THIS IS EXHIBIT "O"

REFERRED TO IN THE AFFIDAVIT OF

JANE MUSTAC

SWORN BEFORE ME THIS $24^{\text{TH}}\,\text{DAY}$

OF JULY, 2020. _____ A Commissioner, etc.

Enbridge Pipeline Vehicle Loading Analysis

Proposed NPS 6 Windsor Line along County Road 46, County of Essex Ontario

Introduction:

Enbridge is proposing to replace the existing NPS 10 Windsor Line with a new NPS 6 pipeline. The pipeline will be installed within the road allowance parallel to roads for approximately 64 kms between Chatham-Kent and The County of Essex. There was a concern about the stress of the pipeline in its proposed location as it is likely to be exposed to vehicle loading including but not limited to superloads, particularly on County Road 46 in the County of Essex as the pipelines proposed alignment is within approximately 2m of road edge in some locations. The following analysis will provide results of a load assessment on this new pipeline under vehicle loading conditions to meet the Enbridge's design and operating requirements and those of CSA Z662-15 and to determine the max allowable axle load that can be accepted by the pipeline. Analysis considers the hoop stress due to internal pressure and those imposed on it by the soil and vehicle loading.

Assumptions:

- Basis for axle load will be the Ministry of Transportation Ontario (MTO) legal axle load limit of 9000kgs per axle.
- Superload is considered a vehicle weighing more than 120000kgs, from MTO, A Guide to Oversize/Overweight Vehicles and Loads in Ontario, but is limited to max axle load of 9000kgs per axle.
- Vehicle axle load is to be positioned directly vertical over the pipeline. This arrangement will create the maximum loading for this condition.
- An imbalance factor of 10% which increases the wheel load of the axle to allow for consideration of illegal loads and an impact factor of 1.5 was used to simulate vehicles driving on uneven surface over the pipeline.
- Analysis will consider tired vehicles only, which will simulate the maximum ground pressure over the pipeline. Other vehicles, such as those that ride on tracks generally disperse their weight over a larger area and therefore have a lower ground pressure values than those of tired vehicles.
- Assume the pipeline is backfilled only with the native material found within the road allowance, which is known to be ordinary clay. This is considered a conservative assumption as compacted granular fill over and/or around the pipeline would bear more of the vehicle loading than clay and transfer less to the pipeline.

Pipeline Design Parameters:

Outside Diameter (OD): NPS 6 (168.3mm) Wall Thickness: 4.8mm Material: Gr. 359, Cat. I, HFERW seam, CSA Z245.1-18 steel pipe Specified Minimum Yield Strength: 359 MPa Cover Depth: 100cm Max Op Temp: 20C degree Max Op Pressure: 3450 kPa Min Install Temp: 0C degree Content: Sweet Natural Gas Pipeline design to meet the requirements of Clause 12, of CSA Z661-15 During vehicle loading pipeline shall operate at less than 85% SMYS

Live Loads To Calculate:

- 1. MTO road legal limit or 9000kgs per axle. See analysis equipment label SHL.
- 2. 5 x MTO road legal limit or ~45000kgs per axle. See analysis equipment label 5xSHL
- 3. 10 x MTO road legal limit or ~90000kgs per axle, to simulate a maximum pipeline loading. See analysis equipment label 10xSHL

Results:

In all live load cases the results display that the pipeline operates below allowable stress limits under the proposed design conditions for the pipeline located near or under the travelled portion of the roadway. This includes a superload.

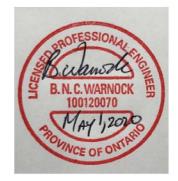
The results of the analysis meet the requirements of the Transportation Association of Canada (TAC) Guidelines For Underground Utilities Crossing Highway Right-Of-Ways.

Results for the 9000kgs and ~45000kgs per axle load considered the impacts of fluctuating hoop stresses or fatigue loading. This can be assumed to represent the case of loads sustained by regular vehicle traffic over the roadway and pipeline.

Results for the \sim 45000kgs per axle analysis displays an allowable loading factor of safety of 5 over what could be expected the normal vehicle use along the roadway.

Results for the ~90000kgs per axle analysis display a near maximum loading that can be accepted by the pipeline. In this case if a superload were to be overweight or given a permit to operate an axle load at greater than 9000kgs up to ~90000kgs per axle the pipeline is robust enough to carry that extreme load.

