EFFECTIVENESS BASELINE) – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	2
OEB Filing Date	December 22, 2017
OEB Approval Date	
Commercial → Space Heating → Incremental Energy Recovery Ventilation → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition			
Measure Category	New Construction (NC) is required by Ontario Building Code Time of Natural Replacement (TNR)			
Baseline Technology	ERV with Minimum 55% Energy Recovery Effectiveness as per Ontario Building Code 2017, Supplement SB-10 January 1, 2017			
Efficient Technology	ERV with Minimum 65% Sensible Heat Recovery Effectiveness ¹ and 63% Total Energy Recovery Effectiveness at 32°F			
	ERV with Minimum 75% with Sensible Heat Recovery Effectiveness and 73% Total Energy Recovery Effectiveness at 32°F			
	ERV with Minimum 85% Sensible Heat Recovery Effectiveness and 83% Total Energy Recovery Effectiveness at 32°F			
Market Type	Commercial			
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE} 1	Group	Average Group Gas Savings (m ³ /working CFM)

¹ This measure is eligible for commercial buildings where Energy Star does not apply (the applicable OBC code is Supplementary Standard SB-10).

Parameter	Definition			
Annual Gas Savings Rate With a Minimum ERV Sensible Heat Recovery Effectiveness of 65%, $\epsilon_{EE} 1$ (m ³ /working CFM) ²	Multi-Family, Health Care and Nursing Homes	0.94	High Use	0.94
	Hotels	0.67	Medium Use	0.52
	Restaurant	0.49		
	Retail	0.41		
	Office	0.36	Low Use	0.34
	Warehouse	0.34		
	School	0.30		
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /working CFM), $\epsilon_{EE} 2$	Group	Average Group Gas Savings (m ³ /working CFM)
Annual Natural Gas Savings With a Minimum ERV Sensible Heat Recovery Effectiveness of 75%, $\epsilon_{EE} 2$ (m ³ /working CFM) ¹	Multi-Family, Health Care and Nursing Homes	1.89	High Use	1.89
	Hotels	1.35	Medium Use	1.05
	Restaurant	0.98		
	Retail	0.82		
	Office	0.72	Low Use	0.67
	Warehouse	0.69		
	School	0.61		
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /working CFM), $\epsilon_{EE} 3$	Group	Average Group Gas Savings (m ³ /working CFM)
Annual Natural Gas Savings With a Minimum ERV Sensible Heat Recovery Effectiveness of 85%, $\epsilon_{EE} 3$ (m ³ /working CFM)	Multi-Family, Health Care and Nursing Homes	2.83	High Use	2.83
	Hotels	2.02	Medium Use	1.57
	Restaurant	1.47		
	Retail	1.23		

² No latent losses

Parameter	Definition			
working CFM) ¹	Office	1.08	Low Use	1.01
	Warehouse	1.03		
	School	0.91		
Measure Life	14 Years			
Incremental Costs (\$ CAD)	\$1.00 per CFM at ϵ_{EE} 1			
	\$2.00 per CFM at ϵ_{EE} 2			
	\$3.00 per CFM at ϵ_{EE} 3			
Restrictions	<p>This measure is not eligible in areas where:</p> <ul style="list-style-type: none"> The ERV unit has a sensible effectiveness of less than 65% at 32°F, 100% of the exhaust air must be evacuated from the building in order to avoid cross contamination, and therefore 100% fresh air is required such as described in OBC section 1.1.1.4. No recirculation is allowed by codes or standards. For instance, any limitations as per CSA Z317.2_10 (Special Requirements for Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities) Contaminants (gases and vapors) may be present and the ERV may bring them back into the breathing zone Systems where DCV or scheduled setbacks are used during operated hours³ 			

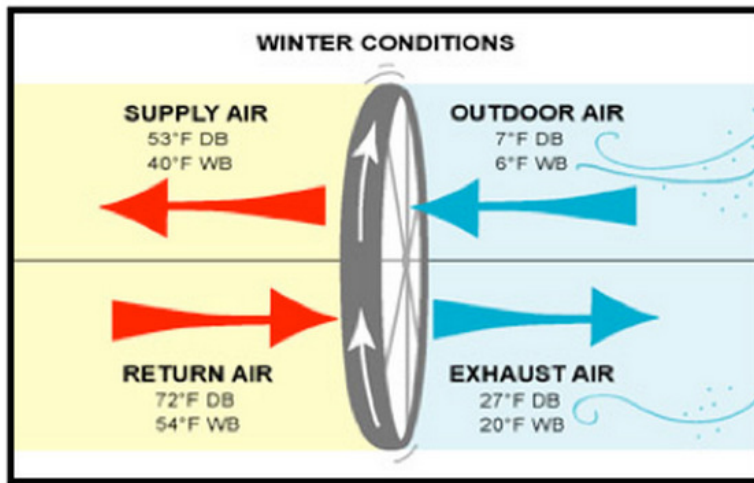
OVERVIEW

An energy recovery ventilator (ERV) refers to heat exchanger equipment that is designed to transfer heat and moisture between the building exhaust air and the outside supply air. During the heating season, this raises the temperature of the outside supply air through heat transfer within the heat exchanger and typically adjusts the humidity of the supply air through moisture transfer. By doing so, the amount of energy wasted in heat through the exhaust air stream is reduced and energy is saved through decreased load on the building heating system. ERVs are available as desiccant rotary wheels or membrane plate exchangers [1].

Figure 1 is an illustration of a wheel-type energy recovery ventilator and functionality.

³ These configurations require that projects be submitted as custom measures.

Figure 1: Energy Recovery Ventilator⁴



⁴ From <http://www.aceenergy.com/aloha/products/energy-recovery/>, 12/10/2014.

APPLICATION

The performance of the ERV can be quantified by its total effectiveness, which is a function of both its sensible and latent effectiveness. Sensible refers to heat transfer and latent refers to moisture transfer. Sensible effectiveness is defined as the ratio of actual heat energy captured to the maximum heat energy that could be captured. Latent effectiveness is defined as the ratio of actual moisture transferred to the maximum moisture that could be transferred. Total effectiveness is defined similarly as the ratio of actual energy transferred to the total energy transferred. These values are determined during testing and both vary with temperature and moisture differences. Other performance parameters to be considered are the pressure drop over the ERV, and the method of frost control [2].

BASELINE TECHNOLOGY

The baseline is considered to be a building operating with the use of an ERV as per Ontario Building Code 2017 (SB-10). [3] [4]

Table 2. Baseline for Energy Recovery Ventilators

Type	Efficiency
ERV	ERV with 55% Energy Recovery Effectiveness per Ontario Building Code (OBC)

EFFICIENT TECHNOLOGY

The efficient technology is defined as an ERV with a sensible heat recovery effectiveness of at least 65% as shown in Table 3. Note, ENERGY STAR requires that qualifying ERVs have a minimum rated sensible effectiveness of 60% at -13°F (-25°C) and 65% at 32°F (0°C) [5].

Table 3. Efficient Technology for Energy Recovery Ventilators

Type	Efficiency
ERV ε_{EE1}	ERV with Minimum 65% Sensible Heat Recovery Effectiveness and 63% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)
ERV ε_{EE2}	ERV with Minimum 75% with Sensible Heat Recovery Effectiveness and 73% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)
ERV ε_{EE3}	ERV with Minimum 85% Sensible Heat Recovery Effectiveness and 83% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)

ENERGY IMPACTS

Heat and moisture are recovered from the outgoing exhaust air and added to the incoming supply air. Natural gas savings are achieved because the supply air arrives at the building heating equipment at a higher enthalpy than it would without an ERV. This means that less energy is required to heat the supply air to the set point temperature.

There are potential cooling electric savings that are possible with an ERV. However, those savings have not been quantified.

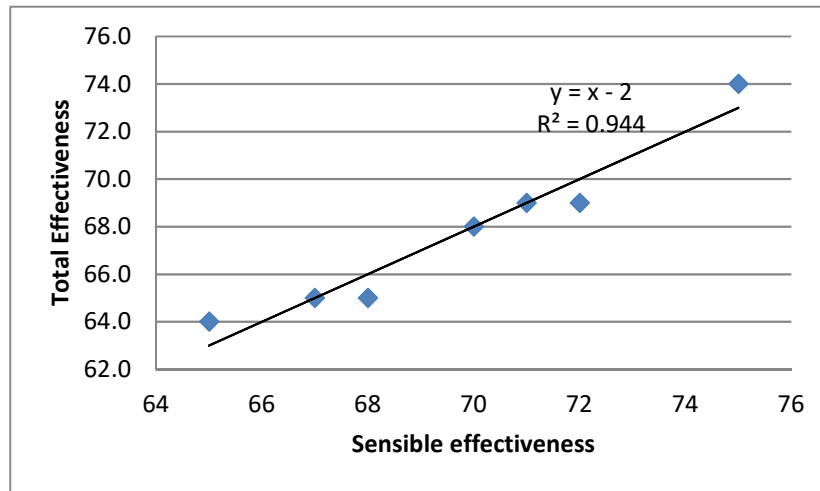
NATURAL GAS SAVINGS ALGORITHMS

The following algorithms are used to calculate the gas impact in cubic meters and are formulae from ASHRAE Heating, Ventilating and Air Conditioning Systems and Equipment Handbook 2012, chapter 26 [2]. The ASHRAE equations make the following assumptions: no vapor condensation within the ERV, no cross transfer of anything but moisture, no heat gains from fan motors, and equal supply and exhaust air flow rates.

The energy saved by an ERV is a function of the heat and moisture transfer rates through the heat exchanger and the length of time it operates. The heat and moisture transfer can be calculated from the enthalpy difference between the supply and exhaust air entering the ERV, the total effectiveness of the ERV, the physical properties of air, and the flow rate through the ERV. A defrost factor must also be considered to account for the time that exhaust air is diverted through the core in order to prevent freezing, which impedes the operation of the ERV.

Since the efficient technology is defined by the sensible heat recovery effectiveness, an assumption for the total recovery effectiveness is needed to calculate the energy savings for the measure. By comparing rated values of sensible heat recovery and total recovery effectiveness from the Air Conditioning, Heating and Refrigeration Institute (AHRI) database, [6] a relationship was developed between the two. This relationship is shown in Figure 2.

Figure 2. Total Effectiveness Versus Sensible Effectiveness



Total recovery effectiveness is approximately two percent less than heat recovery effectiveness. For instance, based on a sensible heat recovery effectiveness of 65%, a total recovery effectiveness of 63% is assumed for the efficient technology in this measure.

The natural gas savings¹ rates in Table 1 are calculated using the following formulae.

$$hrs = Heathrs \times \frac{weeklyhrs}{168 \frac{hrs}{week}}$$

and,

$$NG\ Savings = hrs \times \frac{60min}{hr} \times \frac{(\epsilon_{EE} - 53\%)}{\eta} \times \frac{\rho}{35,738 \frac{Btu}{m^3}} \times (h_3 - h_1) \times \left(1 - \frac{DF}{100\%}\right)$$

Where,

- hrs* = Annual hours that the ERV is expected to be in use (hours/year)
- Heathrs* = Number of hours in the heating season (hours/year)
- weeklyhrs* = Number of weekly operating hours (hours/week)
- $168 \frac{hrs}{week}$ = Number of hours in a week
- NG Savings* = Annual natural gas savings per CFM of ERV (m³/CFM/year)
- $\frac{60min}{hr}$ = Conversion from minutes to hours
- ϵ_{EE} = Total effectiveness of the high efficiency ERV (%)⁵
- η = The efficiency of the building's heating system (%)
- ρ = Density of air at 72°F (lb_m/ft³)

⁵ Note, for this analysis the rated total effectiveness is being used as an average total effectiveness.

- $35,738 \frac{Btu}{m^3}$ = Conversion from Btu to m³ of natural gas
 h_3 = Enthalpy of the inside (exhaust) air entering the ERV (Btu/lb)
 h_1 = Enthalpy of the outside (supply) air entering the ERV (Btu/lb)
 DF = Defrost control de-rating factor (%)
 53% = ERV Baseline Total Effectiveness

ASSUMPTIONS

Table 4 shows the list of assumptions used in the algorithms sections.

Table 4. Assumptions

Variable	Definition	Value	Source
<i>Heathrs</i>	Hours in Heating Season, 55°F Balance Temperature ⁶	5,567 hrs	Common assumptions table
ϵ_{EE1}	Total minimum effectiveness	63%	[6] and analysis in this document
ϵ_{EE2}	Total minimum effectiveness	73%	[6] and analysis in this document
ϵ_{EE3}	Total minimum effectiveness	83%	[6] and analysis in this document
ρ	Density of the exhaust air	0.0741 lb _m /ft ³	Common assumptions table
η	Efficiency of gas fired heating equipment	80%	Common assumptions table
h_1	Average enthalpy of outside (supply) air during the heating season	11.23 Btu/lb	[7], validated against psychrometric chart given rh1 / T1 and rh3 / T3 temperature and humidity (provide below).
h_3	Average enthalpy of inlet exhaust air	22.72 Btu/lb	
RH ₁	Average outdoor relative humidity	78.1%	[8]
RH ₃	Average indoor relative humidity	30%	[9], [2]

⁶ The annual heating hours, and average outside air temperature, assume an average building balance temperature of 55°F, which is the temperature at which neither heating nor cooling is required. The actual balance point for a particular application will vary based on building construction, internal loads, HVAC system zoning, and other factors.

Variable	Definition	Value	Source
<i>DF</i>	Defrost control de-rating factor	5% ⁷	[1] [2] [10] [9]
T1	Average temperature of outside (supply) air during the heating season (OA temperature heating system enabled)	33.03°F	Common assumptions table
T3	Average temperature of inlet exhaust air (Space temperature setpoint)	72°F	Common assumptions table

The assumed weekly hours of operation for different building types are given in Table 5.

Table 5. Hours of Weekly Operation [9]

Building Type	Hours of Operation per Week
Multi-Family	168
Health Care	168
Nursing Home	168
Hotel	120
Restaurant	87
Retail	73
Office	64
Warehouse	61
School	54

EXAMPLE

For this example, it will be assumed that a new health care facility installs an ERV unit working at 500 CFM with a total effectiveness of 73%. In this case the ϵ_{EE2} is applicable.

⁷ All air-to-air heat recovery equipment requires frost control in colder climates to prevent freeze-up of exhaust air condensate on heat exchange components. There are different types of frost control methods and depending on the defrost control system, annual heat recovery estimates should be reduced by 5% to 15%. The cited Nexant document specifically considers the factor for Ontario (p. 6-47 and 6-48) and recommends 5% as a conservative value for the base case scenario.

$$hrs = 5,567hrs \times \frac{168 \frac{hrs}{week}}{168 \frac{hrs}{week}} = 5,567 \frac{hrs}{year}$$

and,

$$NG Savings = 5,567 \frac{hrs}{year} \times \frac{60 min}{hr} \times 0.0741 \frac{lb_m}{ft^3} \times \frac{(73\% - 53\%)}{80\%} \times \frac{1}{35,738 \frac{Btu}{m^3}} \\ \times \left(22.72 \frac{Btu}{lb_m} - 11.23 \frac{Btu}{lb_m} \right) \times \left(1 - \frac{5\%}{100\%} \right) = 1.89 \frac{m^3}{CFM \cdot year}$$

Therefore,

$$NG Savings = 500CFM \times 1.89 \frac{m^3}{CFM \cdot year} = 945 \frac{m^3}{year}$$

USES AND EXCLUSIONS

Note measure is intended for buildings with an existing ERV, or new construction buildings required to have an energy recovery system. For buildings without an existing ERV, or new buildings not required to have an energy recovery system, please see supporting measure with no ERV baseline. Also:

- Measure not applicable to areas and rooms where 100% fresh air is required.
- Measure not applicable to areas and rooms where no recirculation is allowed by codes or standards. For instance, CSA Z317.2_10 (Special Requirements for Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities).
- Measure not applicable to areas and rooms where contaminants (gases and vapors) may be present and the ERV may bring them back into the breathing zone.
- Measure not applicable to systems where no DCV or scheduled setbacks are required.

MEASURE LIFE

A 14-year measure life is recommended by DEER is based on KEMA-XENERGY's Retention Study of PG&Es 1996-1997 Energy Incentive Program. This study tracked installed equipment over 6 years and used statistical analysis to calculate EUL [11].

INCREMENTAL COST

The incremental costs, representing differences in equipment costs, between baseline units meeting minimum code efficiency and high efficiency units are \$1.00 per cfm at 65%, \$2.00 at 75%, and \$3.00 at 85% efficiency⁸ [12]

REFERENCES

- [1] Natural Resources Canada, "Heat/Energy Recovery Ventilators," 2 2012. [Online]. Available:
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. [Accessed 11 2013].
- [2] ASHRAE Handbook, "Heating, Ventilating and Air Conditioning Systems and Equipment, 22, 26, and 28," 2012. [Online]. Available:
<http://handbook.ashrae.org/Handbook.aspx>. [Accessed Oct 2014].
- [3] "Ontario Building Code Act 1992 - Supplementary Standard SB-10," 14 September 2012. [Online].
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- [5] ENERGY STAR, "Technical Specifications for Residential Heat Recovery Ventilators and Energy Recovery Ventilators (H/ERVs) Version 2.0", 2015. [Online]. Available: <http://www.nrcan.gc.ca/energy/products/for-participants/specifications/13695>. [Accessed Nov 2017].
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- [7] W. Jayes, "Psychrometric Calculations," The Sugar Engineers, [Online]. Available: <http://www.sugartech.co.za/psychro/index.php>. [Accessed Nov 2014].
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⁸ Based on a manufacturer's estimate that typical incremental installed cost premium for 85% efficiency heat recovery units are \$3.00 /cfm greater than for 50% efficiency units.

https://energyplus.net/weather-location/north_and_central_america_wmo_region_4/CAN/ON/CAN_ON_London.716230_CWEC. [Accessed Oct 2014].

- [9] Nexant, "Evaluation of Natural Gas DSM Measures: ERVs & HRVs," March 12 2010.
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COMMERCIAL – INCREMENTAL ENERGY RECOVERY VENTILATION (ERV) (NO ERV BASELINE) – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	2
OEB Filing Date	December 22, 2017
OEB Approval Date	
Commercial → Space Heating → Incremental Energy Recovery Ventilation → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definitions			
Measure Category	New construction (NC), ERV not required by Ontario Building Code Retrofit (R)			
Baseline Technology	No ERV			
Efficient Technology	ERV with Minimum 55% Sensible Heat Recovery Effectiveness ¹ and 53% Total Energy Recovery Effectiveness at 32°F			
	ERV with Minimum 65% Sensible Heat Recovery Effectiveness and 63% Total Energy Recovery Effectiveness at 32°F			
	ERV with Minimum 75% with Sensible Heat Recovery Effectiveness and 73% Total Energy Recovery Effectiveness at 32°F			
	ERV with Minimum 85% Sensible Heat Recovery Effectiveness and 83% Total Energy Recovery Effectiveness at 32°F			
Market Type	Commercial			
Annual Gas Savings Rate With a Minimum ERV Sensible Heat Recovery Effectiveness of 55%,	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE} 1	Group	Average Group Gas Savings (m ³ /working CFM), ϵ_{EE} 1
	Multi-Family, Health Care and Nursing	5.01	High Use	5.01

¹ This measure is eligible for commercial buildings where Energy Star does not apply (the applicable OBC code is Supplementary Standard SB-10).

Some commercial buildings are required by SB-10 to have Energy Recovery Ventilation or Heat Recovery Ventilation with a minimum of 55% sensible effectiveness. For buildings with no code requirement, systems that bring efficiency up to code level (55% sensible effectiveness) are eligible.

Parameter	Definitions			
$\varepsilon_{EE} 1$ (m ³ / working CFM) ¹	Homes			
	Hotels	3.58	Medium Use	2.78
	Restaurant	2.59		
	Retail	2.18		
	Office	1.91	Low Use	1.78
	Warehouse	1.82		
	School	1.61		
Annual Gas Savings Rate With a Minimum ERV Sensible Heat Recovery Effectiveness of 65%, $\varepsilon_{EE} 2$ (m ³ / working CFM) ¹	Building Type	Gas Savings Rate (m³/working CFM), $\varepsilon_{EE} 2$	Group	Average Group Gas Savings (m³/working CFM), $\varepsilon_{EE} 2$
	Multi-Family, Health Care and Nursing Homes	5.95	High Use	5.95
	Hotels	4.25	Medium Use	3.31
	Restaurant	3.08		
	Retail	2.59		
	Office	2.27	Low Use	2.11
	Warehouse	2.16		
School	1.91			
Annual Gas Savings Rate With a Minimum ERV Sensible Heat Recovery Effectiveness of 75%, $\varepsilon_{EE} 3$ (m ³ / working CFM) ¹	Building Type	Gas Savings Rate (m³/working CFM), $\varepsilon_{EE} 3$	Group	Average Group Gas Savings (m³/working CFM), $\varepsilon_{EE} 3$
	Multi-Family, Health Care and Nursing Homes	6.90	High Use	6.90
	Hotels	4.93	Medium Use	3.83
	Restaurant	3.57		
	Retail	3.00		
	Office	2.63	Low Use	2.45
	Warehouse	2.50		
School	2.22			
Annual Gas Savings Rate	Building Type	Gas Savings Rate	Group	Average Group Gas Savings

Parameter	Definitions			
With a Minimum ERV Sensible Heat Recovery Effectiveness of 85%, ϵ_{EE}^4 (m ³ /working CFM) ¹		(m ³ /working CFM), ϵ_{EE}^4		(m ³ /working CFM), ϵ_{EE}^4
	Multi-Family, Health Care and Nursing Homes	7.84	High Use	7.84
	Hotels	5.60	Medium Use	4.36
	Restaurant	4.06		
	Retail	3.41		
	Office	2.99	Low Use	2.79
	Warehouse	2.85		
	School	2.52		
Annual Electric Penalty ² (kWh/working CFM)	Building Type	Electric Penalty Rate (kWh/working CFM)	Group	Average Group Electric Penalty (kWh/working CFM)
	Multi-Family, Health Care and Nursing Homes	4.62	High Use	4.62
	Hotels	3.30	Medium Use	2.57
	Restaurant	2.39		
	Retail	2.01		
	Office	1.76	Low Use	1.64
	Warehouse	1.68		
	School	1.49		
Measure Life	14 Years			
Incremental First Cost (\$ CAD) ϵ_{EE}^1	Integrated ERV		Standalone or Bolt-On ERV	
	\$4.86/CFM		\$7.80/CFM	
Incremental Cost (\$ CAD)	\$4.86 + \$1.00 per CFM at ϵ_{EE}^2		\$7.80 + \$1.00 per CFM at ϵ_{EE}^2	
	\$4.86 + \$2.00 per CFM at ϵ_{EE}^3		\$7.80 + \$2.00 per CFM at ϵ_{EE}^3	
	\$4.86 + \$3.00 per CFM at ϵ_{EE}^4		\$7.80 + \$3.00 per CFM at ϵ_{EE}^4	

² The electric penalty does not apply when the ERV unit is installed as part of an integrated HVAC package.

Restrictions	<p>This measure is not eligible in areas where:</p> <ul style="list-style-type: none"> • ERV is required by building code, • 100% of the exhaust air must be evacuated from the building in order to avoid cross contamination, and therefore 100% fresh air is required such as described in OBC section 1.1.1.4. • No recirculation is allowed by codes or standards. For instance, any limitations as per CSA Z317.2_10 (Special Requirements for Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities), • Contaminants (gases and vapors) may be present and the ERV may bring them back into the breathing zone• • Systems where DCV or scheduled setbacks are used during operated hours³
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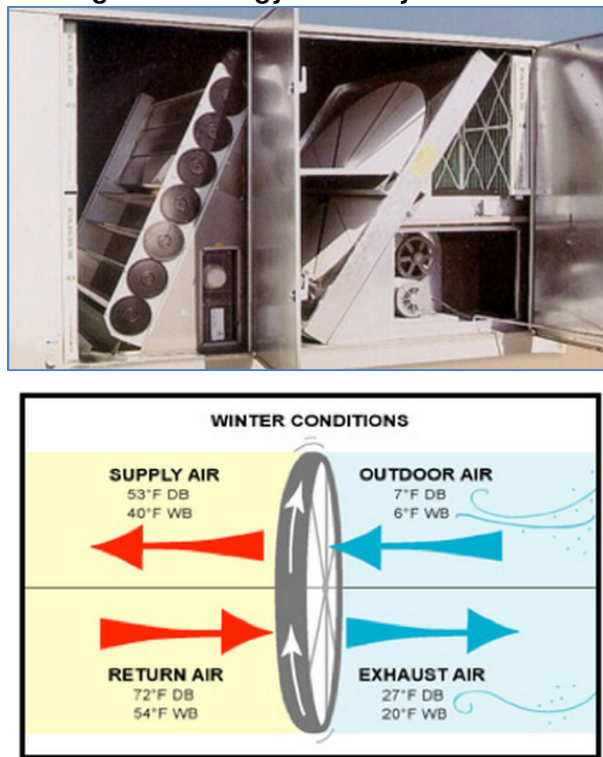
OVERVIEW

An energy recovery ventilator (ERV) refers to heat exchanger equipment that is designed to transfer heat and moisture between the building exhaust air and the outside supply air. During the heating season, this raises the temperature of the outside supply air through heat transfer within the heat exchanger and typically adjusts the humidity of the supply air through moisture transfer. By doing so, the amount of energy wasted in heat through the exhaust air stream is reduced and energy is saved through decreased load on the building heating system. ERVs are available as desiccant rotary wheels or membrane plate exchangers. [1].

One of the components of ERVs is circulation fans, which are typically high efficiency electrically commutated motors. These will consume more electrical energy in cases where the ERV unit is added to the existing HVAC system as a standalone or bolt-on unit [1]. No penalty is assigned if the ERV is integrated as part of the HVAC packaged system installed in new construction because the higher efficiency of the new fans compensates for the additional static pressure. Figure 1 is an illustration of a wheel-type energy recovery ventilator and functionality.

³ These configurations require that projects be submitted as custom measures.

Figure 1: Energy Recovery Ventilator⁴



APPLICATION

The performance of the ERV can be quantified by its total effectiveness, which is a function of both its sensible and latent effectiveness'. Sensible refers to heat transfer and latent refers to moisture transfer. Sensible effectiveness is defined as the ratio of actual heat energy captured to the maximum heat energy that could be captured. Latent effectiveness is defined as the ratio of actual moisture transferred to the maximum moisture that could be transferred. Total effectiveness is defined similarly as the ratio of actual energy transferred to the total energy transferred. These values are determined during testing and both vary with temperature and moisture differences. Other performance parameters to be considered are the pressure drop over the ERV, and the method of frost control [2].

BASELINE TECHNOLOGY

The baseline is considered to be a building operating without the use of an ERV as shown in Table 2. This implies that no energy recovery is taking place between the incoming outside supply air and the exhausting inside air.

⁴ From <http://www.acelaenergy.com/aloha/products/energy-recovery/>, 12/10/2014.

Table 2. Baseline for Energy Recovery Ventilators

Type	Efficiency
No ERV	No Energy Recovery

EFFICIENT TECHNOLOGY

The efficient technology is defined as an ERV with a sensible heat recovery effectiveness of 55%, 65%, 75%, and 85% as shown in Table 3. Note, ENERGY STAR requires that qualifying ERVs have a minimum rated sensible effectiveness of 60% at -13°F (-25°C) and 65% at 32°F (0°C) [3].

Table 3. Efficient Technology for Energy Recovery Ventilators

Type	Efficiency
ERV ϵ_{EE1}	Minimum 55% Sensible Heat Recovery Effectiveness and 53% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)
ERV ϵ_{EE2}	Minimum 65% Sensible Heat Recovery Effectiveness and 63% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)
ERV ϵ_{EE3}	Minimum 75% with Sensible Heat Recovery Effectiveness and 73% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)
ERV ϵ_{EE4}	Minimum 85% Sensible Heat Recovery Effectiveness and 83% Total Energy Recovery Effectiveness at 32°F at working airflow (CFM)

ENERGY IMPACTS

Heat and moisture are recovered from the outgoing exhaust air and added to the incoming supply air. Natural gas savings are achieved because the supply air arrives at the building heating equipment at a higher enthalpy than it would without an ERV. This means that less energy is required to heat the supply air to the set point temperature.

An electrical penalty is incurred due to the operation of ERV fans or increased load on central fans, except when the ERV is integrated as part of the HVAC package. There are potential cooling electric savings that are possible with an ERV. However, those savings have not been quantified.

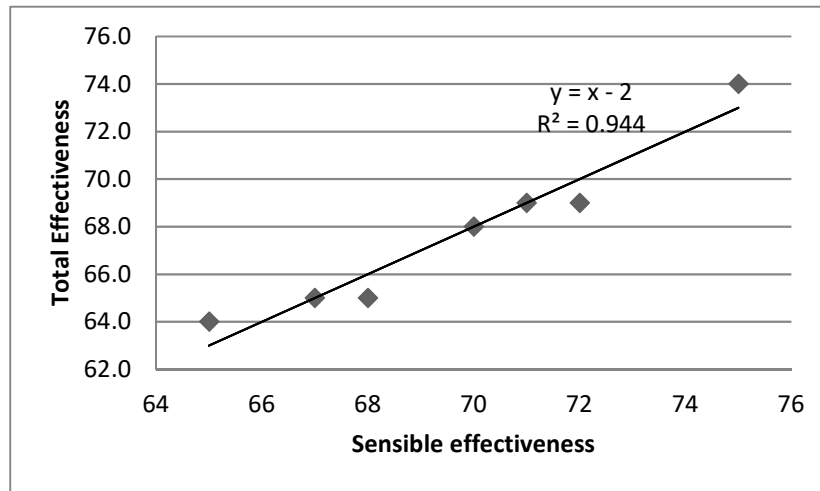
NATURAL GAS SAVINGS ALGORITHMS

The following algorithms are used to calculate the gas impact in cubic meters and are formulae from ASHRAE Heating, Ventilating and Air Conditioning Systems and Equipment Handbook 2012, chapter 26 [2]. The ASHRAE equations make the following assumptions: no vapor condensation within the ERV, no cross transfer of anything but moisture, no heat gains from fan motors, and equal supply and exhaust air flow rates.

The energy saved by an ERV is a function of the heat and moisture transfer rates through the heat exchanger and the length of time it operates. The heat and moisture transfer can be calculated from the enthalpy difference between the supply and exhaust air entering the ERV, the total effectiveness of the ERV, the physical properties of air, and the flow rate through the ERV. A defrost factor must also be considered to account for the time that exhaust air is diverted through the core in order to prevent freezing, which impedes the operation of the ERV.

Since the efficient technology is defined by the sensible heat recovery effectiveness, an assumption for the total recovery effectiveness is needed to calculate the energy savings for the measure. By comparing rated values of sensible heat recovery and total recovery effectiveness from the Air Conditioning, Heating and Refrigeration Institute (AHRI) database, [4] a relationship was developed between the two. This relationship is shown in Figure 2.

Figure 2. Total Effectiveness Versus Sensible Effectiveness



Total recovery effectiveness is approximately two percent less than heat recovery effectiveness.

The natural gas savings¹ rates in Table 1 are calculated using the following formulae.

$$hrs = Heathrs \times \frac{weeklyhrs}{168 \frac{hrs}{week}}$$

and,

$$NG\ Savings = hrs \times \frac{60min}{hr} \times \frac{\epsilon\epsilon_{EE}}{\eta} \times \frac{\rho}{35,738 \frac{Btu}{m^3}} \times (h_3 - h_1) \times \left(1 - \frac{DF}{100\%}\right)$$

Where,

- hrs* = Annual hours that the ERV is expected to be in use (hours/year)
- Heathrs* = Number of hours in the heating season (hours/year)
- weeklyhrs* = Number of weekly operating hours (hours/week)
- $168 \frac{hrs}{week}$ = Number of hours in a week
- NG Savings* = Annual natural gas savings per CFM of ERV (m³/CFM/year)
- $\frac{60min}{hr}$ = Conversion from minutes to hours
- $\epsilon\epsilon_{EE}$ = Total effectiveness of the high efficiency ERV (%)⁵
- η = The efficiency of the building's heating system (%)
- ρ = Density of air at 72°F (lb_m/ft³)

⁵ Note, for this analysis the rated total effectiveness is being used as an average total effectiveness.

- $35,738 \frac{Btu}{m^3}$ = Conversion from Btu to m³ of natural gas
 h_3 = Enthalpy of the inside (exhaust) air entering the ERV (Btu/lb)
 h_1 = Enthalpy of the outside (supply) air entering the ERV (Btu/lb)
 DF = Defrost control de-rating factor (%)

ELECTRIC ENERGY PENALTY ALGORITHMS (FOR ERVs ADDED TO AN EXISTING SYSTEM)

The electric penalty is based on the ENERGY STAR minimum fan efficiency requirements of 0.83 W/CFM. Using this value, and the calculated hours of ERV operation from the natural gas algorithms, the kWh electric penalty can be calculated using the following equation.

The kWh fan penalty analysis presumes that the system has an automatic bypass damper so that there is no added pressure drop during hours when heat recovery is not needed.

$$kWh \text{ penalty} = 0.83 \frac{W}{CFM} \times hrs \div 1000 \frac{W}{kW}$$

Where,

- $kWh \text{ penalty}$ = The annual electric penalty per CFM of ERV capacity (kWh/CFM/year)
 $0.83 \frac{W}{CFM}$ = Minimum efficacy to be qualified for ENERGY STAR (1.20 CFM/W)
 hrs = Annual hours that the ERV is expected to be in use (hours/year)

ASSUMPTIONS

Table 4 shows the list of assumptions used in the algorithms sections.

Table 4. Assumptions

Variable	Definition	Value	Source
<i>Heathrs</i>	Hours in Heating Season, 55°F Balance Temperature ⁶	5,567 hrs	Common assumptions table

⁶ The annual heating hours, and average outside air temperature, assume an average building balance temperature of 55°F, which is the temperature at which neither heating nor cooling is required. The actual balance point for a particular application will vary based on building construction, internal loads, HVAC system zoning, and other factors.

Variable	Definition	Value	Source
ε_{EE1}	Total minimum effectiveness	53%	[4] and analysis in this document
ε_{EE2}	Total minimum effectiveness	63%	[4] and analysis in this document
ε_{EE3}	Total minimum effectiveness	73%	[4] and analysis in this document
ε_{EE4}	Total minimum effectiveness	83%	[4] and analysis in this document
ρ	Density of the exhaust air	0.0741 lb _m /ft ³	Common assumptions table
η	Efficiency of gas fired heating equipment	80%	Common assumptions table
h_1	Average enthalpy of outside (supply) air during the heating season	11.23 Btu/lb	[5], validated against psychrometric chart given rh1 / t1 and rh3 / t3 temperature and humidity (provide below).
h_3	Average enthalpy of inlet exhaust air	22.72 Btu/lb	
Fan Efficiency	Assumed fan efficiency	0.83 W/CFM	[3]
RH ₁	Average outdoor relative humidity	78.1%	[6]
RH ₃	Average indoor relative humidity	30%	[7], [2]
DF	Defrost control de-rating factor	5% ⁷	[1] [2] [8] [7]
T_1	Average temperature of outside (supply) air during the heating season (OA temperature heating system enabled)	33.03 °F	Common assumptions table
T_3	Average temperature of inlet exhaust air (space temperature setpoint)	72 °F	Common assumptions table

The assumed weekly hours of operation for different building types are given in Table 5.

⁷ All air-to-air heat recovery equipment requires frost control in colder climates to prevent freeze-up of exhaust air condensate on heat exchange components. There are different types of frost control methods and depending on the defrost control system, annual heat recovery estimates should be reduced by 5% to 15%. The cited Nexant document specifically considers the factor for Ontario (p. 6-47 and 6-48) and recommends 5% as a conservative value.

Table 5. Hours of Weekly Operation [7]

Building Type	Hours of Operation per Week
Multi-Family	168
Health Care	168
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Hotel	120
Restaurant	87
Retail	73
Office	64
Warehouse	61
School	54

EXAMPLE

For this example, it is assumed that a new health care facility installs an ERV unit working at 500 CFM with a total effectiveness of 63%. In this case the ϵ_{EE2} is applicable.

$$hrs = 5,567 \frac{hrs}{week} \times \frac{168 \frac{hrs}{week}}{168 \frac{hrs}{week}} = 5,567 \frac{hrs}{year}$$

and,

$$NG \text{ Savings} = 5,567 \frac{hrs}{year} \times \frac{60 \text{ min}}{hr} \times 0.0741 \frac{lb_m}{ft^3} \times \frac{63\%}{80\%} \times \frac{1}{35,738 \frac{Btu}{m^3}} \\ \times \left(22.72 \frac{Btu}{lb_m} - 11.23 \frac{Btu}{lb_m} \right) \times \left(1 - \frac{5\%}{100\%} \right) = 5.95 \frac{m^3}{CFM \cdot year}$$

Therefore,

$$NG \text{ Savings} = 500 \text{ CFM} \times 5.95 \frac{m^3}{CFM \cdot year} = 2,977 \frac{m^3}{year}$$

The electrical penalty can be calculated as the following.

$$kWh \text{ penalty} = 500 \text{ CFM} \times 0.83 \frac{W}{CFM} \times 5,567 \frac{hrs}{year} \times \frac{1 \text{ kW}}{1000 \text{ W}} = 2,310 \frac{kWh}{year}$$

USES AND EXCLUSIONS

- Restriction for New Building Construction: This measure is not applicable to buildings in which an ERV is required by Ontario Building Code. [9] Note please see supporting measure that utilizes code minimum as baseline for these scenarios.
- Restriction for New Building Construction: This measure is not applicable to systems serving health care spaces indicated in Table 1 because heat recovery is required by CSA Z317.2-01

MEASURE LIFE

A 14-year measure life is recommended by DEER and is based on KEMA-XENERGY’s Retention Study of PG&Es 1996-1997 Energy Incentive Program. This study tracked installed equipment over 6 years and used statistical analysis to calculate EUL [10].

INCREMENTAL COST

Table 6 demonstrates the first incremental cost of energy recovery ventilators. The first incremental costs were developed by ERS using RSMeans and were corroborated with manufacturer data. The costs for integrated systems were found to be \$4.86/CFM for ERVs integrated into HVAC systems and \$7.80/CFM for standalone systems [11]. The increased cost from integrated to standalone or bolt-on systems is due to the additional materials and equipment required and the added labor for integrating the standalone or bolt-on system with the existing ventilation system.

The first costs represent the incremental costs between no ERV and 55% efficient units. Additional incremental costs between high efficiency units are \$1.00 per CFM at 65%, \$2.00 at 75%, and \$3.00 at 85% efficiency⁸ [12].

Table 6. Incremental Cost⁹ [11]

Measure Type	Cost
First Cost Integrated units	\$4.86/CFM
First Cost Bolted-on systems	\$7.80/CFM

⁸ Based on a manufacturer’s estimate that typical incremental installed cost premium for 85% efficiency heat recovery units are \$3.00 /cfm greater than for 50% efficiency units.

⁹ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 11/30/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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COMMERCIAL ENERGY STAR CONVECTION OVEN - NEW CONSTRUCTION AND TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Food Service → ENERGY STAR Convection Oven – Full Size → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definitions
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)
Baseline Technology	A conventional, full-size convection oven
Efficient Technology	A full-size ENERGY STAR rated convection oven
Market type	Commercial
Annual Natural Gas Savings (m ³)	865 m ³
Annual Electric Savings (kWh)	40.1 kWh
Measure Life	12 years
Incremental Cost (\$ CAD)	There are no incremental costs associated with this measure.
Restrictions	Restricted to full sized convection ovens using natural gas.

OVERVIEW

Convection ovens are used in commercial and institutional food service preparation as an alternative to conventional ovens. As food cooks in a conventional oven, it is surrounded by a layer of cooler air due to the lower temperature of the food item(s) being cooked. Convection ovens differ from conventional ovens in that a motorized fan (or blower) pulls in air from the oven cavity, heats it, and distributes it back into the

oven cavity, resulting in a faster and more even cooking process. Convection ovens are thermostatically controlled appliances. The oven is left on during operations and cycles on and off to maintain the desired temperature setting. [1] This measure focuses on full size commercial convection ovens. Convection ovens consume natural gas when they are pre-heating, idling and cooking. “Standard gas convection ovens have a 30% cooking energy efficiency and an idle energy rate of 19,000 Btu/h, whereas ENERGY STAR certified gas convection ovens must meet the specification requirements of 46% cooking energy efficiency and idle energy rate of 12,000 Btu/h.” [2]

APPLICATION

This measure applies to the installation of a full size ENERGY STAR qualifying convection oven in commercial and industrial food processing settings. Convection ovens are designed to cook food within a heated enclosed space, with the food being manually placed into the oven and removed when the cooking process is complete.

BASELINE TECHNOLOGY

The baseline technology is a full size convection oven that is not ENERGY STAR rated.

EFFICIENT TECHNOLOGY

The efficient technology is a full size convection oven that is ENERGY STAR rated. Table 2 shows the requirements for this measure.

Table 2. Efficient Technology [2]

Type	ENERGY STAR Requirements
ENERGY STAR Convection Oven – Full Size	Idle rate ≤ 12,000 Btu/hr and cooking energy efficiency of ≥ 46%

ENERGY IMPACTS

The primary energy impact associated with the installation of a full-size ENERGY STAR convection oven is a reduction in natural gas required during pre-heating, idling and cooking. ENERGY STAR qualified gas convection ovens must meet the specification requirements of 46% cooking energy efficiency and idle energy rate of 12,000 Btu/h. The savings are achieved through reduced cooking time and lower idle energy rate.

There are electric savings resulting from decreased operating hours of the convection fan due to the reduced cooking time.

NATURAL GAS SAVINGS ALGORITHM

The energy savings algorithm compares the annual energy usage of the standard convection equipment and ENERGY STAR qualifying convection ovens. To determine

total energy usage, the calculation must determine the energy consumed in the pre-heating, cooking, and idling modes.

The algorithm is based upon the methodology utilized by the Food Service Technology Center. The calculation to determine the energy usage of baseline and ENERGY STAR ovens is as follows:

$$NG\ Usage = Days \times (Daily\ Preheat + Daily\ Idle + Daily\ Cooking)$$

where,

- NG Usage = the amount of natural gas used by the oven annually in Btu/year
- Days = the number of days per year the oven is in use
- Daily Preheat = the amount of natural gas used to preheat the oven daily in Btu/day
- Daily Idle = the amount of natural gas used when the oven is in idle mode in Btu/day
- Daily Cooking = the amount of natural gas used when the oven is cooking in Btu/day

The “Daily Idle” usage is calculated by the following equation:

$$Daily\ Idle = Idle\ Time \times Idle\ Rate$$

where,

- Idle Time = length of time the unit is idle per day in hours.
- Idle Rate = energy consumed during idling in Btu/hr

The idle time is calculated by subtracting the preheat time and the times the ovens are in heavy load cooking mode from the number of hours the equipment is on per day. This is shown in the following expression:

$$Idle\ Time = Total\ Operating\ Hours - Preheat\ Time - Daily\ Cooking\ Time$$

where,

- Total Operating Hours = length of time in hours where unit is turned on
- Preheat Time = length of time in hours when unit is in preheat mode
- Daily Cooking Time = length of time in hours where unit is cooking

The daily cooking time is calculated with the following equation:

$$Daily\ Cooking\ Time = \frac{Food\ Weight}{Production\ Capacity}$$

where,

- Food Weight = average quantity of food cooked in unit per day in lbs/day
- Production capacity = the maximum production rate of the appliance while cooking in accordance with the heavy-load cooking test in lbs/hr

Finally, the daily energy consumed during cooking is calculated as follows:

$$\text{Daily Cooking Time} = \frac{\text{Food Weight} \times \text{ASTM Energy to Food Rate}}{\text{Efficiency}}$$

where,

- Food Weight = average quantity of food cooked in unit per day in lbs
- ASTM Energy to Food Rate = rate at which energy is transferred to food in Btu/lb
- Efficiency = efficiency of the unit

The savings is then calculated from the difference between the baseline and efficient cases.

$$NG_{savings} = (NG\ Usage_{baseline} - NG\ Usage_{ENERGY\ STAR}) \times \frac{1m^3}{35,738\ Btu}$$

where,

- $NG_{savings}$ = annual reduction in natural gas consumption in m³/year
- $NG\ Usage_{baseline}$ = annual energy usage of a conventional oven in Btu/year
- $NG\ Usage_{ENERGY\ STAR}$ = annual energy usage for an ENERGY STAR oven in Btu/year

ELECTRIC SAVINGS ALGORITHMS

The electric savings result from the reduction in fan energy from the reduced cooking time. The electric savings are calculated as follows:

$$\begin{aligned} Elec_{savings} = & (\text{Daily Cooking Time}_{Conventional} - \text{Daily Cooking Time}_{ENERGY\ STAR}) \\ & \times HP_{fan} \times 0.7457 \frac{kW}{hp} \times Days \end{aligned}$$

Where,

$Elec_{Savings}$ = annual reduction in electric consumptions in kWh/year

$Daily\ Cooking\ Time_{Conventional}$ = Cooking time for a conventional convection oven in hours

$Daily\ Cooking\ Time_{ENERGY\ STAR}$ = Cooking time for an ENERGY STAR convection oven in hours

HP_{fan} = Horsepower of convection fan

Days = the number of days per year the oven is in use

ASSUMPTIONS

The assumptions used to calculate natural gas savings are shown in Table 3.

Table 3. Assumptions

Parameter	Baseline	High Efficiency	Source
Food service days per year	312		Common assumptions table
Preheat Time (hrs)	0.20		[3]
Total Operating Hours (hrs)	12		[4]
Preheat Energy (Btu/day)	19,000	11,000	[5]
Idle Time (hrs/day)	10.4	10.6	Calculated
Idle Rate (Btu/hr)	18,000	11,758	[5]
Food Weight (lbs/day)	100		[5]
ASTM Energy to Food Rate (Btu/lb)	250		[5], [6], [7]
Production Capacity (lbs/hr)	70	83	[5]
Efficiency	30%	46%	[2]
Convection oven fan power ¹	0.75 hp		
Energy density of natural gas	35,738 Btu/m ³		Common assumptions table

¹ Looking at several manufacturers' websites, the convection fan range in size from 0.5 hp to 0.75 horsepower. (<http://montaguecompany.com/uploads/documents/Vectaire-Full-Size-Gas-Convection-Double-Oven-Models-2-70-and-2-115-Spec-Sheet.pdf>, <http://www.centralrestaurant.com/Gas-Convection-Oven---Double-Stack-120000-BTU-Snorkel-Gas-c105p29049.html>, http://www.garland-group.com/docs/uploaded/gar/products/G_GO_SS_CONVECTION_MC0G10SD.pdf, http://www.blodgett.com/blodgett_products/dfg-100-es/)

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for an ENERGY STAR convection oven – full size with typical hours of usage.

Daily Conventional Convection Oven Usage:

$$\text{Daily Preheat} = 19,000 \frac{\text{Btu}}{\text{day}}$$

$$\text{Daily Cooking Time} = \frac{100 \frac{\text{lbs}}{\text{day}}}{70 \frac{\text{lbs}}{\text{hr}}} = 1.43 \frac{\text{hrs}}{\text{day}}$$

$$\text{Idle Time} = 12 \frac{\text{hrs}}{\text{day}} - 0.2 \frac{\text{hrs}}{\text{day}} - 1.43 \frac{\text{hrs}}{\text{day}} = 10.4 \frac{\text{hrs}}{\text{day}}$$

$$\text{Daily Idle} = 10.4 \frac{\text{hrs}}{\text{day}} \times 18,000 \frac{\text{Btu}}{\text{hr}} = 186,686 \frac{\text{Btu}}{\text{day}}$$

$$\text{Daily Cooking} = \frac{100 \frac{\text{lbs}}{\text{day}} \times 250 \frac{\text{Btu}}{\text{lb}}}{30\%} = 83,333 \frac{\text{Btu}}{\text{day}}$$

$$\text{NG Usage} = \left(19,000 \frac{\text{Btu}}{\text{day}} + 186,686 \frac{\text{Btu}}{\text{day}} + 83,333 \frac{\text{Btu}}{\text{day}} \right) \times 312 \frac{\text{days}}{\text{year}} = 90,173,943 \frac{\text{Btu}}{\text{year}}$$

Daily ENERGY STAR Convection Oven Usage:

$$\text{Daily Preheat} = 11,000 \frac{\text{Btu}}{\text{day}}$$



Gas Convection Oven Life-Cycle Cost Calculator

[About](#) | [How To Use](#) | [Definitions](#)

User Inputs			
Choose an Oven: (optional)	User Input Oven	Base Efficiency Oven	Energy Efficient Oven
-- Brand --	-- Model --		
User Inputs			
Oven Performance (Based on ASTM Standard Test Method F1496)			
Oven Size (Select from Box at Right)	Full Size	Full Size	Full Size
Preheat Energy (Btu)	19000	19000	11000
Idle Energy Rate (Btu/h)	18000	18000	11758
Heavy-Load Energy Efficiency (%)	30.0	30.0	45.0
Production Capacity (lbs/h)	70.0	70.0	83.0
Oven Usage			
Operating Hours per Day (h/day)	12.0	12.0	12.0
Operating Days per Year (d/year)	365	365	365
Number of Preheats per Day (#/day)	1	1	1
Pounds of Food Cooked per Day (lbs/day)	100.0	100.0	100.0
Utility Cost and Lifespan			
Choose State (Optional)	CA	CA	CA
Gas Cost per Therm (\$/therm)	0.916	0.916	0.916
Lifespan of Oven in Years (years)	12.0	12.0	12.0
Discount Rate (%/year)	0.00	0.00	0.00
<input type="button" value="Calculate"/> <input type="button" value="Reset Fields"/>			
Annual Results			

$$\text{Daily Cooking Time} = \frac{100 \frac{\text{lbs}}{\text{day}}}{83 \frac{\text{lbs}}{\text{hr}}} = 1.20 \frac{\text{hrs}}{\text{day}}$$

$$\text{Idle Time} = 12 \frac{\text{hrs}}{\text{day}} - 0.2 \frac{\text{hrs}}{\text{day}} - 1.20 \frac{\text{hrs}}{\text{day}} = 10.6 \frac{\text{hrs}}{\text{day}}$$

$$\text{Daily Idle} = 10.6 \frac{\text{hrs}}{\text{day}} \times 11,758 \frac{\text{Btu}}{\text{hr}} = 124,578 \frac{\text{Btu}}{\text{day}}$$

$$\text{Daily Cooking} = \frac{100 \frac{\text{lbs}}{\text{day}} \times 250 \frac{\text{Btu}}{\text{lb}}}{46\%} = 54,348 \frac{\text{Btu}}{\text{day}}$$

$$\text{NG Usage} = \left(11,000 \frac{\text{Btu}}{\text{day}} + 124,578 \frac{\text{Btu}}{\text{day}} + 54,348 \frac{\text{Btu}}{\text{day}} \right) \times 312 \frac{\text{days}}{\text{year}} = 59,256,900 \frac{\text{Btu}}{\text{year}}$$

Natural Gas Savings:

$$\text{NG}_{\text{savings}} = (90,173,943 - 59,256,900) \times \frac{1 \text{ Btu}}{35,738 \text{ m}^3} = 865 \frac{\text{m}^3}{\text{year}}$$

Electric Savings:

$$\text{Elec}_{\text{savings}} = (\text{Daily Cooking Time}_{\text{Conventional}} - \text{Daily Cooking Time}_{\text{ENERGY STAR}}) \times \text{HP}_{\text{fan}} \times 0.7457 \frac{\text{kW}}{\text{HP}} \times \frac{\text{Days}}{\text{Year}}$$

$$\text{Elec}_{\text{savings}} = \left(1.43 \frac{\text{hours}}{\text{day}} - 1.20 \frac{\text{hours}}{\text{day}} \right) \times 0.75 \text{ HP} \times 0.7457 \frac{\text{kW}}{\text{hp}} \times 312 \frac{\text{days}}{\text{year}} = 40.1 \text{ kWh}$$

USES AND EXCLUSIONS

To qualify for this measure the full size convection oven must be utilized for food preparation or processing with natural gas as its energy source and must be ENERGY STAR rated.

MEASURE LIFE

The measure life attributed to this measure is 12 years. [5]

INCREMENTAL COST

There are no incremental costs associated with this measure.

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COMMERCIAL ENERGY STAR DISHWASHERS – NEW CONSTRUCTION /TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Water Heating → ENERGY STAR Dishwasher → New Construction/ Time of Natural Replacement	

Table 1 shows the key measure parameters including the savings for each type of dishwasher.

Table 1. Measure Key Data

Parameter	Definitions			
Measure Category	New Construction Time of Natural Replacement			
Baseline Technology	Table 2			
Efficient Technology	Table 3			
Market Type	Commercial			
Annual Natural Gas Savings (m ³) Annual Electric Savings (kWh) Annual Water Savings (liters)	Dishwasher Type	Savings		
		Natural Gas (m³)	Electric (kWh)	Water (liters)
	High Temperature Dishwashers			
	Under Counter	137	1,791	20,371
	Stationary Single Tank Door	890	4,173	132,263
	Single Tank Conveyor	540	4,251	80,303
	Multi Tank Conveyor	2,049	9,680	304,677
	Low Temperature Dishwashers			
	Under Counter	322	0	47,827
	Stationary Single Tank Door	2,046	0	304,205
	Single Tank Conveyor	1,652	0	245,631
	Multi Tank Conveyor	2,383	0	354,276
Measure Life	Dishwasher Type	High and Low Temperature (years)		
	Under Counter	10		
	Stationary Single-Tank Door	15		
	Single-Tank Conveyor	20		
	Multi-Tank Conveyor	20		

Parameter	Definitions		
	Dishwasher Type	High Temperature	Low Temperature
Incremental cost (\$ CAD)	Under Counter	\$171	\$71
	Stationary Single-Tank Door	\$1,100	\$0
	Single-Tank Conveyor	\$2,929	\$0
	Multi-Tank Conveyor	\$1,386	\$1,386
Restrictions	Commercial facilities with natural gas hot water heating.		

OVERVIEW

Dishwasher types are broken into two primary categories: high temperature and low temperature. High temperature dishwashers use a booster water heater to heat the already hot tap water to a minimum of 180°F [1] as required by the National Sanitation Foundation (NSF) Standard No. 3 [2]. At these temperatures, hard-to-remove residues like lipstick and grease are dissolved without the need for additional sanitizing chemicals. These dishwashers have the additional benefits of shorter wash cycles and less water use per cycle. Low temperature dishwashers require chemical sanitizers and may require multiple cycles to clean hard to remove residues. Low temperature dishwashers are less expensive than high temperature models. For this measure, booster heaters are assumed to be electric, as they are most prevalent, although natural gas booster heaters are available.

Besides high and low temperature categories, dishwashers can be further categorized by the volume of dishes or the number of racks they handle. Types of dishwashers in order of increasing capacity are: under-counter, stationary rack, and rack conveyer. Under-counter types are similar to residential dishwashers and can handle up to 35 racks per hour. Stationary rack or pull-down-hood dishwashers are suitable for small commercial settings and can handle up to 80 racks an hour. Conveyer dishwashers pull racks through on a conveyer system and can handle up to 400 racks per hour [3].

Conveyer-type dishwashers are configured with either one tank for circulation water or several; one for each stage of the wash cycle (wash, rinse, and sanitize). Multiple-tank dishwashers can handle up to 600 racks per hour and have different ENERGY STAR requirements from their single-tank counterparts.

ENERGY STAR-qualified dishwashers are performance rated for water use per rack and idle power draw. Each type of dishwasher has its own product qualification criteria as outlined in Table 3. The water consumption values are a key component used in the calculation of energy consumption for dishwashers.

New Construction/Time of Natural Replacement Projects

Installing ENERGY STAR-rated dishwashers in new construction projects or at the end of the existing equipment's useful life will result in natural gas savings from the increased washing efficiency. The washing efficiency and energy savings are primarily derived from the reduced use of hot water.

APPLICATION

This measure provides incentives for installing ENERGY STAR-rated dishwashers in a commercial setting.

BASELINE TECHNOLOGY

Non-ENERGY STAR-rated dishwashers are assumed to have the parameters shown in Table 2. The baseline value is derived from the ENERGY STAR commercial kitchen equipment calculator, which cites EPA/Food Service Technology Center's equipment specification research, 2013, as their source.

Table 2. Baseline Technology [4]

Machine Type	High Temperature Efficiency		Low Temperature Efficiency	
	Idle Energy Rate (kW) ¹	Water Consumption (GPR) ²	Idle Energy Rate (kW) ¹	Water Consumption (GPR) ²
Under Counter	0.76	1.09	0.50	1.73
Stationary Single Tank Door	0.87	1.29	0.60	2.10
Single Tank Conveyor	1.93	0.87	1.50	1.31
Multiple Tank Conveyor	2.59	0.97	2.00	1.04

¹ Idle results should be measured with the door closed and represent the total idle energy consumed by the machine including all tank heater(s) and controls. Booster heater (internal or external) energy consumption should not be part of this measurement unless it cannot be separately monitored per the ENERGY STAR test method [5].

² GPR = gallons per rack

EFFICIENT TECHNOLOGY

ENERGY STAR-rated dishwashers must have idle energy and water consumption rates as defined in Table 3.

Table 3. ENERGY STAR Energy Efficiency Requirements for Commercial Dishwashers [5]

Machine Type	High Temperature Efficiency Requirements		Low Temperature Efficiency Requirements	
	Idle Energy Rate (kW) ¹	Water Consumption (GPR) ²	Idle Energy Rate (kW) ¹	Water Consumption (GPR) ²
Under Counter	≤ 0.50 kW	≤ 0.86 GPR	≤ 0.50 kW	≤ 1.19 GPR
Stationary Single Tank Door	≤ 0.70 kW	≤ 0.89 GPR	≤ 0.60 kW	≤ 1.18 GPR
Single Tank Conveyor	≤ 1.50 kW	≤ 0.70 GPR	≤ 1.50 kW	≤ 0.79 GPR
Multiple Tank Conveyor	≤ 2.25 kW	≤ 0.54 GPR	≤ 2.00 kW	≤ 0.54 GPR

¹ Idle results should be measured with the door closed and represent the total idle energy consumed by the machine including all tank heater(s) and controls. Booster heater (internal or external) energy consumption should not be part of this measurement unless it cannot be separately monitored per the ENERGY STAR Test Method [5].

² GPR = gallons per rack

ENERGY IMPACTS

Natural gas and electrical savings are achieved due to the fact that the higher efficiency equipment requires less heated water and typically less electricity for each load than its baseline non-ENERGY STAR counterpart.

NATURAL GAS AND ELECTRICAL SAVINGS ALGORITHMS

The following algorithms are referenced from the ENERGY STAR Commercial Kitchen Equipment Calculator for dishwashers.

The natural gas savings are a function of the water saved by the energy efficient technology, and the electrical savings are a result of lower idle energy rates. It is notable that the baseline and ENERGY STAR low temperature dishwashers have the same idle energy rates, which results in zero electricity savings.

First, the heat input required to raise the water to the desired temperature (Q_{in}) is calculated on a per gallon basis. Next, the annual water consumption is calculated for both the baseline and ENERGY STAR-rated dishwashers based on the water use per rack (GPR) and the number of racks washed per day (RPD). Finally the fuel savings are calculated using results from the previous calculations.