Analysis performed by Blair Warnock, P.Eng, Senior Pipeline Design Engineer, Enbridge Inc.



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Pipelines Crossed by Equipment on Tires

| Location: | | | | | |
|--|--------------------|--|----------------------------|-------------------|------------------|
| Description & Purpose | NPS 6 Windsor LI | ne - Oversize Vehicle Load Analysis | | | |
| Province | ON | Permanent crossing? Yes | Туре | 3rd Party | |
| Equipment: | | Tire or ground be | aring pressure, psi kPa | 110 758 | |
| Label | SHL | Distance betw | veen axles in set, in cm | 48 122 | |
| Description | MTO limit of 9000 | kgs/axle under Fatigue/Cyclic loading | Axle gauge, ft m | 6.0 1.83 | |
| Axle Load, lb kg | 19,841 8,998 | | Impact Factor | 1.5 | |
| # axles in set | 3 | | Imbalance Factor | 10% | |
| Line(s) to be crossed: | | | | | |
| Line Name | 6WL | | | | |
| OD, in cm | 6.625 16.8 | | | | |
| Wall thickness, in mm | 0.189 4.8 | | | | |
| Pipe grade, ksi MPa | 52 359 | | | | |
| Pressure, psi kPa | 500 3447 | | | | |
| Long seam type | ERW | | | | |
| Installation: | | | | | |
| Depth of cover, in cm | 39 100 | | | | |
| Installation type | Settled | | | | |
| Bottom Reaction Angle, deg | 60 | | | | |
| Trench or bore width, in cm | 7 17 | | | | |
| Soil Unit Weight, pcf kg/m ³ | 120 1922 | | | | |
| Soil Type | 4 | | | | |
| Modulus of soil reaction E', psi kPa | 250 1724 | | | | |
| Slab or Matting: | no slab | | | | |
| Slab thickness, in cm | | | | | |
| Impact Factor on slab or mat | | | | | |
| Slab material | | | | | |
| Slab width across pipe, ft m | | | | | |
| Slab length along pipe, ft m | | | | | |
| odulus of subgrade reaction k, pci MPa/m | | | | | |
| Maximum Hoop Stress, % SMYS: | | | | | |
| Calculated | 26.3% | | | | |
| Allowable | 85% | | | | |
| Fluctuating Hoop Stress, psi MPa: | | | | | |
| Calculated | 4.2 28.7 | | | | |
| Allowable | 20 138 | | | | |
| Requirements / Notes: | | is of ~9000 kgs or MTO Road Legal A | • | | |
| | | ss limit and max allowable fluctuating | • | • | r cyclic loading |
| | which can be assum | ned to be representative of continuous | vehicle traffic over the | pipeline/roadway. | |
| A 1 I 1 I | BNW 4/17/2020 | | | | |
| Analyzed by: | . DINVV 4/17/2020 | | | | |

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Pipelines Crossed by Equipment on Tires

| Location: | i pen | les Crossed by Equipment of | | | |
|--|------------------------|--------------------------------------|--------------------------------|---|-------------------------|
| Description & Purpose | NPS 6 Mindsor Lino | Oversize Vehicle Load Analysis | | | |
| Province | | Permanent crossing? Yes | Type | 3rd Party | |
| | | <u> </u> | d bearing pressure, psi kPa | 110 758 | |
| Equipment: | SHLx5 | | | 48 122 | |
| Label | | | between axles in set, in cm | 6.0 1.83 | |
| Description | | gs/axle under Fatigue/Cyclic loadi | | | |
| Axle Load, lb kg | 99,000 44,898 | | Impact Factor | 1.5 | |
| # axles in set | 1 | | Imbalance Factor | 10% | 1 |
| Line(s) to be crossed: | G) 0.4 | | | | |
| Line Name | 6WL 6.625 16.8 | | | | |
| OD, in cm | | | | | |
| Wall thickness, in mm | 0.189 4.8 | | | | |
| Pipe grade, ksi MPa | 52 359 | | | | |
| Pressure, psi kPa | 500 3447 | | | | |
| Long seam type | ERW | | | | |
| Installation: | 00 100 | | | | |
| Depth of cover, in cm | 39 100 Octiled | | | | |
| Installation type | Settled 60 | | | | |
| Bottom Reaction Angle, deg | | | | | |
| Trench or bore width, in cm | 7 17 | | | | |
| Soil Unit Weight, pcf kg/m ³ | 120 1922 | | | | |
| Soil Type | 4 | | | | |
| Modulus of soil reaction E', psi kPa | 250 1724 | | | | |
| Slab or Matting: | no slab | | | | |
| Slab thickness, in cm | | | | | |
| Impact Factor on slab or mat | | | | | |
| Slab material | | | | | |
| Slab width across pipe, ft m | | | | | |
| Slab length along pipe, ft m | | | | | |
| odulus of subgrade reaction k, pci MPa/m | | | | | |
| Maximum Hoop Stress, % SMYS: | 50 500 | | | | |
| Calculated | 50.5% | | | | |
| Allowable | 85% | | | | |
| Fluctuating Hoop Stress, psi MPa: | 10.4 1 100.7 | | | | |
| Calculated | 19.4 133.7 | | | | |
| Allowable | 20 138 | | | a la alta a la accordia a l'ara | atill as as a loss boot |
| Requirements / Notes: | | ~45000kgs or ~5 x MTO Road Leg | , | | |
| | | p stress limit and max allowable flu | • | The second conversion and the second second second second | jue or cyclic loading |
| | which can be assumed t | o be representative of continuous | venicie tranic over the pipeli | ne/roadway. | |
| Analyzed by: | BNW 4/17/2020 | | | | |
| Allalyzeu by. | | | | | |