Starting with the calculation for the water heater specific energy consumption:

$$Q_{In} = T_{Inc} \times C_P \times \frac{\rho}{Eff_{Gas}}$$

where,

Q_{In} = Water heater specific energy consumption (Btu/gal)

T_{Inc} = Temperature increase required by building heating system for supply water (see Table 4, °F)

C_p = Specific heat of water (Btu/lb °F)

ρ = Density of water (lb/gal)

Eff_{Gas} = Building water heating system efficiency (%)

The annual water consumption can be calculated as:

$$Annual\ water\ consumption = GPR \times RPD \times Days$$

where,

Annual water consumption = Annual water consumption of the dishwasher (gallons/year)

GPR = Gallons per rack water consumption of dishwasher (gal/rack)

RPD = Racks washed per day (racks/day)

Days = Annual days of operation (days/year)

The annual fuel consumption can be calculated as:

$$Annual\ fuel\ consumption = Annual\ water\ consumption \times Q_{In}$$

where,

Annual fuel consumption – Annual fuel consumption to heat water for the dishwasher (MMBtu)

The fuel savings can be calculated as the difference between the baseline and energy efficiency calculated annual fuel consumptions.

$$Fuel\ savings = Annual\ fuel\ consumption_{Base} - Annual\ fuel\ consumption_{EE}$$

where,

Base refers to the annual fuel consumption for the baseline technology.

EE refers to the annual fuel consumption for the energy efficient technology.

Dishwashers use electricity while idle, called the idle energy rate (IER), and are performance rated for this parameter by ENERGY STAR. The electricity consumption of a dishwasher can be calculated from the idle energy rate and by calculating the amount of time that the machine spends idle.

$$Elec = IER \times (Hrs \times Days - Days \times RPD \times \frac{TWT}{60})$$

where,

Elec = Annual electricity consumption (kWh)

IER = Idle energy rate (kW)

Hrs = Average daily operation (hours)

Days = Annual days of operation (days/year)

RPD = Racks washed per day (racks/day)

TWT = Typical wash time (minutes)

For high temperature models there is also an electric component that is attributable to the booster heater, which is responsible for heating the supply water from 140°F to 180°F. The energy required to heat the water the additional 40°F is calculated in a way similar to that for the primary natural gas water heater by first calculating the kWh per gallon required to raise the temperature of the water the desired amount.

$$Q_{Boost} = \frac{T_{Boost} \times C_p \times \rho}{Eff_{Elec} \times 3,412 \text{ Btu/kWh}}$$

where,

Q_{Boost} = Energy required to raise the temperature of the water from the primary water heater set point to the high temperature set point of the booster heater (kWh/gallon)

T_{Boost} = Temperature difference between the primary water heater setpoint and the booster heater high temperature setpoint (°F)

C_p = Specific heat of water (Btu/lb °F)

ρ = Density of water (lb/gal)

Eff_{Elec} = Efficiency of the electrical booster heater (%)

$3,412 \frac{Btu}{kWh}$ = Conversion factor for kilowatt hours (kWh) British thermal units (Btus)

The electrical energy attributable to the booster heater can be calculated by multiplying the kWh per gallon required to raise the temperature of the water to 180°F by the annual water consumption.

$$Elec_{Boost} = Q_{Boost} \times \text{Annual water consumption}$$

The electrical savings can be calculated by tabulating electrical consumption for both the base and energy efficient models from the idle energy equation and the booster heater if a high temperature model.

$$Elec \text{ savings} = Elec_{Base} - Elec_{EE}$$

where,

$Elec \text{ savings}$ = Annual electricity savings for the measure (kWh)

$Elec_{Base}$ = Annual electricity consumption for the baseline dishwasher, including the booster heater contribution if a high temperature model (kWh)

$EleC_{EE}$ = Annual electricity consumption for the ENERGY STAR dishwasher, including the booster heater contribution of a high temperature model (kWh)

ASSUMPTIONS

Table 4 shows the list of conversions utilized in the measure savings algorithm.

Table 4. Assumptions

Variable	Definition	Inputs for Baseline and Energy Efficient Options	Source/Comments
C_P	Specific heat capacity of water	1.00 Btu/lb °F	Common assumptions table
ρ	Density of water	8.29 lb/gal (US)	Common assumptions table
	City supply water temperature	48.9°F (9.39°C)	Common assumptions table
	Commercial hot water tank temperature	140°F (60°C)	Common assumptions table
T_{Inc}	Temperature delta that building heating system will need to heat city supply water to feed hot water tank	$\Delta T = 91.1^\circ\text{F}$ ($\Delta T = 50.61^\circ\text{C}$)	$T_{inc}=140^\circ\text{F} - 48.9^\circ\text{F}$
	Energy density of natural gas	35,738 Btu/m ³	Common assumptions table
T_{Boost}	Temperature difference that needs to be met by booster heater	$\Delta T = 40^\circ\text{F}$ ($\Delta T = 22.2^\circ\text{C}$)	[5]
Eff_{Gas}	Commercial water heating efficiency	83%	Common assumptions table
Eff_{Elec}	Electric booster heater efficiency	98%	[6]
Hrs	Average daily operation	18 hrs	[6]
Days	Food service days per year	312 days	Common assumptions table

ENERGY STAR uses the assumptions in Table 5 for racks washed per day.

Table 5. Assumptions for Racks Washed Per Day [6]

Dishwasher Type	High and Low Temperature
Under counter	75

Dishwasher Type	High and Low Temperature
Stationary single-tank door	280
Single-tank conveyor	400
Multi-tank conveyor	600

ENERGY STAR uses the assumptions in Table 6 for typical wash times.

Table 6. Assumptions for Typical Wash Time Minutes [6]

Dishwasher Type	High Temperature	Low Temperature
Under counter	2.0	2.0
Stationary single-tank door	1.0	1.5
Single-tank conveyor	0.3	0.3
Multi-tank conveyor	0.2	0.3

There are two considerations that should be taken into account before making the savings calculations:

1. All high temperature boosters are assumed to be electric.
2. Primary water heating systems are assumed to be natural gas.

SAVINGS CALCULATION EXAMPLE

The example below shows how the savings would be calculated for the measure. For the example, it will be assumed that an ENERGY STAR-rated low temperature single-tank conveyor dishwasher will be installed.

The heat required to raise the temperature of the water to the desired point (constant for all dishwasher types):

$$Q_m = \frac{91.1^\circ F \times 1 \frac{Btu}{lb} \times 8.29 \frac{lb}{gal}}{0.83 \times 35,738 Btu/m^3} = 0.02546 m^3/US gal$$

Then the annual water consumption can be calculated for the ENERGY STAR-rated dishwasher as:

$$\begin{aligned} \text{Annual water consumption}_{EE} &= 0.79 \text{ gal/rack} \times 400 \text{ racks/day} \times 312 \text{ days/year} \\ &= 98,592 \text{ gallons per year} \end{aligned}$$

The conventional water consumption can be calculated similarly as:

$$\text{Annual water consumption}_{Base} = 163,488 \text{ gallons per year}$$

Energy efficient fuel consumption can be calculated as follows:

$$\text{Annual fuel consumption}_{EE} = 98,592 \times 0.02546 = 2,510.2 \frac{m^3}{yr}$$

$$\text{Annual fuel consumption}_{\text{Base}} = 191,260 \times 0.02546 = 4,162.5 \frac{\text{m}^3}{\text{yr}}$$

Annual fuel savings:

$$\text{Fuel savings} = 4,162.5 \frac{\text{m}^3}{\text{yr}} - 2,510.2 \frac{\text{m}^3}{\text{yr}} = 1,652.3 \frac{\text{m}^3}{\text{yr}}$$

The low temperature dishwashers do not have any electricity savings.

USES AND EXCLUSIONS

The installed dishwasher must be ENERGY STAR-qualified and installed in a commercial setting.

MEASURE LIFE

Table 7 shows the measure lifetimes for each type of dishwasher

Table 7. Equipment Lifetime (Years) [5] [7]

Dishwasher Type	High and Low Temperature
Under counter	10
Stationary single-tank door	15
Single-tank conveyor	20
Multi-tank conveyor	20

The equipment lifetimes were derived from the Food Service Technology Center (FSTC), which contributed to the development of the ENERGY STAR U.S. calculator. No lifetime distinction was identified relative to the sanitation method (high or low temperature) or to the efficiency (ENERGY STAR-qualified or not) of the dishwashers.

INCREMENTAL COST

Table 8 shows the equipment incremental costs for each type of dishwasher.

Table 8. Incremental Costs¹ [8]

Dishwasher Type	High Temperature	Low Temperature
Under counter	\$171	\$71
Stationary single-tank door	\$1,100	\$0

¹ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

Dishwasher Type	High Temperature	Low Temperature
Single-tank conveyor	\$2,929	\$0
Multi-tank conveyor	\$1,386	\$1,386

Incremental costs were obtained from the ENERGY STAR commercial kitchen equipment energy savings calculator.

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COMMERCIAL – ENERGY STAR FRYER – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Food Service → ENERGY STAR Fryer → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definitions
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)
Baseline Technology	A non-ENERGY STAR rated fryer
Efficient Technology	An ENERGY STAR rated fryer
Market Type	Commercial
Annual Natural Gas Savings (m ³ per vat)	1,408 m ³
Measure Life	12 years
Incremental Cost (\$CAD)	\$2,476
Restrictions	Restricted to commercial facilities with standard or large-vat natural gas fryers for food service.

OVERVIEW

Fryers are used in commercial and institutional food service preparation for frying food in heated oil. Though fryers are available in a range of configurations, with the exception of specialized fryers for specific food items, they share a common design. The food is immersed in a kettle that holds the oil, which is typically heated by atmospheric or infrared gas burners underneath the kettle, or via “fire tubes” running through the kettle wall. The heating elements are controlled by a thermostat. The kettle holds enough oil so that the food is supported by displacement of the oil, rather than by the bottom of the vessel. There are three primary types of fryers: open deep-fat fryers, pressure fryers, and specialty fryers. Open fryers are the most common. [1]

During food service operations the fryers are turned on at the beginning of the day and turned off at the end of the shift; the fryer cycles on and off to maintain the desired temperature setting. Fryers are estimated to be idle 75% of the time. [1]

ENERGY STAR fryers are up to 30% more efficient than non-ENERGY STAR rated fryers. [2]

APPLICATION

This measure applies to ENERGY STAR qualifying open-vat fryers in commercial and institutional food processing settings. A fryer is designed to cook food in heated oil. The fryer consumes natural gas during three modes: preheat – at the beginning of the shift when the fryer is turned on and the oil is raised from room temperature to cooking temperature, idling - maintaining the temperature of the cooking oil between cooking, and cooking – restoring heat to the oil when cold foods are dropped in the fryer.

ENERGY STAR fryers save energy by offering shorter cook times and higher production rates through advanced burner and heat exchanger designs. Fry pot insulation reduces standby losses resulting in a lower idle energy rate.

BASELINE TECHNOLOGY

The baseline technology is a single or multiple, standard and large open-vat commercial fryer.

EFFICIENT TECHNOLOGY

The efficient technology is a single, or multiple, open-vat fryer that is ENERGY STAR rated. Vats may be standard size (12 inches to 18 inches wide) or large size (18 to 24 inches wide)¹ [3]

Table 2. Efficient Requirements [2] [4]

Type	ENERGY STAR Requirements
ENERGY STAR Open-Vat Fryer	Single or multiple gas-fired open deep-fat fryers with cooking efficiency of $\geq 50\%$, and maximum idling rates of: <ul style="list-style-type: none">• Standard vat size; $\leq 9,000$ Btu/hr idling rate• Large vat fryers (larger than 18" wide); $\leq 12,000$ Btu/hr idling rate.

¹ The ENERGY STAR cooking efficiency requirements are the same for standard, large, and multiple vat fryers. The idling rate requirement varies with vat size.

ENERGY IMPACTS

The primary energy impact associated with the installation of an ENERGY STAR fryer is natural gas savings associated with a reduction in natural gas required during pre-heat, idling and cooking times. ENERGY STAR qualified fryers must meet a minimum cooking efficiency of 50%, and maximum idling rates. This savings is achieved through shorter cook times and higher production rates through advanced burner and heat exchanger designs. Fry pot insulation also reduces standby losses resulting in lower idle energy rates. There are no electric savings for this measure.

NATURAL GAS SAVINGS ALGORITHM

The energy savings algorithm is calculated by determining and comparing the annual energy usage in baseline and ENERGY STAR qualifying fryers. To determine total energy usage the calculation must determine the energy consumed during pre-heating, cooking, and idling modes.

The algorithm is based upon the methodology utilized by the Food Service Technology Center and ENERGY STAR for each vat. For both the baseline and the efficient case, the following calculation is used to determine the energy usage.

$$NG\ Usage = Days \times (Daily\ Preheat + Daily\ Idle + Daily\ Cooking)$$

where,

NG Usage	= the amount of natural gas used by the fryer annually in Btu/year
Days	= the number of days per year the fryer is in use
Daily Preheat	= the amount of natural gas used to preheat the fryer daily in Btu/day
Daily Idle	= the amount of natural gas used when the fryer is in idle mode in Btu/day
Daily Cooking	= the amount of natural gas used when the fryer is cooking in Btu/day

The daily idle energy is calculated using the following equation:

$$Daily\ Idle = Idle\ Time \times Idle\ Rate$$

where,

Idle Time	= length of time the unit is idle per day in hours
Idle Rate	= energy consumed during idling in Btu/hr

The idle time is calculated using the following equation:

$$Idle\ Time = Total\ Operating\ Hours - Preheat\ Time - Cooking\ Time$$

where,

- Idle Time = length of time the unit is idle per day in hours
- Total Operating Hours = amount of time fryers operate a day in hours
- Preheat Time = length of time unit is in preheat mode in hours
- Cooking Time = amount of time fryers are cooking food in hours

$$Daily\ Cooking = \frac{Food\ Weight \times ASTM\ Energy\ to\ Food\ Rate}{Efficiency}$$

where,

- Food Weight = average quantity of food cooked in unit per day in pounds
- ASTM Energy to Food Rate = rate at which energy is transferred to food in Btu/lb
- Efficiency = efficiency of the unit

The savings is then calculated from the difference between the baseline and efficient cases.

$$NG_{savings} = (NG\ Usage_{baseline} - NG\ Usage_{ENERGY\ STAR}) \times \frac{1\ m^3}{35,738\ Btu}$$

where,

- $NG_{savings}$ = annual reduction in natural gas consumption in m³/year
- $NG\ Usage_{baseline}$ = annual energy usage of a conventional fryer in Btu/year
- $NG\ Usage_{ENERGY\ STAR}$ = annual energy usage for an ENERGY STAR fryer in Btu/year

ASSUMPTIONS

The assumptions used to calculate natural gas savings are shown in Table 3.

Table 3. Assumptions

Parameter	Baseline	High Efficiency	Source
Food Service Days	312		Common assumptions table
Preheat Time (hours)	0.175		[5]
Preheat Energy (Btu)	18,500	16,000	[5]

Parameter	Baseline	High Efficiency	Source
Cooking Time (hours)	2		[6]
Operating hours per day	14		[5]
Idle Time (hours)	11.83		Calculated
Idle Rate (Btu/h)	17,000	9,841	[5]
Food Weight (lbs/day)	150		[5]
Heavy Load Energy to Food (Btu/pound)	577		[7] [8]
Efficiency	35%	50%	[5] [4]
Energy Density of Natural Gas	35,738 Btu/m ³		Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the deemed savings value is determined for an ENERGY STAR Fryer with typical hours of usage.

Annual Conventional Fryer Usage:

$$\text{Daily Preheat} = 18,500 \text{ Btu}$$

$$\text{Daily Idle} = 11.825 \text{ hours} \times 17,000 \frac{\text{Btu}}{\text{hr}} = 201,025 \text{ Btu}$$

$$\text{Daily Cooking} = \frac{150 \text{ pounds} \times 577 \text{ Btu/pound}}{35\%} = 247,286 \text{ Btu}$$

To calculate the annual conventional fryer consumption:

$$\text{NG Usage} = 312 \frac{\text{days}}{\text{year}} \times \left(18,500 \frac{\text{Btu}}{\text{day}} + 201,025 \frac{\text{Btu}}{\text{day}} + 247,286 \frac{\text{Btu}}{\text{day}} \right) = 145,644,943 \frac{\text{Btu}}{\text{year}}$$

Annual ENERGY STAR Fryer Usage:

$$\text{Daily Preheat} = 16,000 \text{ Btu}$$

$$\text{Daily Idle} = 11.83 \text{ hours} \times 9,841 \frac{\text{Btu}}{\text{hr}} = 116,375 \text{ Btu}$$

$$\text{Daily Cooking} = \frac{150 \text{ pounds} \times 577 \text{ Btu/pound}}{50\%} = 173,100 \text{ Btu}$$

To calculate the annual ENERGY STAR fryer consumption:

$$\text{NG Usage} = 312 \frac{\text{days}}{\text{year}} \times \left(16,000 \frac{\text{Btu}}{\text{day}} + 116,375 \frac{\text{Btu}}{\text{day}} + 173,100 \frac{\text{Btu}}{\text{day}} \right) = 95,308,295 \frac{\text{Btu}}{\text{year}}$$

Natural Gas Savings:

$$NG_{savings} = (145,644,943 \text{ Btu} - 95,308,295 \text{ Btu}) \times \frac{1}{35,738 \frac{\text{Btu}}{\text{m}^3}} = 1,408 \text{ m}^3$$

USES AND EXCLUSIONS

To qualify for this measure the fryer must be utilized for food preparation or processing with natural gas as its energy source and be ENERGY STAR rated.

MEASURE LIFE

The measure life attributed to this measure is 12 years. [5]

INCREMENTAL COST

Table 4 presents the measure incremental cost.

Table 4. Incremental Cost² [9]

Measure Category	Incremental Cost (\$)
New Construction/Time of Natural Replacement	\$2,476

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COMMERCIAL – ENERGY STAR STEAM COOKER – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Food Service → ENERGY STAR Steam Cookers → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings.

Table 1. Measure Key Data

Parameter	Definitions
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)
Baseline Technology	Boiler-Based Steam Cooker
Efficient Technology	ENERGY STAR Rated Steam Cooker
Market Type	Commercial
Annual Natural Gas Savings (m ³)	8,889 m ³
Annual Water Savings (liters)	340,142 liters
Measure Life	12 years
Incremental Cost (\$ CAD)	\$3,880
Restrictions	Measure is limited to steam cookers that have either a connectionless or steam-generator design.

OVERVIEW

Steam cookers are used in commercial and institutional food service preparation to cook foods that do not need to form a crust. The steamer resembles an oven where food is steamed in a sealed cavity. [1]

The steam can be delivered to the cavity in several different ways. In a pressureless steamer, steam is injected through openings in the sides of the cooking compartment. A variety of foods

can be cooked at the same time, and the cooking compartment door can be opened at any time during the cooking procedure. Pressure steamers use steam that has been pressurized to 5 to 15 psi. The cooking compartment needs to be depressurized before it can be opened. [2]

The steam itself may be produced in several ways:

- Boiler steamer: The steamer has an external boiler (relative to the cooking compartment) that generates potable steam.
 - Pressurized steamers: The pressurized steam is delivered as demanded by control settings. Compartment must be depressurized before it is opened.
 - Pressureless steamer: The compartment is openly connected to a condensate drain and the pressure in the compartment is at or slightly above atmospheric pressure.
- Steam generator: The steam generator is located within or connected to the cooking cavity, generating steam at (or slightly above) atmospheric pressure.
- “Connectionless” Steamer: the steam is produced by boiling water delivered directly to a reservoir located within the cooking compartment prior to operation. [1]

There are several steam cooker configurations which include: countertop models, wall-mounted models, and floor models mounted on pedestal or cabinet-style base. Commercial steamers come in different sizes, but steamers holding six or more pans are the most common, based on the ENERGY STAR approved products list. [3] Energy efficient steam cookers that have earned the ENERGY STAR designation offer shorter cook times, higher production rates, and reduced heat loss due to better insulation and more efficient steam delivery system. [4]

This measure is for ENERGY STAR approved steam cookers with either connectionless or steam-generator design. These steamer designs are often termed: “boilerless.” Standard boiler steamers are not eligible as they do not meet ENERGY STAR efficiency criteria due to their low efficiencies during idling and cooking. [1]

APPLICATION

This measure applies to the installation of ENERGY STAR qualifying steam cookers in commercial and institutional food preparation. The food is manually placed into the steamer and removed when the cooking is complete. Steam cookers consume natural gas when they are pre-heating, idling and cooking.

BASELINE TECHNOLOGY

The baseline technology is a standard boiler-based steam cooker. No boiler-based steam cookers are ENERGY STAR-listed as their efficiency levels fall below the ENERGY STAR requirements. Boiler-based steamers are connected to a potable water line and continually supply steam to the cooking compartment, leading to high idle energy consumption [1]

EFFICIENT TECHNOLOGY

The efficient technology is an ENERGY STAR rated steam cooker meeting the criteria presented in Table 2.

Table 2. Efficient Technology [5]

Type	ENERGY STAR Requirements
6-pan ENERGY STAR Steam Cooker	ENERGY STAR rated Steam Cooker used in a commercial or institutional environment, with a minimum efficiency of 38% and a maximum idle-rate of 12,500 Btu/hr

The majority of ENERGY STAR steamers on the qualifying products list are “connectionless.” “Connectionless steamers” do not require potable water feed, or condensate drain connections. Water is poured into a compartment at the bottom that is refilled during the day and any remaining water at the end of operation is drained from the cavity into a pan or bucket. [1] ENERGY STAR steam generation cookers require a water connection and a condensate drain, but offers improved efficiency over standard boiler-based cookers.

ENERGY IMPACTS

The primary energy impact associated with the installation of an ENERGY STAR steam cooker is a reduction in natural gas required during pre-heat, idle and cooking modes.

Connectionless steamers are inherently more energy efficient than boiler-based or conventional steam generation systems since any steam that does not condense on the food remains in the cooking compartment, rather than being condensed and drained. [1]

ENERGY STAR qualified steam cookers must meet the specification requirements of 38% natural gas minimum cooking efficiency, and a maximum idle rate. The idle rate requirement varies with the size of the steamer. The savings are achieved through shorter cook times, higher production rates, through improved steam delivery, and reduced heat loss due to better insulation. Water savings are also achieved through reduced consumption of steam during shorter cooking times and reduced condensate draining. [4] [6] There are no electric impacts for this measure.

NATURAL GAS SAVINGS ALGORITHM

The energy savings algorithm is calculated by determining and comparing the annual energy usage in baseline and ENERGY STAR steam cookers. To determine total energy usage, the calculation must determine the energy consumed during pre-heating, cooking, and idling modes.

The algorithm is based upon the methodology utilized by the Food Service Technology Center and ENERGY STAR. For both the baseline and the efficient case, the following calculation is used to determine the energy usage.

$$NG\ Usage = Days \times (Daily\ Preheat + Daily\ Idle + Daily\ Cooking)$$

where,

- NG Usage = the amount of natural gas used by the steam cooker annually in Btu/year
- Days = the number of days per year the steam cooker is in use
- Daily Preheat = the amount of natural gas used to preheat the steam cooker daily in Btu/day
- Daily Idle = the amount of natural gas used daily when the steam cooker is in idle mode in Btu/day
- Daily Cooking = the amount of natural gas used daily when the steam cooker is cooking in Btu/day

The “*Daily Idle*” energy is calculated using the following equation:

$$Daily\ Idle = Actual\ Idling + Residual\ Idling$$

where,

- Actual Idling = energy consumed when unit is actually idling in Btu/day
- Residual Idling = energy consumed in manual mode during idling in Btu/day

The baseline steamers operate in manual mode 90% of the time. That means that the operator has control of the unit, and the steamer will typically be maintained at a constant steam mode, using energy equivalent to when cooking. During that time, "idle" energy rate is equal to full-load energy rate. ENERGY STAR units are typically controlled by an integral timer.

The “*Actual Idling*” energy is calculated using the following equation:

$$Actual\ Idling = (1 - \%Manual\ Mode) \times Idle\ Rate \times Idling\ Time$$

where,

- %Manual Mode = Percentage of time unit is injecting steam in the cavity but is not actually cooking
- Idle Rate = Idling energy rate in Btu/hr
- Idling Time = Time unit is in idle mode in hours

The “*Idling Time*” is determined using the following equation:

$$Idling\ Time = Total\ Hours\ of\ Operation - Preheat\ time - \frac{Food\ Cooked\ per\ Day}{Production\ Capacity}$$

where,

Total Hours of Operation	= Total hours unit is operation in hours
Preheat time	= time it takes to preheat the unit to operating temperature in hours
Food cooked per day	= amount of food cooked by unit per day in lbs/day
Production capacity	= the average load capacity of unit to cook food in lbs/hr.

The expression $\frac{\text{Food Cooked per Day}}{\text{Production Capacity}}$ calculates the actual cooking time.

The other portion of the *Daily Idling* use is the *Residual Idling*. This is the amount of energy the unit is on manual mode and continually providing steam without the need for cooking. The expression to calculate this is as follows:

$$\begin{aligned} & \text{Residual Idling} \\ &= \% \text{Manual Mode} \times \frac{\text{Production Capacity} \times \text{ASTM Energy to Food Rate}}{\text{Efficiency}} \\ & \times \text{Idling Time} \end{aligned}$$

where,

ASTM Energy to Food Rate	= rate at which energy is transferred to food in Btu/lb
Efficiency	= efficiency of the unit

The expression, $\frac{\text{Production Capacity} \times \text{ASTM Energy to Food Rate}}{\text{Efficiency}}$, in the “*Residual Idling*” equation calculates the cooking rate in Btu/hr. During manual mode, the unit will provide steam at the cooking rate.

The daily cooking energy is calculated as follows:

$$\text{Daily Cooking} = \frac{\text{Food Cooked per Day} \times \text{ASTM Energy to Food Rate}}{\text{Efficiency}}$$

where,

Daily Cooking= the amount of natural gas used when the unit is cooking in Btu/day. The savings is then calculated from the difference between the baseline and efficient cases.

$$NG_{\text{savings}} = (NG \text{ Usage}_{\text{baseline}} - NG \text{ Usage}_{\text{ENERGY STAR}}) \times \frac{1\text{m}^3}{35,738\text{Btu}}$$

where,

NG_{savings}	= annual reduction in natural gas consumption in m ³ /year
$NG \text{ Usage}_{\text{baseline}}$	= annual energy usage of a conventional steamer in Btu/year
$NG \text{ Usage}_{\text{ENERGY STAR}}$	= annual energy usage for an ENERGY STAR steamer in Btu/year

WATER SAVINGS ALGORITHM

There are also water savings associated with this measure. They are calculated according to this formula:

$$\text{Water Saved} = \text{Days} \times \text{Total Hours of Operation} \\ \times (\text{Water Use}_{\text{baseline}} - \text{Water Use}_{\text{ENERGY STAR}})$$

where,

Total Hours of Operation = the total hours unit is operating per day

Water Use = the water use of the unit in liters per hour

ASSUMPTIONS

The assumptions used to calculate natural gas savings are shown in Table 3.

Table 3. Assumptions

Parameter	Baseline	High Efficiency	Source
Food Service Days per Year	312		Common assumptions table
Operation Time (hours)	12		[7] [8]
Preheat Time (hours)	0.17		[9]
Preheat Energy (Btu/h)	20,000	9,000	[7]
Idle Rate (Btu/hr)	15,000	2,921	[7]
Production Capacity (lbs/hr)	140	125	[7]
Food Cooked per Day (lbs/day)	100	100	[7]
Percent of Time in Manual Mode	0.9	0	[7]
ASTM Energy to Food Rate (Btu/pound)	105		[7], [10], [11]
Efficiency	15% [7]	38% [5]	[7], [5]
Water Use(liters/hr)	136 liters/hr (36 gals/hr)	45.4 liters/hr (12 gals/hr)	[7]

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings values are determined for an ENERGY STAR Steam Cooker with typical hours of usage.

Daily Baseline Steamer Usage:

$$\text{Daily Preheat} = 20,000 \frac{\text{Btu}}{\text{day}}$$

Daily Idle:

$$\text{Daily Idle} = \text{Actual Idling} + \text{Residual Idling}$$

First we need to determine actual idling time to determine actual and residual idling energy.

$$\text{Idling Time} = 12 \text{ hrs} - 0.17 \text{ hrs} - \frac{100 \frac{\text{lbs}}{\text{day}}}{140 \frac{\text{lbs}}{\text{hr}}} = 11.1 \frac{\text{hrs}}{\text{day}}$$

Actual Idling:

$$\text{Actual Idling} = (1 - 90\%) \times 15,000 \frac{\text{Btu}}{\text{hr}} \times 11.1 \frac{\text{hrs}}{\text{day}} = 16,674 \frac{\text{Btu}}{\text{day}}$$

Residual Idling:

$$\text{Residual Idling} = 90\% \times \frac{140 \frac{\text{lbs}}{\text{hr}} \times 105 \frac{\text{Btu}}{\text{lb}}}{15\%} \times 11.1 \frac{\text{hrs}}{\text{day}} = 980,406 \frac{\text{Btu}}{\text{day}}$$

Daily Idle Energy:

$$\text{Daily Idle} = 16,674 \frac{\text{Btu}}{\text{day}} + 980,406 \frac{\text{Btu}}{\text{day}} = 997,080 \frac{\text{Btu}}{\text{day}}$$

Daily Cooking:

$$\text{Daily Cooking} = \frac{100 \frac{\text{lb}}{\text{day}} \times 105 \frac{\text{Btu}}{\text{lb}}}{15\%} = 70,000 \frac{\text{Btu}}{\text{day}}$$

Total Daily Usage:

$$\text{NG Usage} = \left(20,000 \frac{\text{Btu}}{\text{day}} + 997,080 \frac{\text{Btu}}{\text{day}} + 70,000 \frac{\text{Btu}}{\text{day}} \right) = 1,087,080 \frac{\text{Btu}}{\text{day}}$$

Total Annual Usage:

$$\text{NG Usage}_{\text{Baseline}} = 1,087,080 \frac{\text{Btu}}{\text{day}} \times 312 \frac{\text{days}}{\text{year}} = 339,168,826 \frac{\text{Btu}}{\text{year}}$$

Daily ENERGY STAR Usage:

$$\text{Daily Preheat} = 9,000 \frac{\text{Btu}}{\text{day}}$$

Daily Idle:

$$\text{Daily Idle} = \text{Actual Idling} + \text{Residual Idling}$$

First we need to determine actual idling time to determine actual and residual idling energy.

$$\text{Idling Time} = 12 \text{ hrs} - 0.17 \text{ hrs} - \frac{100 \frac{\text{lbs}}{\text{day}}}{125 \frac{\text{lbs}}{\text{hr}}} = 11.03 \frac{\text{hrs}}{\text{day}}$$

Actual Idling:

$$\text{Actual Idling} = (1 - 0\%) \times 2,921 \frac{\text{Btu}}{\text{hr}} \times 11.03 \frac{\text{hrs}}{\text{day}} = 32,219 \frac{\text{Btu}}{\text{day}}$$

Residual Idling:

$$\text{Residual Idling} = 0\% \times \frac{125 \frac{\text{lbs}}{\text{hr}} \times 105 \frac{\text{Btu}}{\text{lb}}}{38\%} \times 11.03 \frac{\text{hrs}}{\text{day}} = 0 \frac{\text{Btu}}{\text{day}}$$

Daily idle energy:

$$\text{Daily Idle} = 32,219 \frac{\text{Btu}}{\text{day}} + 0 \frac{\text{Btu}}{\text{day}} = 32,219 \frac{\text{Btu}}{\text{day}}$$

Daily cooking:

$$\text{Daily Cooking} = \frac{100 \frac{\text{lb}}{\text{day}} \times 105 \frac{\text{Btu}}{\text{lb}}}{38\%} = 27,632 \frac{\text{Btu}}{\text{day}}$$

Total Daily Usage:

$$\text{NG Daily Usage} = \left(9,000 \frac{\text{Btu}}{\text{day}} + 32,219 \frac{\text{Btu}}{\text{day}} + 27,632 \frac{\text{Btu}}{\text{day}} \right) = 68,850 \frac{\text{Btu}}{\text{day}}$$

Total Annual Usage:

$$\text{NG Usage}_{\text{ENERGY STAR}} = 68,850 \frac{\text{Btu}}{\text{day}} \times 312 \frac{\text{days}}{\text{year}} = 21,481,265 \frac{\text{Btu}}{\text{year}}$$

Natural Gas Savings:

$$\text{NG}_{\text{savings}} = \left(339,168,826 \frac{\text{Btu}}{\text{year}} - 21,481,265 \frac{\text{Btu}}{\text{year}} \right) \times \frac{1}{35,738 \frac{\text{Btu}}{\text{m}^3}} = 8,889 \text{ m}^3$$

Water Savings:

$$\text{Water Saved} = 312 \frac{\text{days}}{\text{year}} \times 12 \frac{\text{hours}}{\text{day}} \times \left(136.3 \frac{\text{liters}}{\text{hour}} - 45.4 \frac{\text{liters}}{\text{hour}} \right) = 340,142 \frac{\text{liters}}{\text{year}}$$

USES AND EXCLUSIONS

To qualify for this measure the steam cooker must be utilized for food preparation or processing with natural gas as its energy source and be ENERGY STAR rated. The measure is limited to steam cookers that have either a connectionless or steam-generator design.

MEASURE LIFE

The measure life attributed to steam cookers is 12 years. [7]

INCREMENTAL COST

Table 4 presents the measure incremental cost. The average incremental cost for ENERGY STAR rated 6-pan, floor standing steam cookers, compared with standard efficiency steam cookers of the same type and capacity is listed.

Table 4. Incremental Cost [12]

Measure Category	Incremental Cost (\$)
New Construction/Time of Natural Replacement	\$3,880

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COMMERCIAL – INCREMENTAL HEAT RECOVERY VENTILATION (HRV) (55% EFFECTIVENESS BASELINE) – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	2
OEB Filing Date	December 22, 2017
OEB Approval Date	
Commercial → Space Heating → Incremental Heat Recovery Ventilation → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition			
Measure Category	New construction (NC) where HRV is required by Ontario Building Code Time of Natural Replacement (TNR)			
Baseline Technology	HRV with Minimum 55% Sensible Heat Recovery Effectiveness as per Ontario Building Code 2017, Supplement SB-10 January 1, 2017			
Efficient Technology	HRV with Minimum 65% Sensible Heat Recovery Effectiveness ¹ at 32°F			
	HRV with Minimum 75% Sensible Heat Recovery Effectiveness at 32°F			
	HRV with Minimum 85% Sensible Heat Recovery Effectiveness at 32°F			
Market Type	Commercial			
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE} 1	Group	Average Group Gas Savings (m ³ /working CFM)
Annual Natural Gas Savings Rate with a HRV with Minimum 65% Sensible Heat Recovery	Multi-Family, Health Care and Nursing Homes	0.77	High Use	0.77
	Hotels	0.55	Medium Use	0.43

¹ This measure is eligible for commercial buildings where Energy Star does not apply (the applicable OBC code is Supplementary Standard SB-10).

Parameter	Definition			
Effectiveness at 32°F, ϵ_{EE} 1 (m ³ / working CFM)	Restaurant	0.40	Low Use	0.27
	Retail	0.33		
	Office	0.29		
	Warehouse	0.28		
	School	0.25		
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /CFM), ϵ_{EE} 2	Group	Average Group Gas Savings (m ³ /working CFM)
Annual Natural Gas Savings Rate with a HRV with Minimum 75% Sensible Heat Recovery Effectiveness at 32°F, ϵ_{EE} 2 (m ³ / working CFM)	Multi-Family, Health Care and Nursing Homes	1.54	High Use	1.54
	Hotels	1.10	Medium Use	0.86
	Restaurant	0.80		
	Retail	0.67	Low Use	0.55
	Office	0.59		
	Warehouse	0.56		
	School	0.49		
Measure Efficiency	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE} 3	Group	Average Group Gas Savings (m ³ /working CFM)
Annual Natural Gas Savings Rate with a HRV with Minimum 85% Sensible Heat Recovery Effectiveness at 32°F, ϵ_{EE} 3 (m ³ /working CFM)	Multi-Family, Health Care and Nursing Homes	2.31	High Use	2.31
	Hotels	1.65	Medium Use	1.28
	Restaurant	1.20		
	Retail	1.00	Low Use	0.82
	Office	0.88		
	Warehouse	0.84		
	School	0.74		
Measure Life	14 Years			
Incremental Cost (\$)	\$1.00 per CFM at ϵ_{EE} 1			

Parameter	Definition
CAD)	\$2.00 per CFM at $\epsilon_{EE} 2$
	\$3.00 per CFM at $\epsilon_{EE} 3$
Restrictions	<p>This measure is not eligible in areas where:</p> <ul style="list-style-type: none"> • The HRV unit has an effectiveness of less than 65%, • 100% of the exhaust air must be evacuated from the building in order to avoid cross contamination, and therefore 100% fresh air is required such as described in OBC section 1.1.1.4. • No recirculation is allowed by codes or standards. For instance, any limitations as per CSA Z317.2_10 (Special Requirements for Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities), • Contaminants (gases and vapors) may be present and the HRV may bring them back into the breathing zone • Systems where DCV or scheduled setbacks are used during operated hours²

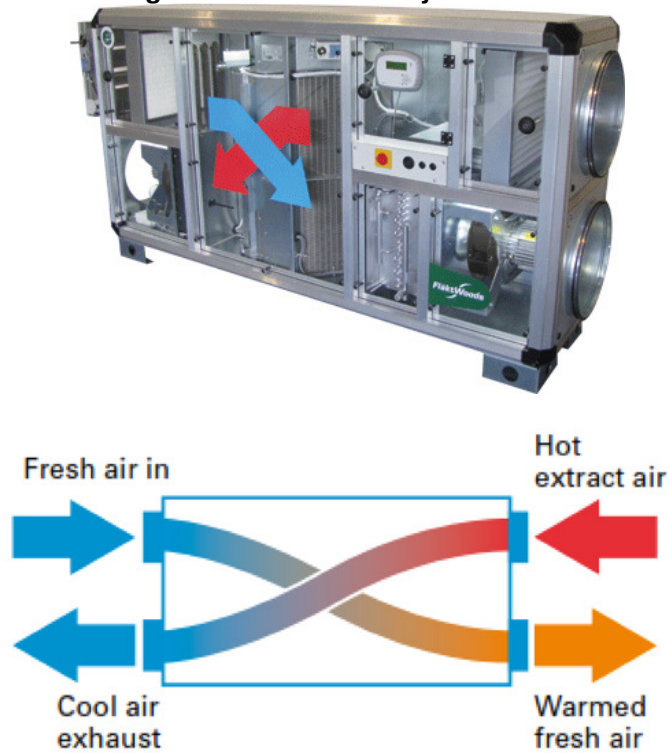
OVERVIEW

A heat recovery ventilator (HRV) refers to heat exchanger equipment that is designed to transfer sensible heat from the building exhaust air to the outside supply air. The temperature of the outside supply air is raised by the heat transferred from the exhaust air stream within the heat exchanger. By doing so, the amount of heat energy lost through the exhaust air stream is reduced and energy is saved through decreased load on the building heating system [1].

Figure 1 shows an example and a schematic of an HRV.

² These configurations require that projects be submitted as custom measures.

Figure 1: Heat Recovery Ventilator³



APPLICATION

The measure covers the installation of heat recovery ventilators in commercial settings. The performance of the HRV can be quantified by its sensible effectiveness, which is defined as the ratio of actual heat energy captured to the maximum heat energy that could be captured. This is a value determined during testing and varies with temperature difference. Sensible heat recovery effectiveness is not to be confused with total effectiveness which is a measure of the heat and moisture transfer. All references to effectiveness within this document refer to sensible effectiveness, not total effectiveness. Other performance parameters to be considered are the pressure drop over the HRV, and the method of frost control for the heat exchanger [2].

BASELINE TECHNOLOGY

The baseline is considered to be a building operating with the use of an HRV as per Ontario Building Code 2017 (SB-10) and as shown in Table 2. [3] [4]

³ From http://www.nfan.co.uk/what_are_heat_recovery_systems, 12/15/2014

Table 2. Baseline for Heat Recovery Ventilators

Type	Efficiency
HRV	HRV with 55% Sensible Heat Recovery Effectiveness per Ontario Building Code (OBC)

EFFICIENT TECHNOLOGY

The efficient technology is defined as an HRV with a sensible heat recovery effectiveness of at least 65% as shown in Table 3. Note, ENERGY STAR requires that qualifying HRVs have a minimum rated sensible effectiveness of 60% at -13°F (-25°C) and 65% at 32°F (0°C) [5].

Table 3. Efficient Technology for Heat Recovery Ventilators

Type	Efficiency
HRV ε_{EE1}	HRV with Minimum 65% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)
HRV ε_{EE2}	HRV with Minimum 75% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)
HRV ε_{EE3}	HRV with Minimum 85% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)

ENERGY IMPACTS

Heat is recovered from the outgoing exhaust air and added to the incoming supply air. Natural gas savings are achieved because the incoming supply air arrives at the building heating equipment at a higher temperature than it would without an HRV. This means that less energy is required to heat the supply air to the set point temperature.

NATURAL GAS SAVINGS ALGORITHMS

The following algorithms are used to calculate the gas impact in cubic meters and are formulae from ASHRAE Heating, Ventilating and Air Conditioning Systems and Equipment Handbook 2012, Chapter 26 [2]. The ASHRAE equations make the following assumptions: no vapor condensation within the HRV, no cross leakage, no heat gas from fan motors, and equal supply and exhaust air flow rates.

The energy saved by an HRV is a function of the heat transfer rate through the heat exchanger and the length of time it operates. The heat transfer rate can be calculated from the temperature difference between the supply and exhaust air entering the HRV the average effectiveness of the HRV, the physical properties of air and the flow rate

through the HRV. A defrost factor must also be considered to account for the time that exhaust air is diverted through the core in order to prevent freezing, which impedes the operation of the HRV.

The natural gas savings rates in Table 1 are calculated using the following formulae.

$$hrs = Heathrs \times \frac{weeklyhrs}{168 \frac{hrs}{week}}$$

and,

$$NG\ Savings = hrs \times \frac{60min}{hr} \times \rho \times \frac{(\epsilon_{EE} - 55\%)}{\eta} \times \frac{C_p}{35,738 \frac{Btu}{m^3}} \times (T_3 - T_1) \times \left(1 - \frac{DF}{100\%}\right)$$

Where,

<i>hrs</i>	= Annual hours that the HRV is expected to be in use (hours/year)
<i>Heathrs</i>	= Number of hours in the heating season (hours/year)
<i>weeklyhrs</i>	= Number of weekly operating hours (hours/week)
$168 \frac{hrs}{week}$	= Number of hours in a week
<i>NG Savings</i>	= Annual natural gas savings per CFM of HRV (m ³ /CFM/year)
$\frac{60min}{hr}$	= Conversion from minutes to hours
ϵ_{EE}	= Sensible effectiveness of the high efficiency HRV (%)
η	= The efficiency of the building's heating system (%)
C_p	= Specific heat of air (Btu/lb _m -°F)
ρ	= Density of air at 72°F (lb _m /ft ³)
$35,738 \frac{Btu}{m^3}$	= Conversion from Btu to m ³ of natural gas
T_3	= Temperature of the inside (exhaust) air entering the HRV (°F)
T_1	= Average outside temperature during heating hours (°F)
<i>DF</i>	= Defrost control de-rating factor (%)

ASSUMPTIONS

Table 4 shows the list of assumptions used in the algorithms sections.

Table 4. Assumptions

Variable	Definition	Value	Source
<i>Heathrs</i>	Hours in Heating Season, 55°F Balance Temperature ⁴	5,567 hrs	Common assumptions table
ϵ_{EE1}	Minimum sensible effectiveness	65%	
ϵ_{EE2}	Minimum sensible effectiveness	75%	
ϵ_{EE3}	Minimum sensible effectiveness	85%	
ρ	Density of the exhaust air	0.0741 lb _m /ft ³	Common assumptions table
η	Efficiency of gas fired heating equipment	80%	Common assumptions table
C_p	Specific heat of air	0.240 Btu/lb _m -°F	Common assumptions table
<i>DF</i>	Defrost control de-rating factor	5% ⁵	[7] [8] [9] [10]
T1	Average temperature of outside (supply) air during the heating season (OA temperature heating system enabled)	33.03°F	Common assumptions table
T3	Average temperature of inlet exhaust air (Space Temperature Setpoint)	72°F	Common assumptions table

The assumed weekly hours of operation for different building types are given in Table 5.

Table 5. Hours of Weekly Operation [10]

Building Type	Hours of Operation per Week
Multi-Family	168
Health Care	168
Nursing Home	168

⁴ The annual heating hours, and average outside air temperature, assume an average building balance temperature of 55°F, which is the temperature at which neither heating nor cooling is required. The actual balance point for a particular application will vary based on building construction, internal loads, HVAC system zoning, and other factors.

⁵ All air-to-air heat recovery equipment requires frost control in colder climates to prevent freeze-up of exhaust air condensate on heat exchange components. There are different types of frost control methods and depending on the defrost control system, annual heat recovery estimates should be reduced by 5% to 15%. The cited Nexant document specifically considers the factor for Ontario (p. 6-47 and 6-48) and recommends 5% as a conservative value for the base case scenario.

Building Type	Hours of Operation per Week
Hotel	120
Restaurant	87
Retail	73
Office	64
Warehouse	61
School	54

EXAMPLE

For this example, it will be assumed that a new health care facility installs an HRV unit working at 500 CFM with a sensible effectiveness of 75%. In this case the ϵ_{EE2} is applicable.

$$hrs = 5,567 \frac{hrs}{year} \times \frac{168 \frac{hrs}{week}}{168 \frac{hrs}{week}} = 5,567 \frac{hrs}{year}$$

and,

$$NG\ Savings = 5,567 \frac{hrs}{year} \times \frac{60min}{hr} \times 0.0741 \frac{lb_m}{ft^3} \times \frac{75\% - 55\%}{80\%} \times \frac{0.240 \frac{Btu}{lb_m \cdot ^\circ F}}{35,738 \frac{Btu}{m^3}} \\ \times (72^\circ F - 33^\circ F) \times \left(1 - \frac{5\%}{100\%}\right) = 1.54 \frac{m^3}{CFM \cdot year}$$

Therefore,

$$NG\ Savings = 500CFM \times 1.54 \frac{m^3}{CFM \cdot year} = 769 \frac{m^3}{year}$$

USES AND EXCLUSIONS

This measure is intended for buildings with an existing HRV, or a new construction building that requires a heat recovery system. For buildings without an existing HRV, or new buildings not requiring a heat recovery system, please see supporting measure with no HRV baseline. Other restrictions include:

- Measure not applicable to areas and rooms where 100% fresh air is required.
- Measure not applicable to areas and rooms where no recirculation is allowed by codes or standards. For instance, CSA Z317.2_10 (Special Requirements for

Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities).

- Measure not applicable to areas and rooms where contaminants (gases and vapors) may be present and the HRV may bring them back into the breathing zone.
- Measure not applicable to systems where no DCV or scheduled setbacks are required.

MEASURE LIFE

A 14-year measure life is recommended by DEER is based on KEMA-XENERGY's Retention Study of PG&Es 1996-1997 Energy Incentive Program. This study tracked installed equipment over 6 years and used statistical analysis to calculate EUL [11].

INCREMENTAL COST

The incremental costs, representing differences in equipment costs, between baseline units meeting minimum code efficiency and high efficiency units are \$1.00 per CFM at 65%, \$2.00 at 75%, and \$3.00 at 85% efficiency⁶ [12].

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⁶ Based on a manufacturer's estimate that typical incremental installed cost premium for 85% efficiency heat recovery units are \$3.00 /cfm greater than for 50% efficiency units.

Come into effect January 1, 2017.

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COMMERCIAL – INCREMENTAL HEAT RECOVERY VENTILATION (HRV) (NO HRV BASELINE) – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	2
OEB Filing Date	December 22, 2017
OEB Approval Date	
Commercial → Space Heating → Incremental Heat Recovery Ventilation → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition			
Measure Category	New construction (NC) where no HRV is required by Ontario Building Code Retrofit (R)			
Baseline Technology	No HRV			
Efficient Technology	HRV with minimum 55% Sensible Heat Recovery Effectiveness ¹ at 32°F			
	HRV with minimum 65% Sensible Heat Recovery Effectiveness at 32°F			
	HRV with minimum 75% Sensible Heat Recovery Effectiveness at 32°F			
	HRV with minimum 85% Sensible Heat Recovery Effectiveness at 32°F			
Market Type	Commercial			
Annual Gas Savings Rate With a Minimum HRV Sensible Heat Recovery Effectiveness of	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE}^1	Group	Average Group Gas Savings (m ³ /working CFM) ϵ_{EE}^1
	Multi-Family, Health	4.23	High Use	4.23

¹ This measure is eligible for commercial buildings where Energy Star does not apply (the applicable OBC code is Supplementary Standard SB-10).

Some commercial buildings are required by SB-10 to have Energy Recovery Ventilation or Heat Recovery Ventilation with a minimum of 55% sensible effectiveness. For buildings with no code requirement, systems that bring efficiency up to code level (55% sensible effectiveness) are eligible.

Parameter	Definition			
55%, $\epsilon_{EE} 1$ (m ³ /working CFM)	Care and Nursing Homes			
	Hotels	3.02	Medium Use	2.35
	Restaurant	2.19		
	Retail	1.84		
	Office	1.61	Low Use	1.50
	Warehouse	1.54		
	School	1.36		
Annual Gas Savings Rate With a Minimum HRV Sensible Heat Recovery Effectiveness of 65%, $\epsilon_{EE} 2$ (m ³ /working CFM)	Building Type	Gas Savings Rate (m³/working CFM), $\epsilon_{EE} 2$	Group	Average Group Gas Savings (m³/working CFM) $\epsilon_{EE} 2$
	Multi-Family, Health Care and Nursing Homes	5.00	High Use	5.00
	Hotels	3.57	Medium Use	2.78
	Restaurant	2.59		
	Retail	2.18		
	Office	1.91	Low Use	1.78
	Warehouse	1.82		
School	1.61			
Annual Gas Savings Rate With a Minimum HRV Sensible Heat Recovery Effectiveness of 75%, $\epsilon_{EE} 3$ (m ³ /working CFM)	Building Type	Gas Savings Rate (m³/working CFM), $\epsilon_{EE} 3$	Group	Average Group Gas Savings (m³/working CFM) $\epsilon_{EE} 3$
	Multi-Family, Health Care and Nursing Homes	5.77	High Use	5.77
	Hotels	4.12	Medium Use	3.21
	Restaurant	2.99		
	Retail	2.51		
	Office	2.20	Low Use	2.05
	Warehouse	2.10		

Parameter	Definition			
	School	1.86		
Annual Gas Savings Rate With a Minimum HRV Sensible Heat Recovery Effectiveness of 85%, ϵ_{EE}^4 (m ³ /working CFM)	Building Type	Gas Savings Rate (m ³ /working CFM), ϵ_{EE}^4	Group	Average Group Gas Savings (m ³ /working CFM) ϵ_{EE}^4
	Multi-Family, Health Care and Nursing Homes	6.54	High Use	6.54
	Hotels	4.67	Medium Use	3.64
	Restaurant	3.39		
	Retail	2.84		
	Office	2.49	Low Use	2.32
	Warehouse	2.38		
	School	2.10		
Annual Electric Penalty ² (kWh/working CFM)	Building Type	Electric Penalty Rate (kWh/working CFM)	Group	Average Group Electric Penalty (kWh/working CFM)
	Multi-Family, Health Care and Nursing Homes	4.62	High Use	4.62
	Hotels	3.30	Medium Use	2.57
	Restaurant	2.39		
	Retail	2.01		
	Office	1.76	Low Use	1.64
	Warehouse	1.68		
	School	1.49		
Measure Life	14 Years			
First Incremental Cost (\$ CAD) ϵ_{EE}^1	Integrated HRV		Standalone or Bolt-On HRV	
	\$5.35/CFM		\$8.28/CFM	

² The electric penalty does not apply when the HRV unit is installed as part of an integrated HVAC package.

Incremental Cost (\$ CAD)	\$5.35 + \$1.00 per CFM at $\epsilon_{EE} 2$	\$8.28 + \$1.00 per CFM at $\epsilon_{EE} 2$
	\$5.35 + \$2.00 per CFM at $\epsilon_{EE} 3$	\$8.28 + \$2.00 per CFM at $\epsilon_{EE} 3$
	\$5.35 + \$3.00 per CFM at $\epsilon_{EE} 4$	\$8.28 + \$3.00 per CFM at $\epsilon_{EE} 4$

Restrictions	<p>This measure is not eligible in areas where:</p> <ul style="list-style-type: none"> • HRV is required by building code, • 100% of the exhaust air must be evacuated from the building in order to avoid cross contamination, and therefore 100% fresh air is required such as described in OBC section 1.1.1.4. • No recirculation is allowed by codes or standards. For instance, any limitations as per CSA Z317.2_10 (Special Requirements for Heating, Ventilation, and Air Conditioning (HVAC) Systems in Health Care Facilities), • Contaminants (gases and vapors) may be present and the HRV may bring them back into the breathing zone • Systems where DCV or scheduled setbacks are used during operated hours³
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OVERVIEW

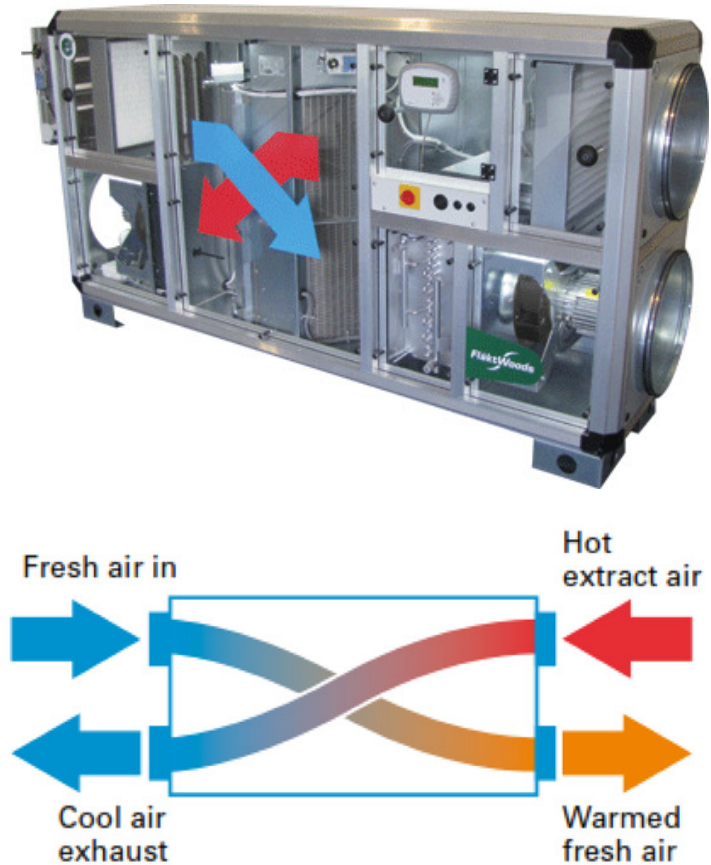
A heat recovery ventilator (HRV) refers to heat exchanger equipment that is designed to transfer sensible heat from the building exhaust air to the outside supply air. The temperature of the outside supply air is raised by the heat transferred from the exhaust air stream within the heat exchanger. By doing so, the amount of heat energy lost through the exhaust air stream is reduced and energy is saved through decreased load on the building heating system [1].

One component of HRVs includes circulation fans, which are typically high efficiency electrically commutated motors. These will consume more electrical energy in cases where HRV unit is added to the existing HVAC system as a standalone or bolt-on unit [1]. No penalty is assigned if the HRV is integrated as part of the HVAC packaged system installed at retrofit or new construction because the higher efficiency of the new fans compensates for the additional static pressure.

An important distinction to make for an HRV is that it does not transfer moisture between the air streams like an energy recovery ventilator would. Figure 1 shows an example and a schematic of a heat recovery ventilator.

³ These configurations require that projects be submitted as custom measures.

Figure 1. Heat Recovery Ventilator⁴



APPLICATION

The measure covers the installation of heat recovery ventilators in commercial settings. The performance of the HRV can be quantified by its sensible effectiveness, which is defined as the ratio of actual heat energy captured to the maximum heat energy that could be captured. This is a value determined during testing and varies with temperature difference. Sensible heat recovery effectiveness is not to be confused with total effectiveness which is a measure of the heat and moisture transfer. All references to effectiveness within this document refer to sensible effectiveness, not total effectiveness. Other performance parameters to be considered are the pressure drop over the HRV, and the method of frost control for the heat exchanger [2].

⁴From http://www.nfan.co.uk/what_are_heat_recovery_systems, 12/15/2014

BASELINE TECHNOLOGY

The baseline is considered to be a building operating without the use of a HRV as shown in Table 2. This implies that no heat is being recovered between the exhausted inside air and the incoming outside supply air.

Table 2. Baseline for Heat Recovery Ventilators

Type	Efficiency
No HRV	No Heat Recovery

EFFICIENT TECHNOLOGY

The efficient technology is an HRV with a sensible effectiveness of 55%, 65%, 75%, and 85% as shown in Table 3. Note, ENERGY STAR requires that qualifying HRVs have a minimum rated effectiveness of 60% at -13°F (-25°C) and 65% at 32°F (0°C) [3].

Table 3. Efficient Technology for Heat Recovery Ventilators

Type	Efficiency
HRV ϵ_{EE1}	Minimum 55% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)
HRV ϵ_{EE2}	Minimum 65% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)
HRV ϵ_{EE3}	Minimum 75% with Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)
HRV ϵ_{EE4}	Minimum 85% Sensible Heat Recovery Effectiveness at 32°F at working airflow (CFM)

ENERGY IMPACTS

Natural gas savings are achieved because the incoming supply air arrives at the building heating equipment at a higher temperature than it would without an HRV. This means that less energy is required to heat the supply air to the set point temperature.

An electrical penalty is incurred due to the operation of HRV fans or increased load on central fans, except when the HRV is integrated as part of the HVAC package.

NATURAL GAS SAVINGS ALGORITHMS

The following algorithms are used to calculate the gas impact in cubic meters and are formulae from ASHRAE 2012, chapter 26 [2]. The ASHRAE equations make the following assumptions: no vapor condensation within the HRV, no cross leakage, no heat gas from fan motors, and equal supply and exhaust air flow rates.

The energy saved by an HRV is a function of the heat transfer rate through the heat exchanger and the length of time it operates. The heat transfer rate can be calculated from the temperature difference between the supply and exhaust air entering the HRV the average effectiveness of the HRV, the physical properties of air and the flow rate through the HRV. A defrost factor must also be considered to account for the time that exhaust air is diverted through the core in order to prevent freezing, which impedes the operation of the HRV.

$$hrs = Heathrs \times \frac{weeklyhrs}{168 \frac{hrs}{week}}$$

and,

$$NG\ Savings = hrs \times \frac{60min}{hr} \times \rho \times \frac{\epsilon_{EE}}{\eta} \times \frac{C_p}{35,738 \frac{Btu}{m^3}} \times (T_3 - T_1) \times \left(1 - \frac{DF}{100\%}\right)$$

Where,

hrs	= Annual hours that the HRV is expected to be in use (hours/year)
$Heathrs$	= Number of hours in the heating season (hours/year)
$weeklyhrs$	= Number of weekly operating hours (hours/week)
$168 \frac{hrs}{week}$	= Number of hours in a week
$NG\ Savings$	= Annual natural gas savings per CFM of HRV (m ³ /CFM/year)
$\frac{60min}{hr}$	= Conversion from minutes to hours
ρ	= Density of air at 72 °F (lb _m /ft ³)
ϵ_{EE}	= Sensible effectiveness of the high efficiency HRV (%) ⁵
η	= The efficiency of the building's heating system (%)
C_p	= Specific heat of air (Btu/lb _m -°F)
$35,738 \frac{Btu}{m^3}$	= Conversion from Btu to m ³ of natural gas
T_3	= Temperature of the inside (exhaust) air entering the HRV (°F)
T_1	= Average outside temperature during heating hours (°F)
DF	= Defrost control de-rating factor (%)

⁵ Note, for this analysis the rated effectiveness is being used as an average effectiveness.