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Pipelines Crossed by Equipment on Tires

| Location: | | | | es Crosseu by Equ | -pinent on 1 | | | |
|---|---------|----------------|------------|-------------------------|------------------|----------------------------|--|---------------------|
| Description & Purpose | NPS 61 | Vindsor | I Ine - Ov | versize Vehicle Load | Analysis | | | |
| Province | | made | | Permanent crossing? | | Type | 3rd Party | |
| Equipment: | | | | <u> </u> | | earing pressure, psi kPa | 110 758 | |
| Label | SHLx10 | | | | | ween axles in set, in cm | 157 400 | |
| Description | | | of 9000kc | s/axle assumed Sup | | Axle gauge, ft m | 19.7 6.00 | |
| Axle Load, lb kg | 198,000 | Î | 89,796 | | | Impact Factor | 1.5 | |
| # axles in set | 1 | | , | | | Imbalance Factor | 10% | |
| Line(s) to be crossed: | | | | | | | | |
| Line Name | | 6WL | | | | | | |
| OD, in cm | 6.625 | - I | 16.8 | | | | | |
| Wall thickness, in mm | 0.189 | È. | 4.8 | | | | | |
| Pipe grade, ksi MPa | 52 | Т ¹ | 359 | | | | | |
| Pressure, psi kPa | 500 | - î | 3447 | | | | | |
| Long seam type | | ERW | | | | | | |
| Installation: | | | | | | | | |
| Depth of cover, in cm | 39 | T I | 100 | | | | | |
| Installation type | | Settled | | | | | | |
| Bottom Reaction Angle, deg | | 60 | | | | | | |
| Trench or bore width, in cm | 7 | I. | 17 | | | | | |
| Soil Unit Weight, pcf kg/m ³ | 120 | 1 | 1922 | | | | | |
| Soil Type | | 4 | | | | | | |
| Modulus of soil reaction E', psi kPa | 250 | 1 | 1724 | | | | | |
| Slab or Matting: | | no slab | | | | | | |
| Slab thickness, in cm | | | | | | | | |
| Impact Factor on slab or mat | | | | | | | | |
| Slab material | | | | | | | | |
| Slab width across pipe, ft m | | | | | | | | |
| Slab length along pipe, ft m | | | | | | | | |
| dulus of subgrade reaction k, pci MPa/m | | | | | | | | |
| Maximum Hoop Stress, % SMYS: | | | | | | | | |
| Calculated | | 77.1% | | | | | | |
| Allowable | | 85% | | | | | | |
| Fluctuating Hoop Stress, psi MPa: | | | | | | | | |
| Calculated | N/A | | N/A | | | | | |
| Allowable | 20 | | 138 | | | | | |
| Requirements / Notes: | | | | • | • | Axle limit of 9000kgs. Res | stated from another in the state of the state of | |
| | maximum | allowa | ble hoop s | stress limit. This load | is considered to | o represent a superload o | r over weight vehi | cle permitted load. |
| | | | | | | | | |
| | DAUA/ | 447/0 | | | | | | |
| Analyzed by | : BINVV | 4/17/20 | J20 | | | | | |