ELECTRIC ENERGY PENALTY ALGORITHMS (FOR HRVs ADDED TO AN EXISTING SYSTEM)

The electric penalty is based on the ENERGY STAR minimum fan efficiency requirements of 0.83 W/CFM. Using this value, and the calculated hours of HRV operation from the natural gas algorithms, the kWh electric penalty can be calculated using the following equation.

The kWh fan penalty analysis presumes that the system has an automatic bypass damper so that there is no added pressure drop during hours when heat recovery is not needed.

$$kWh \text{ penalty} = 0.83 \frac{W}{CFM} \times hrs \div 1000 \frac{W}{kW}$$

Where,

$kWh \text{ penalty}$ = The annual electric penalty per CFM of HRV capacity (kWh/ft³/min/year)

$0.83 \frac{W}{CFM}$ = Minimum efficacy to be qualified for ENERGY STAR (1.20 CFM/W)

hrs = Annual hours that the HRV is expected to be in use (hours/year)

ASSUMPTIONS

Table 4 shows the list of assumptions used in the algorithms sections.

Table 4. Assumptions

Variable	Definition	Value	Source
<i>Heathrs</i>	Hours in Heating Season, 55°F Balance Temperature ⁶	5,567 hrs	Common assumptions table
ϵ_{EE1}	Sensible effectiveness	55%	
ϵ_{EE2}	Sensible effectiveness	65%	
ϵ_{EE3}	Sensible effectiveness	75%	
ϵ_{EE4}	Sensible effectiveness	85%	
ρ	Density of the exhaust air	0.0741 lb _m /ft ³	Common assumptions table

⁶ The annual heating hours, and average outside air temperature, assume an average building balance temperature of 55°F, which is the temperature at which neither heating nor cooling is required. The actual balance point for a particular application will vary based on building construction, internal loads, HVAC system zoning, and other factors.

Variable	Definition	Value	Source
η	Commercial Heating System Efficiency	80%	Common assumptions table
C_p	Specific heat of air	0.240 Btu/lb _m °F	Common assumptions table
T_1	Average temperature of outside (supply) air during the heating season (OA temperature heating system enabled)	33.03 °F	Common assumptions table
T_3	Average temperature of inlet exhaust air (Space temperature setpoint)	72 °F	Common assumptions table
Fan Efficiency	Assumed fan efficiency	0.83 W/CFM	[3]
DF	Defrost control de-rating factor	5% ⁷	[1], [2], [7], [6]

The assumed weekly hours of operation for different building types are given in Table 5.

Table 5. Hours of Weekly Operation [6]

Building Type	Hours of Operation per Week
Multi-Family	168
Health Care	168
Nursing Home	168
Hotel	120
Restaurant	87
Retail	73
Office	64
Warehouse	61
School	54

⁷ All air-to-air heat recovery equipment requires frost control in colder climates to prevent freeze-up of exhaust air condensate on heat exchanger components. There are different types of frost control methods and depending on the defrost control system, annual heat recovery estimates should be reduced by 5% to 15%.

EXAMPLE

For this example, it is assumed that a new health care facility installs an HRV unit working at 500 CFM with a total effectiveness of 65%. In this case the ε_{EE2} is applicable.

$$hrs = 5,567hrs \times \frac{168 \frac{hrs}{week}}{168 \frac{hrs}{week}} = 5,567 \frac{hrs}{year}$$

and,

$$NG \text{ Savings} = 5,567 \frac{hrs}{year} \times \frac{60min}{hr} \times 0.0741 \frac{lb_m}{ft^3} \times \frac{65\%}{80\%} \times \frac{0.240 \frac{Btu}{lb_m - ^\circ R}}{35,738 \frac{Btu}{m^3}} \times (72^\circ F - 33^\circ F) \\ \times \left(1 - \frac{5\%}{100\%}\right) = 5.00 \frac{m^3}{CFM \cdot year}$$

Therefore,

$$NG \text{ Savings} = 500CFM \times 5.00 \frac{m^3}{CFM \cdot year} = 2,500 \frac{m^3}{year}$$

The electrical penalty can be calculated as the following.

$$kWh \text{ penalty} = 500 CFM \times 0.83 \frac{W}{CFM} \times 5,567 \frac{hrs}{year} \times \frac{1kW}{1000W} = 2,310 \frac{kWh}{year}$$

USES AND EXCLUSIONS

- Restriction for new building construction: This measure is not applicable to buildings in which an HRV is required by the Ontario Building Code (SB-10) . [8] Note, please see supporting measure that utilizes code minimum as baseline for these scenarios.
- Restriction for new building construction: This measure is not applicable to systems serving health care spaces indicated in Table 1 because heat recovery is required by CSA Z317.2-01

MEASURE LIFE

A 14-year measure life is recommended by DEER and is based on KEMA-XENERGY's Retention Study of PG&Es 1996-1997 Energy Incentive Program. This study tracked installed equipment over 6 years and used statistical analysis to calculate EUL [9].

INCREMENTAL COST

Table 6 demonstrates the incremental cost of heat recovery ventilators. ERS used RSMMeans corroborated with manufacturer data to determine the first costs for integrated systems at \$5.66/CFM and for standalone or bolt-on units at \$8.76/CFM. These costs values are also supported by the 2010 Nexant review of the measure. The additional cost for standalone or bolt-on units is due to the additional materials and equipment required, as well as the labor associated with integrating the standalone or bolt-on system with the existing ventilation system [10].

The first costs represent the incremental costs between no HRV and 55% efficient units. Additional incremental costs between high efficiency units are \$1.00 per CFM at 65%, \$2.00 at 75%, and \$3.00 at 85% efficiency⁸ [11].

Table 6. Incremental Cost⁹ [6] [10]

Measure Type	Cost
First Cost Integrated units	\$5.35/CFM
First Cost Bolted-on systems	\$8.28/CFM

REFERENCES

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⁸ Based on a manufacturer's estimate that typical incremental installed cost premium for 85% efficiency heat recovery units are \$3.00 /cfm greater than for 50% efficiency units.

⁹ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 11/30/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

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COMMERCIAL – HIGH EFFICIENCY CONDENSING FURNACE – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → High Efficiency Condensing Furnace → New Construction /Time of Natural Replacement	

Table 1 below provides a summary of the key measure parameters and savings coefficient.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)	
Baseline Technology	90% AFUE	
Efficient Technology	≥ 95% AFUE	
Market Type	Commercial, Multiresidential	
Annual Natural Gas Savings Rate (m ³ /kBtu/hr)	New Construction	2.33 m ³ per kBtu/hr input capacity
	Time of Natural Replacement	3.11 m ³ per kBtu/hr input capacity
Measure Life	18 years	
Incremental Cost (\$ CAD)	\$494	
Restriction	Must have a rated efficiency of at least 95% and must be a standalone furnace	

OVERVIEW

The measure is for the installation of high efficiency condensing furnaces with an annual fuel utilization efficiency (AFUE) of 95% or higher in commercial buildings. High efficiency gas furnaces achieve savings through the utilization of a sealed, super insulated combustion chamber, more efficient burners, and multiple heat exchangers

that remove a significant portion of the waste heat from the flue gases. Because multiple heat exchangers are used to remove waste heat from the escaping flue gasses, most of the flue gasses condense and must be drained.

APPLICATION

The measure is for the installation of condensing furnaces which have efficiencies that exceed code requirements. Commercial furnaces are typically categorized as being of an input capacity greater than 225 kBtu/hr and are performance-rated by their thermal efficiency. Investigation into the commercial furnace market shows that furnaces greater than 225 kBtu/hr are not made with efficiencies greater than 82% [1]. Because there is no large, high efficiency commercial furnace equipment, this measure is intended to support the purchase of smaller, less than 225 kBtu/hr, high efficiency furnaces.

Furnaces less than 225 kBtu/hr are performance rated by their annual fuel utilization efficiency or AFUE. This is a measure of the seasonal performance of the equipment and is a more comprehensive system efficiency than combustion or thermal efficiency measurements.

BASELINE TECHNOLOGY

Canada’s Energy Efficiency Regulations require that new furnaces under 225 kBtu/hr have at least a 90% AFUE [2]. For new construction installations, the baseline technology is considered to be the minimum efficiency required by the regulations established December 31, 2009.

Table 2. Baseline Technology AFUE

Type	AFUE
Gas Condensing Furnace	90%

EFFICIENT TECHNOLOGY

The efficient technology is a condensing furnace with a thermal efficiency rating equal to, or higher than 95%. This is the minimum efficiency for an ENERGY STAR furnace in Canada, effective February 1, 2013 [3].

Table 3. Efficient Technology AFUE

Type	AFUE
Gas Condensing Furnace	95%

ENERGY IMPACTS

The primary energy impact associated with the installation of condensing furnaces in this service territory is a reduction in natural gas usage resulting from the furnace's improved efficiency.

No water consumption or electric impacts are associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

The measure gas savings are calculated using a common assumption for the equivalent full load hours (EFLH) and the difference in assumed efficiencies for the equipment. The annual natural gas savings for a given size furnace can be calculated by multiplying the rated input of the furnace times the savings factor¹.

The natural gas savings factor attributed to this measure is calculated using the following formula:

$$NG\ Savings\ Factor = \frac{EFLH}{35.738 \frac{kBtu}{m^3}} \times \left(\frac{AFUE_{EE}}{AFUE_{base}} - 1 \right)$$

where,

<i>NG Savings Factor</i>	= Annual gas savings per input capacity resulting from installing the new furnace (m ³ /yr)/(kBtu/hr)
<i>EFLH</i>	= Equivalent full load hours (hrs), see Table 4
$35.738 \frac{kBtu}{m^3}$	= Conversion of rated heating capacity from input kBtu/hr to m ³ /hr, common assumptions table
<i>AFUE_{base}</i>	= Baseline equipment thermal efficiency (%), see Table 2
<i>AFUE_{EE}</i>	= Efficient equipment thermal efficiency (%), see Table 3

ELECTRIC ENERGY SAVINGS

The Ontario Building Code requires that all furnaces installed in new construction with permit pull dates after December 31, 2014 use brushless direct current motors (also known as electronically commutated motors, or ECMs). Such motors are significantly more efficient than traditional permanent split capacitor (PSC) type motors. With this code elevation there is no electricity savings associated with the ECMs often installed with new condensing furnaces [4].

¹ The Regulations are defined based on Btu/hr of gas input and residential boilers and most commercial heating equipment are also rated based on input capacity. Note that some furnace manufacturers rate the capacity based on Btu/hr output. For example, spot checks of manufacturer literature in August 2014 found that Trane, and Bryant publish furnace capacity based on output; Carrier and Rheem list input capacity. Increase the savings by 5% if output capacity is the basis.

ASSUMPTIONS

The assumptions used to calculate the savings coefficient are shown in Table 4.

Table 4. Assumptions

Variable	Definition	Inputs		Source
<i>EFLH</i>	Equivalent full load hours	NC	1,500 hours	Common assumptions table
		TNR	2,000 hours	

*

SAVINGS CALCULATION EXAMPLE

The example below shows how to calculate gas savings achieved from installing one condensing furnace with a rated input of 110 kBtu/h from the savings factor in Table 1.

$$NG \text{ Savings Factor} = \frac{1,500 \text{ hrs}}{35.738 \frac{\text{kBtu}}{\text{m}^3}} \times \left(\frac{95\%}{90\%} - 1 \right) = \frac{2.33 \text{ (m}^3/\text{yr)}}{\frac{\text{kBtu}}{\text{hr}}}$$

And,

$$Annual \text{ NG savings} = \frac{2.33 \left(\frac{\text{m}^3}{\text{yr}} \right)}{\frac{\text{kBtu}}{\text{hr}}} \times 110 \frac{\text{kBtu}}{\text{hr}} = 256 \text{ m}^3$$

USES AND EXCLUSIONS

To qualify for this measure the condensing furnaces must be gas-fired, have an AFUE of at least 95% and be installed in a new commercial facility. The measure applies to standalone furnaces and not to heating systems that are part of rooftop units or to unvented make-up air heaters.

MEASURE LIFE

The measure life attributed to this measure is 18 years [5] [6]. Expert opinions and studies cited by NRCAN are 15, 18, and 20 years [7]. The ASHRAE handbook states that most heat exchangers have a design life of 15 years and the design life of commercial heating equipment is about 20 years [8]

INCREMENTAL COST

The measure incremental cost is \$494² based on the average difference in incremental cost between 90 AFUE and 94 AFUE residential furnaces. [9]

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² Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016.
(<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

COMMERCIAL – HIGH EFFICIENCY UNDER-FIRED BROILER – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Food Service → High Efficiency Underfired Broilers → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters.

Table 1. Measure Key Data

Parameter	Definitions			
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)			
Baseline Technology	A conventional under-fired broiler, see table 2			
Efficient Technology	A high-efficiency under-fired broiler, see table 3			
Market type	Commercial			
Annual Natural Gas Savings ¹ (m ³)	Three-foot 2,511 m ³	Four-foot 3,347 m ³	Five-foot 4,184 m ³	Six-foot 5,021 m ³
Measure Life	12 years			
Incremental Cost ¹ (\$ CAD)	\$1,900			
Restrictions	Restricted to commercial/institutional food service broiler using natural gas, 3-foot or larger			

OVERVIEW

Under-fired broilers (often referred to as “charbroilers”) are used in commercial and institutional food service to do a range of tasks that range from melting cheese to cooking large cuts of meat. Under-fired broilers come in different sizes ranging from three-foot to six-foot. High efficiency broilers utilize improved radiant design and burner control to allow lower firing and gas input levels during both preheat and cooking modes.

The basic design of an under-fired broiler is a suspended metal grill with heat applied from below. Due to their preheat times (up to 30 minutes), broilers are allowed to idle

¹ Broiler sizes are nominal and may vary ½-foot +/- within each category.

during the day. They usually idle at full input so that they are ready to cook when they are needed. It is possible for operators to manually turn down the input, when not actively cooking, but our research revealed no automatic controls that modulate the broilers.

APPLICATION

Under-fired broilers consume natural gas when they are pre-heating and cooking. This measure provides incentives for installing a high efficiency under-fired broilers in commercial or institutional cooking settings. An under fired broiler is designed to cook food on a metal grill with the heat source below the food. The broiler is typically left on during all operating hours so that the broiler is instantly available for cooking. [1]

BASELINE TECHNOLOGY

The baseline technology is a conventional under-fired broiler.

Table 2. Baseline Technology [2]

Type	Inputs
Conventional under-fired broiler	<p>Under-fired broiler, with pre-heat energy and a cooking energy rate at or below the following standard.</p> <ul style="list-style-type: none"> • Three foot broiler: pre-heat of 48,000 Btu or less and a cooking energy rate of 96,000 Btu/hr or less • Four foot broiler: pre-heat between 48,001 and 64,000 Btu and a cooking energy rate between 96,001 and 128,000 Btu/hr • Five foot broiler: pre-heat between 64,001 and 80,000 Btu and a cooking energy rate between 128,001 and 160,000 Btu/hr • Six foot broiler: pre-heat between 80,001 and 96,000 Btu and a cooking energy rate between 160,001 and 192,000 Btu/hr

EFFICIENT TECHNOLOGY

The efficient technology is a high-efficiency under-fired broiler designed to operate at lower firing and input levels.

Table 3. Efficient Technology [2]

Type	Requirement
High Efficiency Under-Fired broiler	<p>Under-fired broiler, with pre-heat energy and a cooking energy rate at or below the following standard.</p> <ul style="list-style-type: none"> • Three foot broiler: pre-heat of 40,500 Btu or less and a cooking energy rate of 72,000 Btu/hr or less

Type	Requirement
	<ul style="list-style-type: none"> • Four foot broiler: pre-heat between 40,501 and 54,000 Btu and a cooking energy rate between 72,001 and 96,000 Btu/hr • Five foot broiler: pre-heat between 54,001 and 67,500 Btu and a cooking energy rate between 96,001 and 120,000 Btu/hr • Six foot broiler: pre-heat between 67,501 and 81,000 Btu and a cooking energy rate between 120,001 and 144,000 Btu/hr

ENERGY IMPACTS

The primary energy impact associated with the installation of a high efficiency under-fired broiler is a reduction in natural gas required during the pre-heat and cook/idle modes. According to the Food Service Technology Center, broilers typically operate continuously with operators leaving the equipment at full burner output, regardless of cooking status. The energy savings is achieved through better radiant design and better burner control which allow lower gas input rates during preheating and idling/cooking activities. There are no electric impacts for this measure.

NATURAL GAS SAVINGS ALGORITHM

The algorithm to determine energy savings is calculated determining and comparing the annual energy usage for a conventional and a high efficiency under-fired broiler. To determine total energy usage, the calculation uses the energy used to pre-heat the broiler and the energy used when cooking.

The savings algorithm is based upon the methodology developed by the Food Service Technology Center. The following calculation determines the energy usage of a conventional and high efficiency under-fired broiler:

$$NG\ Usage = Days \times (Daily\ Preheat + Full\ Burn\ Load \times Cook\ Time)$$

where,

- NG Usage = the amount of natural gas used by the broiler annually in Btu/year
- Days = the number of days per year the broiler is in use
- Daily Preheat = the amount of natural gas used to preheat the broiler daily in Btu/day
- Full Burn Load = the rate of natural gas used when the unit is in cooking mode in Btu/hr
- Cook Time = the number of hours per day that the unit is cooking

The savings is then calculated from the difference between the baseline and efficient cases.

$$NG_{savings} = (NG Usage_{baseline} - NG Usage_{high\ efficiency}) \times \frac{1m^3}{35,738Btu}$$

where,

- $NG_{savings}$ = annual reduction in natural gas consumption in m³/year
- $NG Usage_{baseline}$ = annual energy usage of a conventional broiler in Btu/year
- $NG Usage_{high\ efficiency}$ = annual energy usage for a high efficiency broiler in Btu/year

ASSUMPTIONS

The assumptions used to calculate natural gas savings are shown in Table 4.

Table 4. Assumptions

Parameter	Baseline	High Efficiency	Source
Food Service Days per Year	312		Common assumptions table
Cook Time (hours)	12		[3]
Preheat time (hours)	0.33		[3]
Three foot broiler			
Daily Preheat (Btu)	48,000	40,500	[2]
Full Burn Load (Btu/hr)	96,000	72,000	[2]
Four foot broiler			
Daily Preheat (Btu)	64,000	54,000	[2]
Cooking (Btu/hr)	128,000	96,000	[2]
Five foot broiler			
Daily Preheat (Btu)	80,000	67,500	[2]
Cooking (Btu/hr)	160,000	120,000	[2]
Six foot broiler			
Daily Preheat (Btu)	96,000	81,000	[2]
Cooking (Btu/hr)	192,000	144,000	[2]

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the deemed savings value is determined for a three foot high efficiency under-fired broiler with typical hours of usage.

Annual Conventional Broiler Usage:

$$\begin{aligned} \text{NG Usage} &= 312 \times (48,000 \text{ Btu} + 96,000 \text{ Btu/h} \times (12 \text{ hours} - 0.33 \text{ hours})) \\ &= 364,515,840 \text{ Btu} \end{aligned}$$

Annual High Efficiency Broiler Usage:

$$\begin{aligned} \text{NG Usage} &= 312 \times (40,500 \text{ Btu} + 72,000 \text{ Btu/h} \times (12 \text{ hours} - 0.33 \text{ hours})) \\ &= 274,790,880 \text{ Btu} \end{aligned}$$

Natural Gas Savings:

$$\text{NG}_{\text{savings}} = (364,515,840 \text{ Btu} - 274,790,880 \text{ Btu}) \times \frac{1}{35,738} = 2,511 \text{ m}^3$$

USES AND EXCLUSIONS

To qualify for this measure, the under-fired broiler must use natural gas as its energy source and meet the following standards:

Table 5. Assumptions [2]

Broiler Size	Criteria
Three foot	<ul style="list-style-type: none"> Preheat energy less than 40,500 Btu Cooking energy rate less than 72,000 Btu/hr
Four foot	<ul style="list-style-type: none"> Preheat energy less than 54,000 Btu Cooking energy rate less than 96,000 Btu/hr
Five foot	<ul style="list-style-type: none"> Preheat energy less than 67,500 Btu Cooking energy rate less than 120,000 Btu/hr
Six foot	<ul style="list-style-type: none"> Preheat energy less than 81,000 Btu Cooking energy rate less than 144,000 Btu/hr

MEASURE LIFE

The measure life attributed to high efficiency under-fired broilers is 12 years. [2]

INCREMENTAL COST

Table 6 presents the measure incremental cost.

Table 6. Incremental Cost [4]

Measure Category	Incremental Cost (\$)
All categories of broilers	\$1,900

The incremental cost is very similar for the broilers regardless of their size. This is likely due to the burner technology being similar for high efficiency models. Cost variability between models is related to additional features.

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COMMERCIAL – INFRARED (IR) HEATERS < 300kBTU/HR – NEW CONSTRUCTION

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Infrared Heater → New Construction	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	New Construction (NC)	
Baseline Technology	Gas-Fired Unit Heater	
Efficient Technology	Infrared Heater (Single-Stage, Two-Stage and High Intensity)	
Market Type	Commercial	
Annual Natural Gas Savings Rate (m ³ /kBtu/hr)	Single-Stage and High Intensity	8.6 m ³ per kBtu/hr of IR heater input capacity
	Two Stage	9.8 m ³ per kBtu/hr of IR heater input capacity
Annual Electric Savings (kWh)	Infrared Input Rating (kBtu/hr)	Electric Savings (kWh)
	< 50	0 kWh
	50 – 165	225 kWh
	165 - 300	510 kWh
Measure Life	17 years	
Incremental Cost (\$ CAD)	\$11.22 per kBtu/hr of IR heater input capacity	
Restrictions	The installed equipment must be rated at less than 300 kBtu/hr	

OVERVIEW

Natural gas fired infrared (IR) heaters use radiant tube emitters or ceramic/steel emitters (high intensity) as the body by which to transmit infrared energy and heat. Gas is

burned to heat the emitter which radiates energy to the floor and other objects in the room.

IR heaters heat more efficiently than conventional forced air systems, such as unit heaters, for several reasons. First, they directly heat the objects in the space through infrared radiant energy, including the floor slab, which then radiate heat back into the air space. Because the people in the room are directly being heated, comfort levels can be achieved at a lower air temperature than with forced hot air systems.

Conventional systems heat the air flowing into the room but because heated air is less dense than the existing cool air, it rises to the ceiling and stratifies, gradually working its way down to the floor level. The floor slab and equipment act as heat sinks causing the ceiling level to be much warmer than the floor area. The result is that a forced hot air system needs to work harder than the infrared heater to heat the same space and IR heaters produce a more uniform space temperature by heating the floor and objects first.

Infrared heaters use smaller fans for the same rated capacity compared to a conventional system because conventional systems use fans to circulate the air through the space and infrared heaters use fans only to induce combustion draft.

Infrared heaters are significantly more efficient than conventional forced hot air systems because of differences in the way heat is distributed and additional losses associated with the forced hot air systems as discussed above. According to a study by Agviro, an infrared heater will have an output at full load of 85% its conventional counterpart for the same space heating capacity [1] [2]. This is often referred to as the compensation factor [3]. The 2012 ASHRAE handbook states that IR heaters produce savings of at least 15% [2] based on a study performed by Buckley and Seel in 1988 that found savings to typically be between 15% and 20% [4]. Although some manufacturers claim performance of IR heaters to be dependent on mounting height, ASHRAE has found IR heater savings to be independent of mounting height.

There are three primary types of infrared heaters, single stage, high intensity, and two-stage. The operation of all three types is essentially the same, but high intensity heaters utilize materials such as ceramics that can withstand higher operating temperatures, and two-stage heaters have controls to optimize performance at two levels of output. Because of their controls, two-stage heaters have better compensation factors than single stage or high intensity heaters.

APPLICATION

The measure covers the installation of infrared heaters in commercial settings. Infrared heaters are regulated by the CSA 2.35b standard, which requires that they convert at least 35% of the input fuel energy to radiant energy [5]. This is called the IR efficiency or the radiant efficiency and is not the same as thermal efficiency, which is a measure of the heating energy out over the fuel energy in. Thermal efficiency of an IR heater is higher than the radiant efficiency because the radiant efficiency does not include all heat

delivered to the space, but only includes the radiant component. As such, thermal efficiency is used as the performance metric for savings calculations.

BASELINE TECHNOLOGY

The baseline thermal efficiency for unit heaters is assumed to be 80%.

Table 2. Baseline Technology

Type	Efficiency
Conventional Unit Heater	80% Thermal Efficiency

EFFICIENT TECHNOLOGY

The efficient technology is an infrared heater.

Table 3. Efficient Technology¹ [1] [2] [4] [8]

Type	Compensation Factor	Thermal Efficiency
Infrared Heater Single Stage and High Intensity	0.85	82%
Infrared Heater Two Stages	0.83	82%

ENERGY IMPACTS

Natural gas savings are achieved through four mechanisms:

1. Objects are directly heated instead of the air around them.
2. Less air stratification for more uniform heating of the space.
3. Smaller fans and less stratification which reduces air infiltration changes.
4. Minor electricity savings because of the smaller fans in IR heaters compared to equally sized unit heaters or the blowers in forced hot air systems.

All of these factors are included in the compensation factor.

¹ Values used for engineering calculation purposes and not for eligibility criteria.

NATURAL GAS SAVINGS ALGORITHMS

The natural gas savings from installing an IR heater instead of a conventional unit heater can be calculated as a function of the compensation factor discussed in the measure overview and the thermal efficiencies assumed. This document is based on a compensation factor of 0.85 for single and high intensity and 0.83 for two-stage. The savings are directly proportional to the assumed effective full load hours of operation and the installed capacity of the equipment [3] [2] [4] [8].

The following is a derivation of the natural gas savings from installing an IR heater where,

NG Savings = Natural gas savings from installing an IR heater (kBtu)

NG Conv = Natural gas consumption of the conventional heater (kBtu)

NG IR = Natural gas consumption of the IR heater (kBtu)

EFLH = Equivalent full load hours (hrs)²

Input, Output_{Conv} = Input/output of the conventional heater (kBtu/hr)

Input, Output_{IR} = Input/output of the IR heater (kBtu/hr)

Comp = Compensation factor for the IR heater (%)

$$(1) \text{ } NG \text{ Savings} = NG \text{ Conv} - NG \text{ IR}$$

$$(2) \text{ } NG \text{ Conv} = Input_{Conv} \times EFLH$$

$$(3) \text{ } NG \text{ IR} = Input_{IR} \times ELFH$$

Substituting equations (2) and (3) into equation (1) results in:

$$(4) \text{ } NG \text{ Savings} = Input_{Conv} \times EFLH - Input_{IR} \times ELFH$$

The natural gas inputs to the IR heater can be defines as:

$$(5) \text{ } Input_{Conv} = \frac{Output_{Conv}}{\eta_{conv}}$$

$$(6) \text{ } Input_{IR} = \frac{Output_{IR}}{\eta_{IR}}$$

The IR heater output is shown by the following relationship:

$$(7) \text{ } Output_{IR} = Output_{Conv} \times Comp$$

Substituting equation (7) into equation (6):

$$(8) \text{ } Input_{IR} = \frac{Output_{Conv} \times Comp}{\eta_{IR}}$$

² Note, that the EFLH is assumed to be equal for both conventional and the IR heaters.

Then, substituting equations (8) and (5) into equation (4) yields:

$$(9) \text{ NG Savings} = \frac{\text{Output}_{\text{Conv}}}{\eta_{\text{conv}}} \times \text{EFLH} - \frac{\text{Output}_{\text{Conv}} \times \text{Comp}}{\eta_{\text{IR}}} \times \text{EFLH}$$

Simplifying the relationships:

$$(10) \text{ NG Savings} = \text{Output}_{\text{Conv}} \times \text{EFLH} \times \left(\frac{1}{\eta_{\text{conv}}} - \frac{\text{Comp}}{\eta_{\text{IR}}} \right)$$

Multiplying through by $\frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}}$ results in:

$$(11) \text{ NG Savings} = \text{Output}_{\text{Conv}} \times \text{EFLH} \times \left(\frac{1}{\eta_{\text{conv}}} \times \frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}} - \frac{\text{Comp}}{\eta_{\text{IR}}} \times \frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}} \right)$$

When this relationship is simplified, the equation results in:

$$(12) \text{ NG Savings} = \frac{\text{Output}_{\text{Conv}} \times \text{Comp}}{\eta_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{conv}} \times \text{Comp}} - 1 \right)$$

Substituting equation (7) into equation (12) to replace the conventional system output equals:

$$(13) \text{ NG Savings} = \frac{\text{Output}_{\text{IR}}}{\eta_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{conv}} \times \text{Comp}} - 1 \right)$$

Substituting equation (6) into equation (13) into the $\text{Output}_{\text{IR}}$ term results in:

$$(14) \text{ NG Savings} = \text{Input}_{\text{IR}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{conv}} \times \text{Comp}} - 1 \right)$$

Both sides of equation 14 are divided by the infrared heater input to get the natural gas savings factor, which is the annual natural gas energy savings rate, in m^3 natural gas savings per kBtu/hr input capacity of the IR heater:

$$\text{NG Savings Factor} = \frac{\text{NG Savings}}{\text{Input}_{\text{IR}}} = \frac{\text{Input}_{\text{IR}}}{\text{Input}_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{conv}} \times \text{Comp}} - 1 \right)$$

Finally, the savings factor is divided by the heat content of natural gas to convert to savings on a volumetric basis:

$$\text{NG Savings Factor} = \frac{\text{EFLH}}{35.738 \frac{\text{kBtu}}{\text{m}^3}} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}_{\text{ss,ts}}} - 1 \right)$$

where,

NG Savings Factor = Annual gas savings rate resulting from installing the new IR heater ($\text{m}^3/\text{yr}/(\text{kBtu}/\text{hr})$)

EFLH = Equivalent full load hours of operation, Table 4

$35.738 \frac{\text{kBtu}}{\text{m}^3}$ = Conversion from kBtu/hr to m^3/hr , common assumptions table

- $Comp_{ss,ts}$ = Compensation factor for the IR heaters, where *ss* designates single stage or high intensity heaters, and *ts* indicates two-stage heaters (%), Table 4
- η_{Conv} = Thermal efficiency of the conventional heater (%), Table 2
- η_{IR} = Thermal efficiency of the infrared heater (%), Table 3

ELECTRIC SAVINGS ALGORITHMS

The estimated electricity savings are grouped into three bins corresponding to heater capacity ranges. The savings are calculated using assumed fan power values that were estimated from values provided by several major manufacturers. Multiplying the fan power times the equivalent full load hours of operation calculates approximate annual electricity consumption.

$$\text{Annual kWh Savings} = EFLH \times (kW_{Conv} - kW_{IR})$$

Where,

- Annual kWh Savings* = Annual electrical savings from installing the new IR heater (kWh)
- kW_{Conv} = Conventional heater fan horsepower converted to kW, Table 4
- EFLH* = Effective full load hours of operation, Table 4
- kW_{IR} = IR heater fan horsepower converted to kW, Table 4

ASSUMPTIONS

The IR system type is presumed to be direct-fired with combustion products vented to the outside. Table 4 shows the list of assumptions utilized in the measure savings algorithms.

Table 4. Assumptions

Variable	Definition	Value		Source
$Comp_{ss,ts}$	Compensation factors	$Comp_{ss}$	0.85	[2] [4] [8]
		$Comp_{ts}$	0.83	
<i>EFLH</i>	Effective full load hours (New Construction)	1,500 hours		Common Assumptions Table
kW_{Conv}	Conventional fan	< 50 kBtu/hr	0.02 kW	[9]

Variable	Definition	Value		Source
	kW draw	50 – 1650 kBtu/hr	0.19 kW	
		> 165 kBtu/hr	0.43 kW	
kW_{IR}	IR heater fan kW draw	< 50 kBtu/hr	0.02 kW	[9]
		50 – 165 kBtu/hr	0.04 kW	
		> 165 kBtu/hr	0.09 kW	

SAVINGS CALCULATION EXAMPLE

The following example shows how energy savings are calculated for a 100 kBtu/hr input single stage IR heater to be installed at 30 ft from floor in a new building starting with the calculation of the savings factor in Table 1.

$$NG\ Savings = \frac{1,500\ hours}{35.738\ \frac{kBtu}{m^3}} \times \left(\frac{82\%}{80\% \times 85\%} - 1 \right) = 8.64\ \frac{m^3}{hr}$$

The annual natural gas savings can be calculated as:

$$NG\ Savings = 8.64\ \frac{m^3}{kBtu} \times 100\ \frac{kBtu}{hr} = 864\ m^3$$

The annual electrical savings can be calculated as:

$$Annual\ kWh\ Savings = 1,500\ hrs \times (0.19\ kW - 0.04\ kW) = 225\ kWh$$

USES AND EXCLUSIONS

To qualify for this measure the infrared heaters must be of a rated capacity less than 300 kBtu/hr.

MEASURE LIFE

The measure life attributed to this measure is 17 years [10].

INCREMENTAL COST

The incremental cost is \$11.22 per kBtu/hr IR input capacity. [11].³

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³ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

COMMERCIAL – INFRARED (IR) HEATERS <300KBTU/HR – RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Infrared Heater → Retrofit	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	Retrofit (R)	
Baseline Technology	Gas-Fired Unit Heater	
Efficient Technology	Infrared Heater (Single-Stage, Two-Stage and High Intensity)	
Market Type	Commercial	
Annual Natural Gas Savings Rate (m ³ /kBtu/hr)	Single-Stage and High Intensity	11.5 m ³ per kBtu/hr of IR heater input capacity
	Two-Stage	13.1 m ³ per kBtu/hr of IR heater input capacity
Annual Electric Savings (kWh)	Infrared Input Rating (kBtu/hr)	Electric Savings (kWh)
	< 50	0 kWh
	50 – 165	300 kWh
	165 - 300	1,040 kWh
Measure Life	17 years	
Incremental Cost (\$ CAD)	\$30.28 per kBtu/hr of IR heater input capacity	
Restrictions	The installed equipment must be rated at less than 300 kBtu/hr	

OVERVIEW

Natural gas fired infrared (IR) heaters use radiant tube emitters or ceramic/steel emitters (high intensity) as the body by which to transmit infrared energy and heat. Gas is burned to heat the emitter which radiates energy to the floor and other objects in the room.

IR heaters heat more efficiently than conventional forced air systems, such as unit heaters, for several reasons. First, they directly heat the objects in the space through infrared radiant energy, including the floor slab, which then radiate heat back into the air space. Because the people in the room are directly being heated, comfort levels can be achieved at a lower air temperature than with forced hot air systems.

Conventional systems heat the air flowing into the room but because heated air is less dense than the existing cool air, it rises to the ceiling and stratifies, gradually working its way down to the floor level. The floor slab and equipment act as heat sinks causing the ceiling level to be much warmer than the floor area. The result is that a forced hot air system needs to work harder than the infrared heater to heat the same space and IR heaters produce a more uniform space temperature by heating the floor and objects first.

Infrared heaters use smaller fans for the same rated capacity compared to a conventional system because conventional systems use fans to circulate the air through the space and infrared heaters use fans only to induce combustion draft.

Infrared heaters are significantly more efficient than conventional forced hot air systems because of differences in the way heat is distributed and additional losses associated with the forced hot air systems as discussed above. According to a study by Agviro, an infrared heater will have an input at full load of 85% its conventional counterpart for the same space heating capacity [1]. This is often referred to as the compensation factor [2]. The 2012 ASHRAE handbook states that IR heaters produce savings of at least 15% [3] based on a study performed by Buckley and Seel in 1988 that found savings to typically be between 15% and 20% [4]. Although some manufacturers claim performance of IR heaters to be dependent on mounting height, ASHRAE has found IR heater savings to be independent of mounting height.

There are three primary types of infrared heaters, single stage, high intensity, and two-stage. The operation of all three types is essentially the same, but high intensity heaters utilize materials such as ceramics that can withstand higher operating temperatures, and two-stage heaters have controls to optimize performance at two levels of output. Because of their controls, two stage heaters have better compensation factors than single stage or high intensity heaters.

APPLICATION

The measure covers the installation of infrared heaters in commercial settings. Infrared heaters are regulated by the CSA 2.35b standard, which requires that they convert at least 35% of the input fuel energy to radiant energy [5]. This is called the IR efficiency or the radiant efficiency and is not the same as thermal efficiency, which is a measure of the heating energy out over the fuel energy in. Thermal efficiency of an IR heater is higher than the radiant efficiency because the radiant efficiency does not include all heat delivered to the space, but only includes the radiant component. As such, thermal efficiency is used as the performance metric for savings calculations.

BASELINE TECHNOLOGY

The baseline thermal efficiency for unit heaters is assumed to be 80.

Table 2. Baseline Technology

Type	Efficiency
Conventional Unit Heater	80% Thermal Efficiency

EFFICIENT TECHNOLOGY

The efficient technology is an infrared heater.

Table 3. Efficient Technology¹ [1] [3] [4] [8]

Type	Compensation Factor	Thermal Efficiency
Infrared Heater Single-Stage and High Intensity	0.85	82%
Infrared Heater Two-Stages	0.83	82%

ENERGY IMPACTS

Natural gas savings are achieved through four mechanisms:

1. Objects are directly heated instead of the air around them.
2. Less air stratification for more uniform heating of the space.
3. Smaller fans and less stratification which reduces air infiltration changes.
4. Minor electricity savings because of the smaller fans in IR heaters compared to equally sized unit heaters or the blowers in forced hot air systems.

All of these factors are included in the compensation factor.

NATURAL GAS SAVINGS ALGORITHMS

The natural gas savings from installing an IR heater instead of a conventional unit heater can be calculated as a function of the compensation factor discussed in the measure overview and the thermal efficiencies assumed. This document is based on a

¹ Values used for engineering calculation purposes and not for eligibility criteria.

compensation factor of 0.85 for single and high intensity and 0.83 for two-stage. The savings are directly proportional to the assumed effective full load hours of operation and the installed capacity of the equipment [2] [3] [4] [8].

The following is a derivation of the natural gas savings from installing an IR heater where,

NG Savings = Natural gas savings from installing an IR heater (kBtu)

NG Conv = Natural gas consumption of the conventional heater (kBtu)

NG IR = Natural gas consumption of the IR heater (kBtu)

EFLH = Equivalent full load hours (hrs)²

Input, Output_{Conv} = Input/output of the conventional heater (kBtu/hr)

Input, Output_{IR} = Input/output of the IR heater (kBtu/hr)

Comp = Compensation factor for the IR heater (%)

$$(1) \text{NG Savings} = \text{NG Conv} - \text{NG IR}$$

$$(2) \text{NG Conv} = \text{Input}_{\text{Conv}} \times \text{EFLH}$$

$$(3) \text{NG IR} = \text{Input}_{\text{IR}} \times \text{ELFH}$$

Substituting equations (2) and (3) into equation (1) results in:

$$(4) \text{NG Savings} = \text{Input}_{\text{Conv}} \times \text{EFLH} - \text{Input}_{\text{IR}} \times \text{ELFH}$$

The natural gas inputs to the IR heater can be defines as:

$$(5) \text{Input}_{\text{Conv}} = \frac{\text{Output}_{\text{Conv}}}{\eta_{\text{Conv}}}$$

$$(6) \text{Input}_{\text{IR}} = \frac{\text{Output}_{\text{IR}}}{\eta_{\text{IR}}}$$

The IR heater output is shown by the following relationship:

$$(7) \text{Output}_{\text{IR}} = \text{Output}_{\text{Conv}} \times \text{Comp}$$

Substituting equation (7) into equation (6):

$$(8) \text{Input}_{\text{IR}} = \frac{\text{Output}_{\text{Conv}} \times \text{Comp}}{\eta_{\text{IR}}}$$

Then, substituting equations (8) and (5) into equation (4) yields:

$$(9) \text{NG Savings} = \frac{\text{Output}_{\text{Conv}}}{\eta_{\text{Conv}}} \times \text{EFLH} - \frac{\text{Output}_{\text{Conv}} \times \text{Comp}}{\eta_{\text{IR}}} \times \text{ELFH}$$

Simplifying the relationships:

² Note, that the EFLH is assumed to be equal for both conventional and the IR heaters.

$$(10) \text{ NG Savings} = \text{Output}_{\text{Conv}} \times \text{EFLH} \times \left(\frac{1}{\eta_{\text{Conv}}} - \frac{\text{Comp}}{\eta_{\text{IR}}} \right)$$

Multiplying through by $\frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}}$ results in:

$$(11) \text{ NG Savings} = \text{Output}_{\text{Conv}} \times \text{EFLH} \times \left(\frac{1}{\eta_{\text{Conv}}} \times \frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}} - \frac{\text{Comp}}{\eta_{\text{IR}}} \times \frac{\eta_{\text{IR}}}{\eta_{\text{IR}}} \times \frac{\text{Comp}}{\text{Comp}} \right)$$

When this relationship is simplified, the equation results in:

$$(12) \text{ NG Savings} = \frac{\text{Output}_{\text{Conv}} \times \text{Comp}}{\eta_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}} - 1 \right)$$

Substituting equation (7) into equation (12) to replace the conventional system output equals:

$$(13) \text{ NG Savings} = \frac{\text{Output}_{\text{IR}}}{\eta_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}} - 1 \right)$$

Substituting equation (6) into equation (13) into the $\text{Output}_{\text{IR}}$ term results in:

$$(14) \text{ NG Savings} = \text{Input}_{\text{IR}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}} - 1 \right)$$

Both sides of equation 14 are divided by the infrared heater input to get the natural gas savings factor, which is the annual natural gas energy savings rate, in m³ natural gas savings per kBtu/hr input capacity of the IR heater:

$$\text{NG Savings Factor} = \frac{\text{NG Savings}}{\text{Input}_{\text{IR}}} = \frac{\text{Input}_{\text{IR}}}{\text{Input}_{\text{IR}}} \times \text{EFLH} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}} - 1 \right)$$

Finally, the savings factor is divided by the heat content of natural gas to convert to savings on a volumetric basis:

$$\text{NG Savings Factor} = \frac{\text{EFLH}}{35.738 \frac{\text{kBtu}}{\text{m}^3}} \times \left(\frac{\eta_{\text{IR}}}{\eta_{\text{Conv}} \times \text{Comp}_{\text{ss,ts}}} - 1 \right)$$

where,

- NG Savings = Annual gas savings rate resulting from installing the new IR heater (m³/yr/(kBtu/hr))
- EFLH = Equivalent full load hours of operation, Table 4
- $35.738 \frac{\text{kBtu}}{\text{m}^3}$ = Conversion from kBtu/hr to m³/hr, common assumptions table
- $\text{Comp}_{\text{ss,ts}}$ = Compensation factor for the IR heaters, where *ss* designates single stage or high intensity heaters, and *ts* indicates two-stage heaters (%), Table 4
- η_{Conv} = Thermal efficiency of the conventional heater (%), Table 2
- η_{IR} = Thermal efficiency of the infrared heater (%), Table 3

ELECTRIC SAVINGS ALGORITHMS

The estimated electricity savings are grouped into three bins corresponding to heater capacity ranges. The savings are calculated using assumed fan power values that were estimated from values provided by several major manufacturers. Multiplying the fan power times the effective full load hours of operation calculates approximate annual electricity consumption.

$$\text{Annual kWh Savings} = \text{EFLH} \times (\text{kW}_{\text{Conv}} - \text{kW}_{\text{IR}})$$

Where,

Annual kWh Savings = Annual electrical savings from installing the new IR heater (kWh)

kW_{Conv} = Conventional heater fan horsepower converted to kW, Table 4

EFLH = Effective full load hours of operation, Table 4

kW_{IR} = IR heater fan horsepower converted to kW, Table 4

ASSUMPTIONS

The IR system type is presumed to be direct-fired with combustion products vented to the outside. Table 4 shows the list of assumptions utilized in the measure savings algorithms.

Table 4. Assumptions

Variable	Definition	Value		Source
$Comp_{ss,ds}$	Compensation factors	$Comp_{ss}$	0.85	[3] [4] [8]
		$Comp_{ts}$	0.83	
<i>EFLH</i>	Effective full load hours (Retrofit)	2,000 hours		Common Assumptions Table
kW_{Conv}	Conventional fan kW draw	< 50 kBtu/hr	0.02 kW	[9]
		50 – 165 kBtu/hr	0.19 kW	
		> 165 kBtu/hr	0.43 kW	
kW_{IR}	IR heater fan kW draw	< 50 kBtu/hr	0.02 kW	[9]
		50 – 165 kBtu/hr	0.04 kW	
		> 165 kBtu/hr	0.09 kW	

SAVINGS CALCULATION EXAMPLE

The following example shows how energy savings are calculated for a 100 kBtu/hr input single stage IR heater to be installed at 30 ft from floor in an existing warehouse starting with the calculation of the savings factor in Table 1.

$$NG\ Savings = \frac{2,000\ hours}{35.738\ \frac{kBtu}{m^3}} \times \left(\frac{82\%}{80\% \times 85\%} - 1 \right) = 11.52\ \frac{m^3}{hr}$$

The annual natural gas savings can be calculated as:

$$NG\ Savings = 11.52\ \frac{m^3}{hr} \times 100\ \frac{kBtu}{hr} = 1,152\ m^3$$

The annual electrical savings can be calculated as:

$$Annual\ kWh\ Savings = 2,000\ hrs \times (0.19\ kW - 0.04\ kW) = 300\ kWh$$

USES AND EXCLUSIONS

To qualify for this measure the infrared heaters must be of a rated capacity less than 300 kBtu/hour.

MEASURE LIFE

The measure life attributed to this measure is 17 years [10].

INCREMENTAL COST

The incremental cost is \$30.28 CAD per kBtu/hr IR input capacity.³ [11].

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MULTI-RESIDENTIAL – LOW-FLOW SHOWERHEADS – NEW CONSTRUCTION/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Multi-residential/Low-Income → Water Heating → Low-flow showerheads → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters and savings values based on the efficient technology.

Table 1. Measure Key Data

Parameter	Definitions	
Measure category	New Construction (NC) Retrofit (R)	
Baseline technology	2.5 gpm	
Efficient technology	1.5 gpm	
	1.25 gpm	
Market type	Multi-residential	
Annual natural gas savings per showerhead (m ³)	Efficient Technology	Savings
	1.25 gpm	38.2 m ³
	1.5 gpm	30.6 m ³
Annual water savings per showerhead (liters)	1.25 gpm	12,105 L
	1.5 gpm	8,322 L
Measure life	10 years	
Incremental cost	Utility to use actual per showerhead cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.	
Restrictions	This document is applicable to low-flow showerheads that have been installed by way of direct installation in multi-residential households where sampling confirms the base case is equal to or less efficient than 2.5 gpm.	

OVERVIEW

In multi-residential households, one of the ways to reduce domestic hot water heating costs is by reducing the amount of hot water use. Installing low-flow showerheads can have a noticeable impact on a building's hot water consumption. The savings that can be achieved are attractive since this measure is relatively inexpensive and easy to implement.

Low-flow showerheads restrict the flow of the water while maintaining water pressure.

APPLICATION

This measure pertains to the implementation of low-flow showerheads in multi-residential households.

BASELINE TECHNOLOGY

The baseline technology is a showerhead with a flow of 2.5 gpm. [1]

EFFICIENT TECHNOLOGY

The efficient technology is a low-flow showerhead with a flow rate of 1.5 gpm or lower.

ENERGY IMPACTS

The primary energy impact associated with implementation of low-flow showerheads is a reduction in natural gas resulting from a reduction in the hot water consumption. There is an additional reduction in water consumption associated with this measure.

NATURAL GAS SAVINGS ALGORITHM

This algorithm outlines a methodology to determine the energy consumption as a function of a showerhead's rated flow-rate. It is based on the methodology developed by Navigant Consulting using data from a SAS statistical billing analysis study with the specific purpose of determining the impact of low-flow showerheads for single family homes in Ontario.

The SAS study [2] analyzed the gas consumption in Enbridge territory over the course of two years for 178 single family households which included a control group, a low-flow group, and a treatment group which had high-flow showerheads in the first year of the study. After a year into the study, showerheads in the treatment group were replaced with low-flow fixtures of 1.25 gpm.

The study resulted in two groups of savings: homes with showerheads that had pre-existing showerheads with full-on flow rates, or nominal/rated flow rates, between 2.0 gpm to 2.5 gpm and homes with showerheads with full-on flow rates greater than 2.5 gpm.

The full-on flow rate groups in the SAS sample and their associated savings levels per household are shown in Table 2:

Table 2. Savings from SAS Study [2] [3]

Rated Flow Rate	Average of Rated Flow Rates (gpm) ¹	Nominal Rated Flow of Low-flow Showerhead (gpm)	Nominal Flow Reduction (gpm)	Annual Savings (m ³) ²	Annual Savings Per Nominal gpm Flow Reduction (m ³ /gpm)
2.0 to 2.5 gpm	2.40	1.25	1.15	46.4	40.3
>2.5 gpm	3.09	1.25	1.84	87.8	47.7

The average reduction in annual natural gas use in each household was 44.0 m³ per gpm reduction in rated showerhead flow rate. Using this relationship, the gas savings can be calculated for any combination of baseline and high efficiency showerheads, if rated flow rate is known. The average number of showers was 2.06 per household. Using this factor, we can adjust the saving to a per showerhead basis.

$$\frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) = \frac{44 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})}{2.06 \frac{\text{showerheads}}{\text{household}}}$$

This results in a savings calculation of:

$$\frac{\text{Annual energy savings}}{\text{showerhead}} \left(\frac{\text{m}^3}{\text{yr}} \right) = 21.4 \frac{\text{m}^3}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

Based on data from Enbridge Gas (for the 2015 program year)³, there are 1.02 showerheads per multifamily residence. Furthermore, for multi-residential homes, Navigant Consulting proposed an adjusted savings based on number of occupants per household to reflect differences in patterns of use and have conservatively assumed that, on average, the seasonal efficiency of the gas devices are similar. [4] The average number of people per single home in the referenced study in the treatment group, or where low-flow showerheads were installed, was 2.75 people per household. The average number of people in a multi-residential residence (weighted by type: buildings over 5 stories and (2) for buildings of five stories or less (1.9)) is 1.96 people.

The showering behaviors of the residents in single family homes as compared to multifamily home should be similar, if not equal. Rather, the proportion of people per showerhead will be the driving factor in the savings.

¹ The average flow rate used here is from actual bag tested flow rate data provided by Enbridge Gas for the corresponding year of the SAS study (2007). [4]

² The savings presented here are from a SAS study, which analyzed consumption of households over two years, beginning in 2007. [3]

³ According to Enbridge Gas data for the program year of 2015, as of November 12, 2015, there had been 7,280 showerheads replaced in 7,127 apartments, totaling about 1.02 showers per suite.

$$\text{Multifamily Savings} \times \frac{\text{MF People}}{\text{SF Showers}} = \text{Single family savings} \times \frac{\text{SF People}}{\text{SF Showers}}$$

Based on these factors, the adjustment can be made as follows:

$$\text{Multifamily Savings} = \text{Single family savings} \times \frac{\text{SF People}}{\text{SF Showers}} \times \frac{\text{SF Showers}}{\text{MF People}}$$

We know the savings per showerhead for single family homes as determined above, thus the relationship reduces to:

$$\text{Multifamily Savings} = 21.4 \frac{\text{m}^3}{\text{yr}} \times (\text{baseline rated gpm} - \text{high efficiency gpm}) \times \text{SF People} \times \frac{\text{SF Showers}}{\text{MF People}}$$

Applying all the factors above: the resulting savings per showerhead for multi-residential is:

$$\begin{aligned} \text{Multifamily Savings} &= 21.4 \frac{\text{m}^3}{\text{yr}} \times (\text{baseline rated gpm} - \text{high efficiency gpm}) \times 2.75 \text{ people} \\ &\times \frac{1.02 \text{ Showers}}{1.96 \text{ People}} \end{aligned}$$

Resulting in:

$$\text{Multifamily Savings} = 30.62 \times (\text{baseline rated gpm} - \text{high efficiency gpm})$$

WATER SAVINGS ALGORITHM

The SAS study only presented natural gas savings for the region but did not report water savings. Another algorithm was used to determine the water savings:

$$\text{Savings} = \frac{\text{Ppl} \times \text{Sh} \times 365 \frac{\text{days}}{\text{year}} \times T \times (\text{Fl}_{\text{base}} - \text{Fl}_{\text{eff}}) \times 3.785 \frac{\text{L}}{\text{gal}}}{\text{Number of Showerheads}}$$

Where,

<i>Savings</i>	= Annual savings in liters
<i>Ppl</i>	= Number of people per household
<i>Sh</i>	= Showers per capita per day
365	= Days per year
<i>T</i>	= Showering time (minutes)
<i>Fl_{base}</i>	= As-used flow rate with base equipment (gpm) – Calculated from equation from Summit Blue Study

Fl_{eff} = As-used flow rate with efficient equipment (gpm) –
 Calculated from equation from Summit Blue Study

Number of Showerheads = Number of showerheads

Fl_{base} and Fl_{eff} are the “as-used” flow rate. The nominal flow-rate is the flow the showerhead will deliver at full flow at 80 psi. However, based on Enbridge flow rate bag test data, the flow for installed fixtures varies from the rated flow rate of the showerhead. [3] [5] [6].

The following regression based on a study in 443 California homes of+ weighted regression analysis of as-used flow compared to full-on flow rate:

$$As - Used Flow Rate^4 = 0.542 \times Nominal Flow Rate + 0.691 \text{ [5]}$$

Where,

As – Used Flow Rate = Actual flow of installed showerhead

Nominal Flow Rate = Rated flow listed on the showerhead

ASSUMPTIONS

Table 3, provides assumptions used in the natural gas calculation.

Table 3. Constants and Assumptions for Natural Gas Savings Calculation

Assumption	Value	Source
Average persons per multi family residence (2006)	1.96	Common assumptions table
Average number of showerheads per multi-family residence	1.02	Enbridge Gas data
Average number of people per single family residence in SAS study treatment group	2.75	[2]
Average number of showers per single family residence in SAS study treatment group	2.06	[2]

Table 4 provides a list of constants and assumption used in the derivation of the water savings values.

Table 4. Constants and Assumptions for Water Savings Calculation

Assumption	Value	Source
Average persons per multi family residence (2006)	1.96	Common assumptions table
Number of showerheads per residence	1.02	Enbridge Gas data

⁴ The lower limit of this equation is 1.25 gpm due to water pressure limitations. As the showerhead flow rate is reduced, the full-on flow will approach the as-used flow since as there is a limit to the acceptable flow-rate. [5] As such, the algorithm assumes that a showerhead with a full-on flow rate of 1.25 gpm also has an as-used flow of 1.25 gpm. Actual flow rates lower than 1.25 gpm can be assumed to result in longer showers, negating additional savings.

Assumption	Value	Source
Showers per capita per day	0.75	[5]
Average showering time per day per showerhead (minutes)	7.6 minutes	[5]

SAVINGS CALCULATION EXAMPLE

The scenario for the gas savings is as follows. A showerhead will be replaced with a 1.5 gpm showerhead for a multi-residential residence.

Natural Gas Savings

Using the equation above for the replacement of a baseline 2.5 gpm showerhead with a 1.5 gpm showerhead,

$$\begin{aligned}
 \text{Annual energy savings (m}^3/\text{yr)} & \\
 &= 30.62 \frac{\text{m}^3/\text{yr}}{\text{gpm}} \times (\text{baseline rated gpm} - \text{high efficiency gpm}) \\
 \text{Annual energy savings (m}^3/\text{yr)} &= 30.62 \times (2.5 - 1.5) \\
 \text{Annual energy savings} &= 30.6 \frac{\text{m}^3}{\text{yr}}
 \end{aligned}$$

Water Savings

$$\begin{aligned}
 \text{Savings} &= 1.96 \frac{\text{people}}{\text{residence}} \times 0.75 \frac{\text{showers}}{\text{person day}} \times 7.6 \frac{\text{mins}}{\text{shower}} \times 365 \frac{\text{days}}{\text{year}} \\
 &\times \left(2.05 \frac{\text{gallons}}{\text{min}} - 1.5 \frac{\text{gallons}}{\text{min}} \right) \times 3.785 \frac{\text{liters}}{\text{gal}} \div 1.02 \text{showerheads} \\
 &= 8,322 \frac{\text{liters}}{\text{year}}
 \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure, low-flow showerheads must be installed in multi-residential households where sampling confirms the base case is equal to or less efficient than 2.5 gpm.

MEASURE LIFE

The measure life attributed to this measure is 10 years. [5]

INCREMENTAL COST

The incremental cost for this measure could not be determined by looking at big-box retailer data. The driver for higher cost of fixtures is the available features of the showerheads. However, the previous substantiation sheet based the incremental cost on bulk purchases by the utility for program implementation. Since the incremental cost of the measure in the previous substantiation sheet is based on actual cost to the utility, it is the most accurate data. This method is consistent with other TRMs. Table 5 presents the measure incremental cost.

Table 5. Measure Incremental Cost

Measure Category	Incremental Cost (\$)
All measure categories	Utility to use actual per showerhead cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.

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COMMERCIAL — OZONE LAUNDRY TREATMENT — NEW CONSTRUCTION/ RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Water Heating → Ozone Laundry Treatment → New Construction/Retrofit	

Table 1 provides a summary of the key measure parameters with savings coefficients.

Table 1. Measure Key Data

Parameter	Definitions			
Measure Category	New Construction (NC) Retrofit (R)			
Baseline Technology	Commercial laundry with no ozone treatment system			
Efficient Technology	Ozone treatment system for commercial laundry			
Market Type	Commercial, Multi-residential ¹			
Annual Natural Gas Savings Rate (m ³ /(lb-yr))	Washer Type	Natural Gas Savings Factor - NGSF (m³/(lb-yr))	Electric Savings - ESF (kWh/(lb-yr))	Water Savings - WSF (L/(lb-yr))
Annual Electric Savings Rate (kWh/(lb-yr))	Extractor Washers	0.0383	0.00213	2.08
Annual Water Savings - Rate (L/(lb-yr))	Tunnel Washers	0.0305	0.00150	1.27
Measure Life	15 years [1]			
Incremental Cost (\$ CAD)	Washer Type			Incremental Cost
	Washer extractor – ≤ 60 lbs			\$15,714
	Washer extractor – > 60 lbs and < 500 lbs			\$35,714
	Washer extractor – ≥ 500 lbs			\$44,286
	Tunnel washer – ≤ 120 lbs			\$71,429
	Tunnel washer – > 120 lbs and < 500 lbs			\$150,000
	Tunnel washer – ≥500 lbs			\$228,571
Restrictions	This measure is restricted to commercial clothes washers using water heated by natural gas. Washers dedicated to cleaning heavily soiled laundry are not eligible for this measure.			

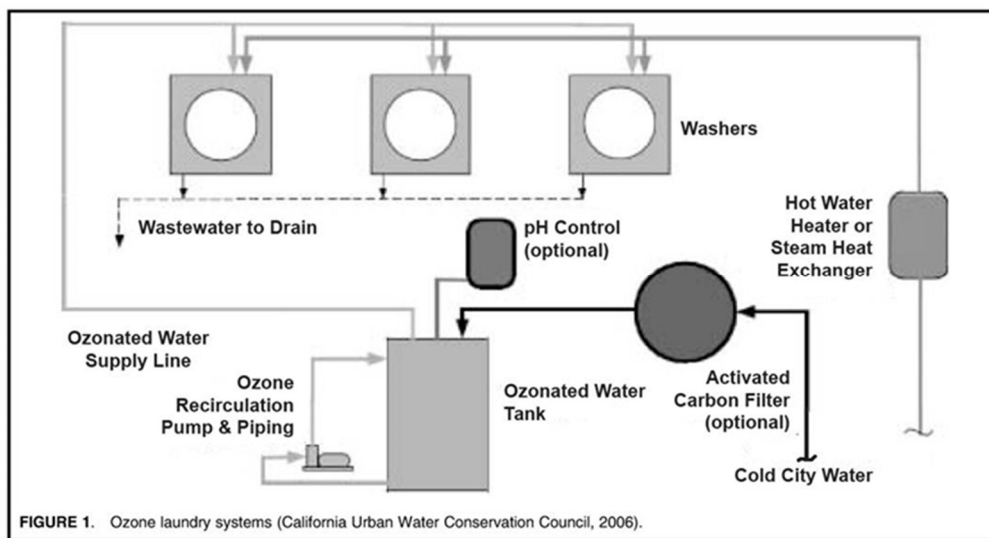
¹ Multi-residential building must have commercial extraction or tunnel washers.

OVERVIEW

In the commercial laundry industry, ozone is generated via a corona discharge or an ultraviolet light. The ozone dissolves in water temperatures ranging from cold to ambient, and activates the detergents, improving their activity and leading to stronger cleaning capabilities. The improved cleaning action results in hot water savings, and as a result, natural gas savings. However, since the solubility of ozone is low and its decomposition is faster at higher temperatures (38°C/100°F), the use of ozone is not recommended for heavily soiled laundry, which requires hotter water.

An important consideration with the use of ozone systems is laundry worker safety. Ozone exposure is regulated worldwide. The exposure limits for workers in Canadian facilities is limited to 0.12 parts per million over a time-weighted average of a one-hour period. The installation of an ozone system usually includes the installation of an ozone sensor to ensure that unsafe levels are not reached [2]. Figure 1 shows the schematics of a laundry system equipped with an ozone treatment system.

Figure 1. Washer Extractors – Example Schematic



APPLICATION

This measure is for installing an ozone system on a commercial clothes washer. There is no distinction between the retrofit and new construction project types for this measure, as the applicable assumptions are the same.

BASELINE TECHNOLOGY

The baseline for this measure is standard commercial laundry equipment that does not utilize ozone laundry treatment and uses natural gas for water heating.

EFFICIENT TECHNOLOGY

The efficient case for this measure is ozone laundry treatment equipment installed on commercial laundry equipment using natural gas for water heating.

ENERGY IMPACTS

The primary savings produced by installing an ozone treatment system are hot water savings from reduced cycles and more efficient cleaning. Natural gas is saved from the reduced hot water demand, in addition to water savings. Although the ozone system consumes additional electricity, electric savings are also realized due to the reduced cycles required per load.

NATURAL GAS SAVINGS ALGORITHMS

The savings for this measure are determined utilizing a savings calculator developed by NGTC (Natural Gas Technology Center). The factors are determined by calculating the water saved from installing an ozone generating system on a washer.

The following algorithm is used to calculate the actual gas impact in cubic meters from the natural gas savings factor.

$$\Delta(m^3) = NGSF \times WC \times Load$$

Where,

NGSF	= Natural gas savings factor; see Table 1 (m ³ /(lbs/yr ²))
WC	= Washer capacity; see application (lbs/load)
Load	= Annual loads processed by the washer; see application (loads/yr)

ELECTRIC SAVINGS ALGORITHMS

The following algorithm is used to calculate the electric impact in kilowatt-hours from the electric energy savings factor.

$$\Delta(kWh) = ESF \times WC \times Load$$

Where,

ESF	= Electric savings factor,(kWh/(lbs/yr ²))
-----	--

- WC = Washer capacity; see application (lbs/load)
 Load = Annual loads processed by the washer; see application (loads/yr)

WATER SAVINGS ALGORITHMS

The following algorithm is used to calculate the water impact from the water savings factor.

$$\Delta(L) = WSF \times WC \times Load$$

Where,

- WSF = Water savings factor; see Table 1 (L/(lbs/yr²))
 WC = Washer capacity; see application (lbs/load)
 Load = Annual loads processed by the washer; see application (loads/yr)

ASSUMPTIONS

Table 2 shows the list of assumptions utilized in the calculations spreadsheet to derive the savings factors in Table 1. Ozone laundry systems cannot use high temperature water since ozone breaks down above 35°C [3]. It is also notable that there is broad range of water recycling capability from commercial machines depending on the rigor of the recycling purification methods. Using simple filtration, 10% to 35% of water can be recycled. By incorporating multiple filtration steps and advanced disinfecting techniques, such as ultraviolet light, up to 90% water savings can be achieved. [4]. For this analysis, operating conditions used to calculate the energy consumption per pound of laundry were evaluated using input data from representatives of an ozone laundry products manufacturer and a large linen services company. These operating conditions are assumed to be typical for industrial laundry facilities.

Table 2. Assumptions

Variable	Value	Sources
Average city or inlet water temperature	48.9 F (9.39 C)	Common assumptions table
Commercial water heating efficiency	83%	Common assumptions table
Ratio of water recycled	30.0% ²	[4]
Water temperature for medium soil (ozone)	20.0°C	[1] [3]

² To provide a conservative estimate of gas savings, 30% water recycling was selected within the 10% - 35% range. This range is noted in [4], which for the range in turn cites "Slash Utility Consumption." Laundry Today July/August 2005, p.12.

SAVINGS CALCULATION EXAMPLE

The natural gas savings for a 120 pound per load tunnel washer where the estimated annual loads are estimated to be 30 loads per hour for 8 hours a day for 350 days a year can be calculated in the following fashion.

The annual number of loads is:

$$\text{Annual Loads} = 30 \frac{\text{loads}}{\text{hr}} \times 8 \frac{\text{hr}}{\text{day}} \times 350 \frac{\text{days}}{\text{yr}} = 84,000 \frac{\text{loads}}{\text{yr}}$$

The annual natural gas savings are:

$$\Delta(m^3) = 0.0305 \frac{(m^3 \text{ yr})}{\text{lb}} \times 120 \frac{\text{lb}}{\text{load}} \times 84,000 \frac{\text{loads}}{\text{yr}} = 307,440 m^3$$

The annual electric and water savings can be calculated similarly to be:

$$\text{Electric savings} = 15,120 \text{ kWh/yr}$$

$$\text{Water savings} = 12,801,600 \text{ L/yr}$$

USES AND EXCLUSIONS

Residential-style clothes washers do not qualify for this measure. Commercial washers that process heavily soiled laundry do not qualify for this measure because of the higher water temperatures utilized.

MEASURE LIFE

The measure life is 15 years [1].

INCREMENTAL COST

Table 4 shows the incremental costs associated with the two different types of washers and grouped into two different sized bins each.

Table 4: Incremental Costs [1] [5] [6] [7]³

Washer Type	Incremental Cost
Washer extractor – ≤ 60 lbs	\$15,714
Washer extractor – > 60 lbs and < 500 lbs	\$35,714
Washer extractor – ≥ 500 lbs	\$44,286

³ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

Washer Type	Incremental Cost
Tunnel washer – ≤ 120 lbs	\$71,429
Tunnel washer – > 120 lbs and < 500 lbs	\$150,000
Tunnel washer – ≥ 500 lbs	\$228,571

Capital and installation incremental costs were obtained from interviews with manufacturer sales representatives. Please note that installed system costs can be highly variable, especially for the tunnel washer systems which tend to be custom installations. The size and cost of the ozone system are primarily determined by the amount of water being used and the level of soil in the laundry, but can also be affected by the type and arrangement of the washers.

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COMMERCIAL – LOW FLOW PRE-RINSE SPRAY NOZZLE – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT/RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Water Heating → Low-Flow Pre-Rinse Spray Nozzle → New Construction/Time of Natural Replacement /Retrofit	

Table 1 below provides a summary of the key measure parameters and savings coefficients differentiated by facility type.

Table 1. Measure Key Data

Parameter	Definitions	
Measure Category	New Construction (NC) Time of Natural Replacement (TNR) Retrofit (R)	
Baseline Technology	Standard Pre-Rinse Spray Nozzle/Valve supplied with hot water from natural gas fueled water heaters.	Flow rate of 6.1 liters/minute (1.6 gpm) or greater
Efficient Technology	Low-Flow Pre-Rinse Spray Nozzles supplied with hot water from natural gas fueled water heaters.	Flow rate of 2.4 liters/minute (0.64 gpm) or less
Market type	Commercial	
Annual Natural Gas Savings (m ³)	Full service restaurant	453 m ³
	Limited service (fast food restaurant)	89 m ³
	Other	107 m ³
Annual Water Savings (liters)	Full service restaurant	97,529 liter
	Limited service (fast food restaurant)	19,100 liters
	Other	23,025 liters
Measure Life	5 years	
Incremental Cost	Utility to use actual per unit cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.	
Restrictions	Hot water is provided by natural gas water heating system.	

OVERVIEW

Pre-rinse spray nozzles (PRSNs) are commonly utilized in commercial kitchens to remove food waste from dishes and cookware prior to cleaning in the dishwasher, using a pressurized flow of hot water. The nozzles are part of pre-rinse assemblies and typically consist of a spray nozzle, a squeeze handle actuator, an insulated grip, and a dish guard bumper. Studies have concluded that PRSNs can account for up to 1/3 of the total water consumption in a typical commercial kitchen. [1]

APPLICATION

This measure provides incentives for installing low-flow PRSNs, designed to provide sustained levels of performance with reduced flow of hot water.

BASELINE TECHNOLOGY

The baseline technology for the purpose of calculating energy savings is a PRSN with flow rate of 1.6 gpm.

The 2005 EPA Act legislation required all spray nozzles manufactured for sale in the United States to have flow rates of 1.6 gpm or less. While this legislation does not specifically pertain to Canadian sales, it does have an impact on the availability of new PRSNs in Ontario. Because the legislation has been in effect for a period of time exceeding the accepted measure life, it is reasonable to accept the 2005 EPA Act standard as the baseline condition for all categories.

Table 2. Baseline PRSN Requirements

Type	Requirement
2005 EPA Act compliant PRSN	Flow rate of 6.1 liters/min (1.6 gpm)

EFFICIENT TECHNOLOGY

Low-flow PRSNs that meet the requirements as shown in Table 3 are supplied with hot water produced by natural gas fueled water heaters.

Table 3. Efficient PRSN Requirements

Type	Requirement
Low-Flow PRSN	Flow rate of 2.4 liters/min (0.64 gpm) or less

ENERGY IMPACTS

The primary energy impact associated with the installation of low-flow PRSN is natural gas savings associated with a reduction in hot-water consumption. Table 1 above provides annual savings coefficients, differentiated by the type of facility.

Water consumption impacts are also provided in Table 1.

NATURAL GAS SAVINGS ALGORITHM

The measure savings are based on the facility type and the values provided in Table 1.

The algorithm leading to the savings values first calculates the reduction in water consumption, and then determines the natural gas savings attributable to this reduction. Equations leading the savings values are as described below.

$$W_{savings} = (Flow_{baseline} - Flow_{efficient}) \times 60 \frac{Minutes}{Hour} \times Utilization$$

where,

$W_{savings}$ = annual reduction in water consumption (liters/year)

$Flow_{baseline}$ = the defined baseline flow from (liters/minute)

$Flow_{efficient}$ = the defined efficient flow from (liters/minute)

$Utilization$ = the annual hours of utilization from (hours/year)

The annual natural gas savings is then calculated as:

$$NG_{savings} = W_{savings} \times \%_{hot} \times Cp_{water} \times \rho_{water} \times (T_{out} - T_{in}) \times \frac{1}{NG_{ec}}$$

where,

$NG_{savings}$ = annual natural gas savings (m³/year)

$W_{savings}$ = annual reduction in water consumption calculated above (liters/year)

$\%_{hot}$ = % of total PRSN flow from hot water supply

Cp_{water} = specific heat of water (Btu/gal-°F)

ρ_{water} = density of water (lb/gal)

- T_{out} = average water heater set-point (°F)
 T_{in} = average water heater inlet temperature (°F)
 Eff_{wh} = average water heater recovery efficiency
 NG_{ec} = Average energy content of natural gas (Btu/m³)

ASSUMPTIONS

The assumptions used to calculate the savings coefficients are shown in Table 1.

Table 1. Assumptions

Parameter	Value	Source/Comments
Annual Utilization – Full Service Restaurants	447.3 hours / year	[2]
Annual Utilization – Limited Service (Fast Food) Restaurants	87.6 hours / year	[2]
Annual Utilization – Other	105. 6 hours / year	[2]
% Hot Water to Supplied to PRSN	69%	[2]
Specific Heat Capacity of Water (in applicable temperature range)	1.0 Btu/lb - °F	Common assumptions table
Density of Water	8.3 lb/gal	Common assumptions table
Average Inlet Water Temperature	9.384°C (48.9 °F)	Common assumptions table
Water Heater Set-Point	60°C (140 °F)	Common assumptions table
Commercial Water Heating Efficiency	83%	Common assumptions table
Energy Content Density of Natural Gas	35,738 Btu/m ³	Common assumptions table

SAVINGS CALCULATION EXAMPLE

The example below illustrates how the savings value is determined for a PRSN installed at a full service restaurant:

$$NG_{savings} = W_{savings} \times \%_{hot} \times Cp_{water} \times \rho_{water} \times (T_{out} - T_{in}) \times \frac{1}{NG_{ec} \times Eff_{wh}}$$

$$\begin{aligned}
 &= \frac{97,529 \frac{\text{liters}}{\text{year}}}{3.785 \frac{\text{liters}}{\text{gal}}} \times 69\% \times 1 \frac{\text{Btu}}{\text{lb} - ^\circ\text{F}} \times 8.3 \frac{\text{lb}}{\text{Gal}} \times (140^\circ\text{F} - 48.9^\circ\text{F}) \times \frac{1}{35,738 \frac{\text{Btu}}{\text{m}^3}} \\
 &= 453 \frac{\text{m}^3}{\text{year}}
 \end{aligned}$$

USES AND EXCLUSIONS

To qualify for this measure the PRSN must meet or exceed the minimum efficiency as defined in the above section "Efficient Technology." Service/Domestic hot water must be provided by a natural gas fueled water heater.

MEASURE LIFE

The measure life attributed to this measure is 5 years. [2] [3] [4]

INCREMENTAL COST

Table 6 presents the measure incremental cost.

Table 6. Incremental Cost

Measure Category	Incremental Cost (\$)
New Construction/ Time of Natural Replacement/Retrofit	Utility to use actual per unit cost in the year when savings are claimed. Likewise, installation costs to be determined similarly, based on utility in-field experience.

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COMMERCIAL – CONDENSING TANKLESS GAS WATER HEATERS – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Water Heating → Condensing Tankless Water Heater → New Construction/Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings coefficients.

Table 1. Measure Key Data

Parameter	Definition			
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)			
Baseline Technology	Non-Condensing Storage Water Heater 75 kBtu/hr. and greater Thermal efficiency of units shipped = 80.1% Stand-by Loss $Q/0.8 + 110\sqrt{V_0}$			
Efficient Technology	Condensing Tankless Water Heater 75 kBtu/hr. and greater Thermal efficiency of units shipped = 92.9% Stand-by Loss = negligible			
Market Type	Commercial			
Annual Natural Gas Savings Rate (m ³ /kBtu/hr + m ³)	Utilization Category	Combustion Efficiency Savings	Input Rating	Storage Savings
	Low	0.790 m ³ /kBtu/hr. input	<200 kBtu/hr.	212 m ³
			≥ 200 kBtu/hr.	326 m ³
	Medium	1.290 m ³ /kBtu/hr. input	<200 kBtu/hr.	212 m ³
			≥ 200 kBtu/hr.	326 m ³
	High	1.79 m ³ /kBtu/hr. input	<200 kBtu/hr.	212 m ³
≥ 200 kBtu/hr.			326 m ³	
Measure Life	20 years			
Incremental Cost (\$ CAD)	\$2,227			
Restrictions	This measure applies to the installation of natural gas condensing tankless water heaters in commercial facilities.			

OVERVIEW

The measure consists of the installation of natural gas condensing tankless water heaters for hot water production in commercial facilities. Non-condensing tankless water heaters are not eligible under this measure.

Tankless, also called instantaneous or on-demand, water heaters provide hot water without using a storage tank. There is nominal “storage”, in the form of water in the coil, but it is typically less than 2 gallons and standby losses can be considered negligible. This reduced storage capacity results in the need for higher capacity burners to generate the flow of hot water necessary to serve equivalent peak loads. This translates to higher equipment and installation costs for these units.

The savings from installing condensing tankless hot water units result from two factors: a higher average thermal efficiency and the elimination of the standby losses associated with the storage units.

Thermal Efficiency

Condensing water heaters reclaim a significant quantity of thermal energy from exhaust gases, improving the overall efficiency by up to 10% over non-condensing models. The shipment weighted average efficiency for non-condensing storage units provided in Table 1 were derived by Caneta Research Inc. as part of a 2009 study. [1] The efficiency, calculated using manufacturers published thermal efficiency data and market share information provided by the Consortium for Energy Efficiency is 80.1% and does not include the impact of standby losses.

The shipment weighted average efficiency for the condensing tankless units is taken from the same report by Caneta. The report indicates that market share data was not available for tankless units. The reported shipment weighted average efficiency of 92.9% assumes an even distribution of sales between manufactures offering a condensing tankless model.

The annual savings values attributed to the increased thermal efficiency are reported in units of m³ natural gas per kBtu/hr. rated input capacity of the tankless unit. The savings values are differentiated by the anticipated utilization level of the water heater based on the type of facility where it is installed.

Standby Losses

There is continuous loss from storage water heaters to the surrounding space, with the magnitude of this loss largely dependent upon the size of the storage tank. The standby loss savings values reported in Table 1 were determined by applying the standby loss term from Ontario Building Code SB-10 document [2]

$$\text{Storage loss} = \frac{Q}{0.8} + 110\sqrt{V_0}$$

Where,

Q = the input rating of the water heater in kBtu/hr.

V_0 = the storage capacity in gallons

Annual savings values attributed to the elimination of standby loss for tankless units are reported in units of m³, and are differentiated by the input capacity of the tankless units being installed.

For most commercial installations, storage water heaters are located in mechanical spaces that are not intentionally maintained at the temperature of the occupied space, and savings resulting from reduced standby losses does not add to the space heating load for the facility. The savings are not de-rated to reflect any increase in the overall facility space heating load.

The algorithms and the associated variables are presented in the “Natural Gas Savings Algorithm” section.

APPLICATION

This measure provides incentives for installing tankless natural gas water heaters in commercial facilities for either the new construction or time of natural replacement measure category. The units provide service hot water for entire commercial facilities, or in some cases for selected loads within the facility.

BASELINE TECHNOLOGY

The baseline technology for this measure is a non-condensing natural gas fueled storage water heater, rated 75 kBtu/hr. and greater [2] [3], providing the service hot water needs for all or portions of commercial facilities.

Table 1 provides the shipment weighted average thermal efficiency for non-condensing storage water heaters meeting these criteria.

EFFICIENT TECHNOLOGY

The high efficiency technology is a natural gas fueled condensing tankless water heater. Tankless water heaters with input rating of 200 kBtu/hr. or greater are considered commercial units, but smaller units are frequently installed in commercial facilities to serve all of the service water needs or selected end uses. Units with input capacity of 75 kBtu/hr. [2] [3] or greater are eligible for this measure. Units must be certified according to the appropriate CSA standard such as: CAN/CSA P.7-10, CSA 4.3/ANSI Z21.10.3, or DOE 10 CFR Part 431.

Table 1 provides the shipment weighted average thermal efficiency of tankless condensing water heaters from the Caneta report referenced earlier.

ENERGY IMPACTS

Natural gas savings are achieved as a result of the higher overall average thermal efficiency of the condensing tankless units and elimination of storage or standby losses.

There are no electric or water consumption impacts associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Shipment-weighted overall average efficiency values for non-condensing storage and condensing tankless water heaters are as shown in Table 2. The values are based on manufacturers published efficiency ratings and market share data obtained in a 2009 study completed for Union Gas. [1]

Table 2. Shipment-Weighted Average Commercial Water Heater Efficiencies

Type	Average Efficiency
Storage	80.1%
Tankless	92.9%

The 2011 ASHRAE Application Handbook provides typical peak hourly demand and average daily hot water consumption data for several building types. [4] A 2012 Enbridge Gas funded study [5] indicates that water heaters are generally sized based on peak 15-minute demands with an oversizing factor applied. The same study includes data indicating the peak 15-minute demand can be estimated as 140% of the peak hourly demand. These values were used to derive Equivalent Full Load Hours (EFLH) values using the following algorithm.

$$EFLH = Demand_{avg. daily} \times \frac{1}{Demand_{peak 15 minute} \times OS_{factor}} \times Days per year$$

Where,

- EFLH* = The annual EFLH (hours/year)
- Demand_{avg. daily}* = The reported average daily service hot water demand for a specific building type (US gallon/occupant-day) [4]
- Demand_{peak 15 minute}* = The peak 15-minute hot water demand for a specific building type (US gallon/occupant-hour) [4] [5]
- OS_{factor}* = Typical tankless water heater oversizing factor relative to 15-minute peak demand (200%)¹ [5]
- Days per year* = The number of days per year when the facility is operational

¹ This value is on the higher end of the range of typical oversizing for storage water heaters. Storage water heaters can be more closely sized to the peak load than tankless units. In the case of tankless water heaters there is no buffer, such as a hot water tank, to meet the demand.

Table 3 provides the EFLH values derived from this data and a description of typical building types and end uses for each utilization category.

Table 3. Utilization Categories and EFLH Values

Category	EFLH	Typical End Uses	Facility Types
Low Utilization	176	Lavatories (hand washing), kitchenette, custodial uses	Elementary schools, office, retail, churches
Medium Utilization	287	Low to moderate use showers, fast food kitchen	Secondary schools, fast food restaurant, dormitories, other
High Utilization	399	High use showers, full commercial kitchen, laundry	Fitness center, full service restaurant, hotels, in patient health care, multi-residential

These average efficiency and EFLH values are used to derive savings values representing the annual natural gas savings (m³ per kBtu/hr. input rating) associated with the increase in the thermal efficiency values for each utilization category based on the following algorithm.

$$Thermal\ Efficiency\ Savings = EFLH \times \left(\frac{\eta_{proposed}}{\eta_{baseline}} - 1 \right) / NG_{ec}$$

Where,

- Thermal Efficiency Savings* = Annual natural gas saving in m³ per kBtu/hr. input rating of condensing tankless water heater
- EFLH* = Annual Equivalent Full Load Hours for the utilization category (hours) (see Table 3)
- $\eta_{proposed}$ = The weighted shipment average efficiency for tankless water heaters (see Table 2)
- $\eta_{baseline}$ = The weighted shipment average efficiency for storage water heaters (see Table 2)
- NG_{ec} = Natural Gas Energy content (35.738 kBtu/m³)

The results are provided in Table 4 below.

Table 4. Natural Gas Savings Resulting from Thermal Efficiency Differential

Category	Savings
Low Utilization	0.79 m ³ per kBtu/hr. input
Medium Utilization	1.29 m ³ per kBtu/hr. input
High Utilization	1.79 m ³ per kBtu/hr. input

The stand-by loss equation from the Ontario Building Code was used to determine annual stand-by losses for the baseline storage water heaters.

$$SL_{baseline} = \frac{Q_{baseline}}{0.8} + 110 X \sqrt{V_{0\ baseline}}$$

Where,

$SL_{baseline}$ = The calculated stand-by losses from the storage water heater (kBtu/yr.)

$Q_{baseline}$ = The input energy rating for the storage water heater (kBtu/hr.)²

$V_{0\ baseline}$ = The storage capacity of the storage water heater (gallons)³

The eliminated standby losses are summarized in Table 5 below:

Table 5. Natural Gas Savings Resulting from Eliminated Stand-by Losses

Tankless Unit Input Capacity	Savings
< 200 kBtu/hr	212 m ³
≥ 200 kBtu/hr.	326 m ³

The total savings are the sum of the savings associated with the thermal efficiency differential and the eliminated standby losses;

$$Total\ Savings = Thermal\ Efficiency\ Savings + Eliminated\ Standby\ Losses$$

² Input energy ratings for the equivalent storage units are equal to 65% of the tankless input rating.

³ For tankless units less than 200 kBtu/hr. input rating, the equivalent storage water heater tank capacity is assumed to be 50 gallons. For tankless units of 200 kBtu/hr. and greater input rating, the equivalent storage water heater tank capacity is assumed to be 100 gallons.

ASSUMPTIONS

Table 6 provides a list of assumptions utilized in the measure savings algorithms to derive the savings values listed in Table 1 above.

Table 6. Assumptions

Variable	Definition	Inputs	Source/Comments
EFLH	Annual equivalent full load hours of operation	Typical peak and hourly average hot water consumption values	Based on data from the ASHRAE HVAC Application Handbook [4] as shown in EFLH formula in the Natural Gas Savings Algorithm section.
η_{proposed} & η_{baseline}	Shipment weighted average efficiency of proposed and baseline units	Results of baseline study	Caneta Research Inc. [6]
Q_{baseline}	Input power rating for equivalent storage water heater	Assumed to be 65% of tankless input power rating	Water heater sizing guidelines from AMEC 2012 report [5]
$V_{0 \text{ baseline}}$	Volume of equivalent storage water heater storage	50 gallons for tankless units less than 200 kBtu/hr., 100 gallons for larger tankless units	Supported by manufacturers specifications data and sizing tools for typical storage units

SAVINGS CALCULATION EXAMPLE

The example below illustrates how savings would be calculated for a tankless water heater with rated input capacity of 400 kBtu/hr. in a full service restaurant.

Table 3 above indicates that installation in a full service restaurant is in the high utilization category, with a savings value from Table 1 of 1.79 m³ per kBtu/hr. rated input capacity, and standby loss value of 326 m³.

Annual natural gas savings attributed to this installation are calculated as:

$$1.79 \frac{\text{m}^3}{\text{kBtu/hr}} \times 400 \frac{\text{kBtu}}{\text{hr}} + 326 \text{m}^3 = 1,042\text{m}^3$$

USES AND EXCLUSIONS

Natural gas-fueled condensing tankless water heaters installed in commercial facilities and serving all or part of the service water heating load qualify for this measure. The measure type must be new construction or time of natural replacement installation where the preexisting unit was a natural gas non-condensing, power vented, storage unit. Non-condensing tankless water heaters are not eligible.

MEASURE LIFE

The measure life is 20 years. [7]

INCREMENTAL COST

The incremental cost data is taken from an incremental cost study completed for six efficiency programs in the northeast US during 2011. [8]

Data reviewed from this and other studies did not show significant variation in incremental cost over the anticipated size range. The average values from the study are reported in Table 7.

Table 7. Incremental Cost⁴

Material	Installation	Total
\$1,327	\$900	\$2,227

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COMMERCIAL – KITCHEN – DEMAND CONTROLLED VENTILATION – NEW CONSTRUCTION/TIME OF NATURAL REPLACEMENT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Kitchen – Demand Controlled Ventilation → New Construction / Time of Natural Replacement	

Table 1 provides a summary of the key measure parameters and savings coefficient.

Table 1. Measure Key Data

Parameter	Definition	
Measure Category	New Construction (NC) Time of Natural Replacement (TNR)	
Baseline Technology	Constant volume commercial kitchen ventilation	
Efficient Technology	Automated, variable/demand flow, commercial kitchen ventilation	
Market Type	Commercial	
Annual Natural Gas Savings (m ³)	Hood Capacity	Savings
	Up to 5,000 CFM	4,207 m ³ per year
	5,001 – 10,000 CFM	10,517 m ³ per year
	10,001 – 15,000 CFM	17,529 m ³ per year
Annual Electric Savings (kWh)	Hood Capacity	Savings
	Up to 5,000 CFM	4,940 kWh per year
	5,001 – 10,000 CFM	16,294 kWh per year
	10,001 – 15,000 CFM	28,929 kWh per year
Measure Life	15 years	
Incremental Cost (\$ CAD)	Hood Capacity	Incremental Cost
	Up to 5,000 CFM	\$2,383
	5,001 – 10,000 CFM	\$5,958
	10,001 – 15,000 CFM	\$9,929
Restrictions	Limited to spaces with natural gas fueled space heating and commercial kitchen hoods with capacity of 15,000 CFM or less.	

OVERVIEW

Commercial Kitchen Ventilation (CKV) systems exhaust smoke, flue gases, heat and cooking odors. Traditional systems use simple on/off fan motor controls that operate at full flow regardless of the quantity of contaminants to be exhausted. Make up air is supplied by a dedicated make-up air unit, or from a whole building ventilation system, either directly through ductwork, or indirectly from adjoining spaces. Commercial Demand Controlled Ventilation (DCV) systems are added to CKV systems to modulate the flow in response to the rate that contaminants are generated.

DCV systems are typically comprised of: a variable frequency drive to control fan motor speed; a sensor or sensors to determine the level of contaminants; a controller or processor to interpret the sensor signal and send a corresponding signal to the drive; and some form of user interface. There are several manufacturers of kitchen DCV systems including Accuerex, Aerco Industries, CaptiveAire, Green Energy Hoods, Greenheck, Halton, Melink, Noveo, and Spring Air. [1]

There are several strategies for sensing the level of contaminants and modulating the exhaust flow-rate, with sensors that detect the exhaust stream opacity and/or temperature being the most common. Other types of control are based on a time schedule, or on feedback from appliances indicating their operating status. Controls are calibrated to modulate fan speed and exhaust flow between full rated capacity when high levels of contaminants are present and minimum flow when no contaminants are detected.

Energy savings are associated with reductions in fan power, space heating, and space cooling loads.

APPLICATION

This measure applies to new commercial kitchen exhaust hoods with rated capacity of not more than 15,000 CFM, equipped with DCV systems as described above. Spaces must be heated with natural gas to qualify for this measure.

BASELINE TECHNOLOGY

A new constant volume kitchen exhaust hood with rated capacity not greater than 15,000 CFM.

EFFICIENT TECHNOLOGY

The efficient technology is a commercial kitchen demand controlled ventilation system with rated capacity not greater than 15,000 CFM, consisting of sensor(s) that determine the level of contaminant in the exhaust air stream, a controller that processes inputs from the sensor(s), and variable frequency drives that receive a signal from the controller and modulate the exhaust and make up air fans to optimize flow rates.

ENERGY IMPACTS

The reduction in the requirement for make-up air results in natural gas savings during the heating season and electric energy savings during the cooling season. In addition, there is significant electric energy savings associated with reduced fan speeds. There is no water usage impact associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Natural gas savings result from reduced exhaust and corresponding make-up air flow rates. The savings values reported in Table 1 are derived using accepted engineering principles and empirical data taken from published case studies representing nineteen commercial kitchen DCV installations. [2] [3] [4] [5]

Because the savings are directly dependent upon hood exhaust capacity expressed in CFM, saving values are provided for three ranges of size, with the savings value based on the midpoint of flow range category.¹

Data from the case studies includes measured average fan input power data for operation under constant volume (baseline) conditions and with DCV systems installed (efficient case). This data was used in conjunction with the fan affinity laws to calculate the average the percent reduction in fan speed and air flow for the nineteen installations as follows.

$$\% \text{ Flow Reduction} = ((\text{Flow Baseline} - \text{Flow EE}) / \text{Flow Baseline}) \times 100\%$$

$$\% \text{ Flow Reduction} = (1 - (\text{Flow EE} / \text{Flow Baseline})) \times 100\%$$

$$\text{Affinity law: } (\text{Flow Efficient} / \text{Flow Baseline})^3 = (FP_{\text{efficient}} / FP_{\text{baseline}}), \text{ or}$$

$$(\text{Flow Efficient} / \text{Flow Baseline}) = (FP_{\text{efficient}} / FP_{\text{baseline}})^{0.333}$$

$$\text{Substituting leads to: } \% \text{ Flow Reduction} = \left[1 - \left(\frac{FP_{\text{efficient}}}{FP_{\text{baseline}}} \right)^{0.333} \right] \times 100\%$$

Where,

$\% \text{ Flow Reduction}$	= The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)
FP_{baseline}	= The average total, (exhaust hood and make up air) fan power for the baseline condition. (kW)
$FP_{\text{efficient}}$	= The average total, (exhaust hood and make up air) fan power for the efficient case. (kW)

This resulted in a percent reduction in flow for each of the nineteen case studies ranging from 12% to 38% with an overall weighted average percent reduction of 25.1%.

¹ Because hood with capacity less than 1,000 CFM are rarely installed, the midpoint of the 0 - 5,000 CFM category was set at 3,000 CFM.

The overall average heating load associated with the introduction of outside air was determined using an Outdoor Air Load Calculator tool [6], developed by The Food Service Technology Center. Annual heating loads expressed in Btu per CFM of outside air were determined using climate data representing London, Ontario and North-Bay, Ontario, with heating season temperature set-points of 22.2°C (72°F), and a daily operating schedule of 6:00 AM through 10:00 PM.

A 2014 distribution of kitchen DCV projects provided by the utilities reflected approximately 70% of installations in areas represented by the London weather data, with 30% represented by North-Bay. These values were used with the London and North-Bay annual heating load to derive a weighted-average annual heating load value of 159,733 Btu per CFM.

This value was used in the following equation to derive natural gas savings values for each of the three kitchen exhaust hood size categories.

$$NG\ Savings = \frac{(OAHL \times Capacity \times \% Flow\ Reduction)}{(Eff_{heating} \times EC_{NG})}$$

Where,

- NG Savings* = Annual natural gas savings (m³)
- OAHL* = The weighted average annual outdoor air heating load (Btu/year per CFM)
- Capacity* = The midpoint of the kitchen hood size range (CFM)
- % Flow Reduction* = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)
- Eff_{heating}* = Efficiency of the space heating system (80%)
- EC_{NG}* = Energy content of natural gas (35,738 Btu/m³)

This equation was used to calculate the natural gas savings for the midpoint of each kitchen hood capacity category as shown in Table 2 below.

Table 2. Natural Gas Savings

Hood Capacity (CFM)	Savings (m ³ per Year)
3,000	4,207
7,500	10,517
12,500	17,579

ELECTRIC SAVINGS ALGORITHMS

Electric energy savings associated with this measure primarily result from a reduction in fan energy associated with VFD controlled modulation of the exhaust hood and make-up air fans. Additional electric savings result from reduced cooling load associated with a decrease in outside air introduced to the space during the cooling season.

Data reflecting system capacities and average baseline fan energy for the case-studies referenced above revealed a relatively consistent increase in fan power relative to system capacity. The baseline values were plotted against system capacity and revealed a roughly linear relationship described by the following equation.

$$Fan\ Input\ Power_{baseline} = 0.73010 \times System\ Capacity - 0.78175$$

Where,

$Fan\ Input\ Power_{baseline}$ = The baseline unitary input power (kW)
 $System\ Capacity$ = The rated capacity of the kitchen exhaust hood (CFM)

This equation was used to calculate the baseline input fan power for the midpoint of each kitchen hood capacity category as shown in Table 3 below.

Table 3. Baseline Input Fan Power

Hood Capacity (CFM)	Baseline Input Fan Power (kW)
3,000	1.41
7,500	4.69
12,500	8.34

The values from table two, the average 25.1% flow reduction derived above, and the fan affinity laws were then used to predict the average input power with the DCV system installed, for the midpoint of each capacity category using the following equation.

$$FP_{efficient} = FP_{baseline} \times (1 - \%Flow\ Reduction)^3$$

Where,

$FP_{efficient}$ = The average total, (exhaust hood and make up air) fan power for the efficient case. (kW)
 $FP_{baseline}$ = The average total, (exhaust hood and make up air) fan power for the baseline condition. (kW)
 $\% Flow\ Reduction$ = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)

The annual fan power savings for each exhaust hood capacity category was then calculated as follows:

$$FP\ Savings = (FP_{baseline} - FP_{efficient}) \times Annual\ Hours$$

Substituting the above equation for $FP_{efficient}$ leads to the following:

$$FP\ Savings = (FP_{baseline} - FP_{baseline} \times (1 - \%Flow\ Reduction)^3) \times Annual\ Hours$$

Where,

- $FP\ Savings$ = The annual fan power electric savings (kWh/Year)
- $FP_{efficient}$ = The average total, (exhaust and make up air) fan power for the efficient case. (kW)
- $FP_{baseline}$ = The average total, (exhaust and make up air) fan power for the baseline condition. (kW)
- $Annual\ Hours$ = The annual operating hours of the system (5,840 Hours/Year)²

The resulting fan power savings are shown in Table 4 below.

Table 4. Fan Power Savings

Hood Capacity (CFM)	Savings (kWh/year)
3,000	4,774
7,500	15,881
12,500	28,240

Cooling season energy savings are calculated in the same manner as the heating season savings with cooling equipment efficiency and electricity energy content substituted for the heating efficiency and natural gas energy content values. The algorithm is as follows.

$$Cooling\ Savings = \frac{(OACL \times Capacity \times \%Flow\ Reduction)}{(Eff_{cooling} \times EC_{Elec})}$$

Where,

- $Cooling\ Savings$ = Annual cooling energy savings (kWh)
- $OACL$ = The weighted average annual outdoor air cooling load (Btu/Year per CFM)
- $Capacity$ = The midpoint of the kitchen hood size range (CFM)

² Sixteen hours per day, seven days per week is the assumed operating hours from the previous version of substantiation sheets. Data from the nineteen case studies referenced earlier supports this assumption.

- % Flow Reduction* = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)
- Eff_{cooling}* = Efficiency of the space cooling equipment (COP = 3.81)
- EC_{elec}* = Energy content of electricity (3,412 Btu/kWh)

The resulting savings for each exhaust hood size category were added to the fan power savings to derive the overall electric savings values reflected in Table 5 below. These values are added to the fan savings from Table 3 to derive the total electric savings reported in Table 1.

Table 5. Fan Power Savings

Hood Capacity (CFM)	Savings (kWh/year)
3,000	166
7,500	413
12,500	689

ASSUMPTIONS

Table 6 provides a list of assumptions utilized in the measure savings algorithms provided above and leading to the savings values listed in Table 1.

Table 6. Assumptions

Variable	Definition	Value	Inputs	Source
<i>%Flow Reduction</i>	The average reduction in exhaust hood flow rate as a % of rated capacity	25.1%	Derived from empirical fan input power data from nineteen case studies.	[2] [3] [4] [5]
<i>Unitary Fan Input Power_{baseline}</i>	Baseline fan input power per CFM of exhaust hood capacity	$0.00073 \times 1000 \text{ CFM} - 0.78715$	Derived from empirical fan input power data from nineteen case studies.	[2] [3] [4] [5]
<i>OAHL</i>	The annual outdoor air heating load for the service territory. (Btu/CFM)	159,733 Btu/CFM	Weather data for London and North Bay, specified operating hours	[6]
<i>OACL</i>	The annual outdoor air cooling load for the service territory. (Btu/CFM)	2,856 Btu/CFM	Weather data for London and North Bay, specified operating hours	[6]
<i>Eff_{Heating}</i>	Commercial heating system efficiency	80%		Common assumptions table
<i>Eff_{Cooling}</i>	Commercial cooling system efficiency	13 SEER		[7]

Variable	Definition	Value	Inputs	Source
		3.81 COP		
EC _{NG}	Energy Density of Natural Gas	35,738 Btu/m ³		Common assumptions table
EC _{Elec}	Conversion of Btu/kWh	3,412 Btu/kWh		Common assumptions table
Annual Hours	Annual Operating Hours	5,840	16 hours per day, consistent with nineteen case studies	[2] [3] [4] [5]

SAVINGS CALCULATION EXAMPLE

The example below illustrates how savings values are calculated for the 5,000 - 10,000 CFM exhaust hood size category.

Capacity = Midpoint of size category: 7,500 CFM

$$NG\ Savings = \frac{(OAHL \times Capacity \times \% \text{ Flow Reduction})}{(Eff_{heating} \times EC_{NG})}$$

$$= (159,733 \text{ Btu/CFM} \times 7,500 \text{ CFM} \times 25.1\%) / (80.0\% \times 35,738 \text{ Btu/m}^3)$$

$$= 10,517 \text{ m}^3 \text{ per year}$$

$$FP\ Savings = (FP_{baseline} - FP_{baseline} \times (1 - \% \text{ Flow Reduction})^3) \times Annual\ Hours$$

$$= (4.69 \text{ kW} - 4.69 \text{ kW} \times (1 - 25.1\%)^3) \times 5,840 \text{ hours per year}$$

$$= 15,881 \text{ kWh per year}$$

$$Cooling\ Savings = \frac{(OACL \times Capacity \times \% \text{ Flow Reduction})}{(Eff_{cooling} \times EC_{Elec})}$$

$$= (2,856 \text{ Btu/CFM} \times 7,500 \text{ CFM} \times 25.1\%) / (3.81 \times 3,412 \text{ Btu/kWh})$$

$$= 413 \text{ kWh per year}$$

USES AND EXCLUSIONS

This measure applies to new commercial kitchen exhaust hoods with rated capacity of not more than 15,000 CFM that are equipped with DCV systems as described above. Spaces must be heated with natural gas to qualify for this measure.

Projects for new DCKV system of greater than 15,000 CFM rated capacity should be reviewed under custom project guidelines.

“Short-circuit” hoods that utilize the hood as a plenum for unconditioned make-up air are not eligible for this measure.

MEASURE LIFE

The measure life is 15 years. [8]³

INCREMENTAL COST

Cost data provided for ten of the nineteen case studies reflected an average installed measure cost of \$1.70 per CFM of hood capacity for retrofit installations [2] [3] [4] [5]. There was no breakdown between equipment and installation and no data reflecting incremental cost for new installations could be located. One resource [4] estimated the incremental cost for new installation at 50% of the average retrofit cost. Applying 50% of the average total cost from the ten retrofit case studies to the midpoint of the three size categories leads to the incremental cost values reported here.

Table 7: Incremental Cost ⁴

Category	Incremental Cost
Up to 5,000 CFM	\$2,383
5,001 – 10,000 CFM	\$5,958
10,001 – 15,000 CFM	\$9,929

REFERENCES

- [1] Consortium for Energy Efficiency, "Commercial Kitchen Ventilation - An Energy Efficiency Program Administrator's Guide to Demand Control Ventilation," Consortium for Energy Efficiency, Boston, MA, 2010.
- [2] D. Fisher, "Future of DCV for Commercial Kitchens," *ASHRAE Journal*, no. February 2013, pp. 48 - 54, 2013.
- [3] Food Service Technology Center, "Demand Control Ventilation in Commercial Kitchens - An Emerging Technology Case Study - FSTC Report 5001-06.13," Fisher Nickel, Inc., San Ramon, CA, 2006.
- [4] San Diego Gas & Electric, "Work Paper WPSDGENRCC0019 - Commercial Kitchen Demand Controls - Electric," San Diego Gas & Electric, San Diego, CA, 2012.

³ Measure life documentation for Kitchen DCV was not found. The CPUC DEER database provides measure life of 15 years for VFDs controlled with CO² sensors.

⁴ Converted to CAD based on Daily Currency Converted for Bank of Canada, as of 1/22/2016. (<http://www.bankofcanada.ca/rates/exchange/daily-converter/>)

- [5] Southern California Edison - Design and Engineering Services, "Demand Control Ventilation for Commercial Kitchen Hoods," Southern California Edison, Rosemead, CA, 2009.
- [6] Food Service Technology Center, "Food Service Technology Center - Outdoor Air Load Calculator," Fisher-Nickel, Inc. - for Pacific Gas and Electric, 2014. [Online]. Available: <http://www.fishnick.com/ventilation/oalc/>. [Accessed 3 November 2014].
- [7] Ministry of Municipal Affairs and Housing-Building and Development Branch, "Supplemental Standard SB-10 (Energy Efficiency Supplement)," Ministry of Municipal Affairs and Housing, Toronto, 2011.
- [8] California Public Utilities Commission, "DEER2014 EUL Table Update," 4 February 2014. [Online]. Available: <http://www.deeresources.com/>. [Accessed 18 August 2014].

COMMERCIAL – KITCHEN – DEMAND CONTROLLED VENTILATION – RETROFIT

Version Date and Revision History	
Version	1
OEB Filing Date	Dec 21, 2016
OEB Approval Date	
Commercial → Space Heating → Kitchen – Demand Controlled Ventilation → Retrofit	

Table 1 Table 1 provides a summary of the key measure parameters and savings coefficient.

Table 1. Measure Key Data

Parameter	Definition	
Measure Category	Retrofit (R)	
Baseline Technology	Constant volume commercial kitchen ventilation	
Efficient Technology	Automated, variable/demand flow, commercial kitchen ventilation	
Market Type	Commercial	
Annual Natural Gas Savings (m ³)	Hood Capacity	Savings
	Up to 5,000 CFM	4,207 m ³ per year
	5,001 – 10,000 CFM	10,517 m ³ per year
	10,001 – 15,000 CFM	17,529 m ³ per year
Annual Electric Savings (kWh)	Hood Capacity	Savings
	Up to 5,000 CFM	4,940 kWh per year
	5,001 – 10,000 CFM	16,294 kWh per year
	10,001 – 15,000 CFM	28,929 kWh per year
Measure Life	15 years	
Incremental Cost (\$CAD)	Hood Capacity	Incremental Cost
	Up to 5,000 CFM	\$4,766
	5,001 – 10,000 CFM	\$11,915
	10,001 – 15,000 CFM	\$19,859
Restrictions	Limited to spaces with natural gas fueled space heating and commercial kitchen hoods with capacity of 15,000 CFM or less.	

OVERVIEW

Commercial Kitchen Ventilation (CKV) systems exhaust smoke, flue gases, heat and cooking odors. Traditional systems use simple on/off fan motors controls that operate at full flow

regardless of the quantity of contaminants to be exhausted. Make up air is supplied by a dedicated make-up air unit, or from a whole building ventilation system, either directly through ductwork, or indirectly from adjoining spaces. Commercial Demand Controlled Ventilation (DCV) systems are added to CKV systems to modulate the flow in response to the rate that contaminants are generated.

DCV systems are typically comprised of: variable frequency drives to control fan motor speed; a sensor or sensors to determine the level of contaminants; a controller or processor to interpret the sensor signal and send a corresponding signal to the drives; and some form of user interface. There are several manufacturers of kitchen DCV systems including Accuerex, Aerco Industries, CaptiveAire, Green Energy Hoods, Greenheck, Halton, Melink, Noveo, and Spring Air. [1]

There are several strategies for sensing the level of contaminants and modulating the exhaust flow-rate, with sensors that detect the exhaust stream opacity and/or temperature being the most common. Other types of control are based on a time schedule, or on feedback from appliances indicating their operating status. Controls are calibrated to modulate fan speed and exhaust flow between full rated capacity when high levels of contaminants are present and minimum flow when no contaminants are detected.

Energy savings are associated with reductions in fan power, space heating, and space cooling loads.

APPLICATION

This measure applies to existing constant volume commercial kitchen exhaust hoods with rated capacity of not more than 15,000 CFM that are retrofit with DCV systems as described above. Spaces must be heated with natural gas to qualify for this measure.

BASELINE TECHNOLOGY

A constant volume kitchen exhaust hood with rated capacity not greater than 15,000 CFM.

EFFICIENT TECHNOLOGY

The efficient technology is a commercial kitchen demand controlled ventilation system with rated capacity not greater than 15,000 CFM, consisting of sensor(s) that determine the level of contaminant in the exhaust air stream, a controller that processes inputs from the sensor(s), and variable frequency drives that receive a signal from the controller and modulate the exhaust and make up air fans to optimize flow rates.

ENERGY IMPACTS

The reduction in the requirement for make-up air results in natural gas savings during the heating season and electric energy savings during the cooling season. In addition, there is significant electric energy savings associated with reduced fan speeds.

There is no water usage associated with this measure.

NATURAL GAS SAVINGS ALGORITHMS

Natural gas savings result from reduced exhaust and corresponding make-up air flow rates. The savings values reported in Table 1 are derived using accepted engineering principles and empirical data taken from published case studies representing nineteen commercial kitchen DCV installations. [2] [3] [4] [5]

Because the savings are directly dependent upon hood exhaust capacity expressed in CFM, saving values are provided for three ranges of size, with the savings value based on the midpoint of each flow range category.¹

Data from the case studies includes measured average fan input power data for operation under constant volume (baseline case) conditions and with DCV systems installed (efficient case). This data was used in conjunction with the fan affinity laws to calculate the average % reduction in fan speed and air flow for each of the nineteen installations as follows.

$$\% \text{ Flow Reduction} = ((\text{Flow Baseline} - \text{Flow Efficient}) / \text{Flow Baseline}) \times 100\%$$

$$\% \text{ Flow Reduction} = (1 - (\text{Flow Efficient} / \text{Flow Baseline})) \times 100\%$$

$$\text{Affinity law:} \quad (\text{Flow Efficient} / \text{Flow Baseline})^3 = (FP_{\text{efficient}} / FP_{\text{baseline}})$$

$$\text{Or,} \quad (\text{Flow Efficient} / \text{Flow Baseline}) = (FP_{\text{efficient}} / FP_{\text{baseline}})^{0.333}$$

$$\text{Substituting leads to: } \% \text{ Flow Reduction} = \left[1 - \left(\frac{FP_{\text{efficient}}}{FP_{\text{baseline}}} \right)^{0.333} \right] \times 100\%$$

Where,

$\% \text{ Flow Reduction}$ = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)

FP_{baseline} = The average total, (exhaust hood and make up air) fan power for the baseline condition. (kW)

$FP_{\text{efficient}}$ = The average total, (exhaust hood and make up air) fan power for the efficient case. (kW)

This resulted in a percent reduction in flow for each of the nineteen case studies ranging from 12% to 38% with an overall weighted average percent reduction of 25.1%.

¹ Because hood with capacity less than 1,000 CFM are rarely installed, the midpoint of the 0 - 5,000 CFM category was set at 3,000 CFM.

The overall average heating load associated with the introduction of outside air was determined using an Outdoor Air Load Calculator tool [6], developed by The Food Service Technology Center. Annual heating loads expressed in Btu per CFM of outside air were determined using climate data representing London, Ontario and North-Bay, Ontario, with heating season temperature set-points of 22.2°C (72°F), and a daily operating schedule of 6:00 AM through 10:00 PM.

A 2014 distribution of kitchen DCV projects provided by the utilities reflected approximately 70% of installations in areas represented by the London weather data, with 30% represented by North-Bay. These values were used with the London and North-Bay annual heating load to derive a weighted-average annual heating load value of 159,733 Btu per CFM.

This value was used in the following equation to derive natural gas savings values for each of the three kitchen exhaust hood size categories.

$$NG\ Savings = \frac{(OAHL \times Capacity \times \% Flow\ Reduction)}{(Eff_{heating} \times EC_{NG})}$$

Where,

- NG Savings* = Annual natural gas savings (m³)
- OAHL* = The weighted average annual outdoor air heating load (Btu/year per CFM)
- Capacity* = The midpoint of the kitchen hood size range (CFM)
- % Flow Reduction* = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)
- Eff_{heating}* = Efficiency of the space heating system (80%)
- EC_{NG}* = Energy content of natural gas (35,738 Btu/m³)

This equation was used to calculate the natural gas savings for the midpoint of each kitchen hood capacity category as shown in Table 2 below.

Table 2. Natural Gas Savings

Hood Capacity (CFM)	Savings (m ³ per Year)
3,000	4,207
7,500	10,517
12,500	17,579

ELECTRIC SAVINGS ALGORITHMS

Electric energy savings associated with this measure primarily result from a reduction in fan energy associated with VFD controlled modulation of the exhaust hood and make-up air fans. Additional electric savings result from reduced cooling load associated with a decrease in outside air introduced to the space during the cooling season.

Data reflecting system capacities and average baseline fan energy for the case-studies referenced above revealed a relatively consistent increase in fan power relative to system capacity. The values were plotted against system capacity and revealed a roughly linear relationship described by the following equation.

$$Fan\ Input\ Power_{baseline} = 0.73010 \times System\ Capacity - 0.78175$$

Where,

$Fan\ Input\ Power_{baseline}$ = The baseline unitary input power (kW/1000 CFM)
 $System\ Capacity$ = The rated capacity of the kitchen exhaust hood (1000 CFM)

This equation was used to calculate the baseline input fan power for the midpoint of each kitchen hood capacity category as shown in Table 3 below.

Table 3. Baseline Input Fan Power

Hood Capacity (CFM)	Baseline Input Fan Power (kW)
3,000	1.41
7,500	4.69
12,500	8.34

The values from table two, the average 25.1% flow reduction derived above, and the fan affinity laws were then used to predict the average input power with the DCV system installed, for the midpoint of each capacity category using the following equation.

$$FP_{efficient} = FP_{baseline} \times (1 - \% Flow\ Reduction)^3$$

Where,

$FP_{efficient}$ = The average total, (exhaust hood and make up air) fan power for the efficient case. (kW)
 $FP_{baseline}$ = The average total, (exhaust hood and make up air) fan power for the baseline condition. (kW)
 $\% Flow\ Reduction$ = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)

The annual fan power savings for each exhaust hood capacity category was then calculated as follows:

$$FP\ Savings = (FP_{baseline} - FP_{efficient}) \times Annual\ Hours$$

Substituting the above equation for $FP_{efficient}$ leads to the following:

$$FP\ Savings = (FP_{baseline} - FP_{baseline} \times (1 - \%Flow\ Reduction)^3) \times Annual\ Hours$$

Where,

- $FP\ Savings$ = The annual fan power electric savings (kWh/Year)
- $FP_{efficient}$ = The average total, (exhaust and make up air) fan power for the efficient case. (kW)
- $FP_{baseline}$ = The average total, (exhaust and make up air) fan power for the baseline condition. (kW)
- $Annual\ Hours$ = The annual operating hours of the system (5,840 Hours/Year)²

The resulting fan power savings are shown in Table 4 below.

Table 4. Fan Power Savings

Hood Capacity (CFM)	Savings (kWh/year)
3,000	4,774
7,500	15,881
12,500	28,240

Cooling season energy savings are calculated in the same manner as the heating season savings with cooling equipment efficiency and electricity energy content substituted for the heating efficiency and natural gas energy content values. The algorithm is as follows.

$$Cooling\ Savings = \frac{(OACL \times Capacity \times \%Flow\ Reduction)}{(Eff_{cooling} \times EC_{Elec})}$$

Where,

- $Cooling\ Savings$ = Annual cooling energy savings (kWh)
- $OACL$ = The weighted average annual outdoor air cooling load (Btu/Year per CFM)
- $Capacity$ = The midpoint of the kitchen hood size range (CFM)

² Sixteen hours per day, seven days per week is the assumed operating hours from the previous version of substantiation sheets. Data from the nineteen case studies referenced earlier supports this assumption.

- % Flow Reduction* = The average % reduction in the exhaust flow rate resulting from the DCV installation (% of baseline flow)
- Eff_{cooling}* = Efficiency of the space cooling equipment (COP = 3.81)
- EC_{elec}* = Energy content of electricity (3,412 Btu/kWh)

The resulting savings for each exhaust hood size category were added to the fan power savings to derive the overall electric savings values reflected in Table 5 below. These values are added to the fan savings from Table 3 to derive the total electric savings reported in Table 1.

Table 5. Fan Power Savings

Hood Capacity (CFM)	Savings (kWh/year)
3,000	166
7,500	413
12,500	689

ASSUMPTIONS

Table 6 provides a list of assumptions utilized in the measure savings algorithms provided above and leading to the savings values listed in Table 1.

Table 6. Assumptions

Variable	Definition	Value	Inputs	Source
<i>%Flow Reduction</i>	The average reduction in exhaust hood flow rate as a % of rated capacity	25.1%	Derived from empirical fan input power data from nineteen case studies.	[2] [3] [4] [5]
<i>Unitary Fan Input Power_{baseline}</i>	Baseline fan input power per CFM of exhaust hood capacity	$0.73010 \times 1000 \text{ CFM} - 0.78715$	Derived from empirical fan input power data from nineteen case studies.	[2] [3] [4] [5]
<i>OAHL</i>	The annual outdoor air heating load for the service territory. (Btu/CFM)	159,733 Btu/CFM	Weather data for London and North Bay, specified operating hours	[6]
<i>OACL</i>	The annual outdoor air cooling load for the service territory. (Btu/CFM)	2,856 Btu/CFM	Weather data for London and North Bay, specified operating hours	[6]
<i>Eff_{Heating}</i>	Commercial heating system efficiency	80%		Common assumptions table

Variable	Definition	Value	Inputs	Source
Eff _{Cooling}	Commercial cooling system efficiency	13 SEER 3.81 COP		[7]
EC _{NG}	Energy Density of Natural Gas	35,738 Btu/m ³		Common assumptions table
EC _{Elec}	Conversion of Btu/kWh	3,412 Btu/kWh		Common assumptions table
Annual Hours	Annual Operating Hours	5,840	16 hours per day, consistent with nineteen case studies	[2] [3] [4] [5]

SAVINGS CALCULATION EXAMPLE

The example below illustrates how savings values are calculated for the 5,000 - 10,000 CFM exhaust hood size category.

Capacity = Midpoint of size category: 7,500 CFM

$$\begin{aligned}
 NG \text{ Savings} &= \frac{(OAHL \times Capacity \times \% \text{ Flow Reduction})}{(Eff_{heating} \times EC_{NG})} \\
 &= (159,733 \text{ Btu/CFM} \times 7,500 \text{ CFM} \times 25.1\%) / (80.0\% \times 35,738 \text{ Btu/m}^3) \\
 &= 10,517 \text{ m}^3 \text{ per year}
 \end{aligned}$$

$$\begin{aligned}
 FP \text{ Savings} &= (FP_{baseline} - FP_{baseline} \times (1 - \% \text{ Flow Reduction})^3) \times Annual \text{ Hours} \\
 &= (4.69 \text{ kW} - 4.69 \text{ kW} \times (1 - 25.1\%)^3) \times 5,840 \text{ hours per year} \\
 &= 15,881 \text{ kWh per year}
 \end{aligned}$$

$$\begin{aligned}
 Cooling \text{ Savings} &= \frac{(OACL \times Capacity \times \% \text{ Flow Reduction})}{(Eff_{cooling} \times EC_{Elec})} \\
 &= (2,856 \text{ Btu/CFM} \times 7,500 \text{ CFM} \times 25.1\%) / (3.81 \times 3,412 \text{ Btu/kWh}) \\
 &= 413 \text{ kWh per year}
 \end{aligned}$$

USES AND EXCLUSIONS

This measure applies to existing constant volume commercial kitchen exhaust hoods with rated capacity of not more than 15,000 CFM that are retrofit with DCV systems as described above. Spaces must be heated with natural gas to qualify for this measure.

Projects for existing DCKV system of greater than 15,000 CFM rated capacity should be reviewed under custom project guidelines.

“Short-circuit” hoods that utilize the hood as a plenum for unconditioned make-up air are not eligible for this measure.

MEASURE LIFE

The measure life is 15 years. [8]³

INCREMENTAL COST

Cost data provided for ten of the nineteen case studies reflected an average installed measure cost of \$1.70 per CFM of hood capacity [2] [3] [4] [5]. Applying this value to the midpoint of the three size categories leads to the incremental cost values reported here.

Table 7: Incremental Cost ⁴

Category	Incremental Cost
Up to 5,000 CFM	\$4,766
5,001 – 10,000 CFM	\$11,915
10,001 – 15,000 CFM	\$19,859

REFERENCES

- [1] Consortium for Energy Efficiency, "Commercial Kitchen Ventilation - An Energy Efficiency Program Administrator's Guide to Demand Control Ventilation," Consortium for Energy Efficiency, Boston, MA, 2010.
- [2] D. Fisher, "Future of DCV for Commercial Kitchens," *ASHRAE Journal*, no. February 2013, pp. 48 - 54, 2013.
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